

Date: 6-27-2014

Subject: Pre-filter media used during TAPE testing

To Whom It May Concern,

The Modular Wetland System Linear (MWS Linear) is an advanced biofiltration system that utilizes a patented horizontal flow biofiltration chamber. This chamber provides greater surface area, minimizes clogging, and contains a large media bed that can be planted with vegetation to enhance removal efficiency. This chamber is where primary pollutant removal takes place.

To further improve performance of the biofiltration chamber the MWS Linear incorporates a pretreatment chamber that includes pre-filter cartridges. The purpose of the pre-filter cartridges is to remove sediments and hydrocarbons to lessen the pollutant load on the primary biofilter.

During TAPE testing the pre-filter cartridges were fitted with porous blocks (solid) of BioMediaGREEN. These porous blocks are highly effective and suitable for loading conditions commonly found on most sites. On sites that contain a high level of fine clay/silt type sediments, which attach to the media surface, the blocks are prone to pre-mature blinding.

The MWS Linear was installed at a maintenance yard in the City of Portland which stores heavy equipment, work trucks and stockpiles of dirt as well as other supplies. During TAPE testing this site generated extremely high levels of TSS loading which in turn led to premature clogging of the blocks. To address the unusually high level of fine sediment, modifications were made to the porous blocks by adding channels (ribbed) on its surface to increase surface area. While the modified blocks did improve filter life additional improvements were sought to further optimize the pre-filters.

A modified pre-filter cartridge was installed onsite which can be fitted with various types of granular media. Initially it was filled with perlite which is a widely accepted and long used media for removing sediments. The perlite was used as a control to see if a change in the pre-filter media would have any effect on the systems overall pollutant removal performance. Results indicated there was no statistical significance that perlite affected the systems overall pollutant removal efficiency since primary filtration takes place in the biofiltration chamber.



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Once data was gathered on the perlite control group the pre-filter cartridges were filled with small 1" cubes of BioMediaGREEN (same material as blocks). The cubed material was used for the majority of the TAPE field testing. The cubes did not have any effect on the systems overall performance, but greatly improved the filter life of the pre-filter cartridges. Performance with the blocks, perlite and cubes was consistent across all three.

The Department of Ecology assessed all of this data and based on the fact that a change in the media used in the pre-filter cartridge had no effect on the systems overall performance all data was accepted. The MWS Linear was approved with the pre-filter cartridges containing cubed BioMediaGREEN since a majority of the testing was done with this material. This is the current configuration for the MWS Linear and is the standard nationwide. It provides the highest level of filter life and minimizes replacement costs.

If you have any questions please feel free to contact us at your convenience.

Sincerely,

Frul h

Zachariha J. Kent Stormwater Engineer Modular Wetland System, Inc.



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DRAFT TECHNICAL EVALUATION REPORT

MODULAR WETLAND SYSTEM STORMWATER TREATMENT SYSTEM PERFORMANCE MONITORING

Prepared for Bio Clean Environmental Services, Inc.

Prepared by Herrera Environmental Consultants, Inc.



Note:

Some pages in this document have been purposely skipped or blank pages inserted so that this document will copy correctly when duplexed.

TECHNICAL EVALUATION REPORT

MODULAR WETLAND SYSTEM STORMWATER TREATMENT SYSTEM PERFORMANCE MONITORING

Prepared for Bio Clean Environmental Services, Inc. P.O. Box 869 Oceanside, California 92049

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July 23, 2013 Draft

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EXECUTIVE SUMMARY

Modular Wetland System-Linear filtration system (MWS-Linear) is a water guality treatment system consisting of a settling chamber, a cartridge-based media pre-filter, a wetland filtration chamber, and an outlet chamber. The system is housed in a precast concrete vault and can be designed in numerous configurations including piped or grated inlet structures.

From April 2012 through May 2013, Herrera Environmental Consultants, Inc. (Herrera) conducted hydrologic and water quality monitoring of a MWS-Linear for Bio Clean Environmental Services, Inc. at one test installation in Portland, Oregon. Herrera conducted this monitoring to obtain performance data to supports the issuance of a General Use Level Designation (GULD) for the MWS-Linear by the Washington Department of Ecology (Ecology). Monitoring was performed in accordance with procedures described in *Guidance for Evaluating* Emerging Stormwater Treatment Technologies; Technology Assessment Protocol - Ecology (TAPE) (Ecology 2011).



Installation of the monitored Modular Wetland-Linear system at the Albina Maintenance Facility in Portland. Oregon.

This technical evaluation report (TER) was prepared by Herrera to demonstrate satisfactory performance of the MWS-Linear in meeting goals specified by Ecology (2011) for basic treatment, phosphorus treatment, and enhanced treatment.

Sampling Procedures

To evaluate the stormwater treatment performance of the MWS-Linear based on Ecology's TAPE guidelines, a test system was installed at the Portland Bureau of Environmental Services Albina Maintenance Facility in Portland, Oregon (Figure 1). This system is identified herein as the Albina Modular Wetland System (AMWS). Automated monitoring equipment was also installed to continuously measure influent, effluent, and bypass flow volumes. Automated equipment was used to collect flow-weighted composite samples of the system's influent and effluent during 28 separate storm events in the monitoring period. The collected flowweighted composite samples were analyzed for the following water quality parameters:

- Total suspended solids (TSS)
- Particle size distribution (PSD) (influent only)



- Total and dissolved copper
- Total and dissolved zinc
- Total phosphorus (TP)
- Soluble reactive phosphorus (SRP)
- Hardness
- pH

These data were subsequently analyzed in the following ways:

- Computation of pollutant removal efficiencies with bootstrap confidence intervals
- Statistical comparisons of influent and effluent concentrations
- Correlation analysis to examine the influence of treated flow rate on system performance

These results were then compared to TAPE goals for basic, phosphorus, and enhanced treatment.

Hydrologic Performance

The water quality treatment goal for the test system was to capture and treat 91 percent of the average annual runoff volume. Monitoring data showed that stormwater bypassed the AMWS test system during 49 out of 81 monitored events during the 14-month monitoring period. The system was able to treat 75 percent of the total volume that entered the system over this period. Consequently, the goal of treating 91 percent of the volume from the site was not achieved. This was most likely due to the high clay content of the runoff rapidly clogging the pre-filtration system in the Settling Chamber (see *Maintenance Schedule*).

During the monitoring period, there was a negative trend over time for treated flow rate during bypass between each pre-filter change. On average, the pre-filters required changing every 2 months. This high frequency of maintenance was due to the high clay content of the runoff. Under more typical stormwater conditions, it is expected that the pre-filters will last between 6 months and a year before they require changing.

Water Quality Performance

Basic Treatment

The basic treatment goal in the TAPE guidelines is 80 percent removal of total suspended solids for influent concentrations ranging from 100 to 200 milligrams per liter (mg/L). For concentrations less than 100 mg/L, facilities must achieve an effluent goal of 20 mg/L pursuant to TAPE guidelines.



Total suspended solids removal rates ranged from 61 to 98 percent, with a mean value of 84.9 percent. The upper 95 percent confidence interval about the mean effluent concentration was 12.8 mg/L. The TAPE effluent goal is 20 mg/L or less, so the basic treatment criteria were met. Analyses of flow and water quality data indicated the treatment goal for total suspended solids removal was met up to and through the design flow rate of 41 gallons per minute (gpm) (equivalent of 1 gpm/ft² of media) for the MWS-Linear.

Phosphorus Treatment

The phosphorus treatment goal in the TAPE guidelines is 50 percent removal of total phosphorus for influent concentrations ranging from 0.1 to 0.5 mg/L.

A bootstrap estimate of the lower 95 percent confidence limit of the mean percent reduction was 61.7 percent. Consequently, it can be concluded that the mean percent removal was significantly greater than the 50 percent goal specified in the TAPE guidelines. The system exhibited removal greater than 50 percent up to and through the design flow rate of 41 gpm.

Enhanced Treatment

The dissolved zinc treatment goal in the TAPE guidelines is 60 percent removal for influent concentrations ranging from 0.02 to 0.3 mg/L. The dissolved copper treatment goal is 30 percent removal for influent concentrations ranging from 0.005 to 0.02 mg/L. The lower 95 percent confidence limit of the mean percent removal was 60.5 and 32.5 percent for dissolved zinc and dissolved copper, respectively. These data indicate that the TAPE removal criteria were met for both dissolved zinc and dissolved copper. Treatment above the TAPE criteria of 60 percent removal was evident in the dissolved zinc results from treated flow rates up to and including the design flow rate of 41 gpm. For dissolved copper treatment was only evident up to 28 gpm; however, if lab data from 2007 are added to the data set, the flow rate at which 30 percent dissolved copper reduction can be achieved increases to 41 gpm.



INTRODUCTION

The Modular Wetland Systems - Linear (MWS Linear) is a structural stormwater treatment system developed by Bio Clean Environmental Services, Inc. The MWS-Linear utilizes multistage treatment processes, including a BioMediaGREEN filter media for primary filtration and a subsurface flow wetland cell for biological remediation and additional filtration. This system is housed in a modular precast concrete structure that can be designed in many configurations. The MWS-Linear provides water quality treatment of captured flows through the processes of separation, sedimentation, filtration, adsorption, and biological remediation.

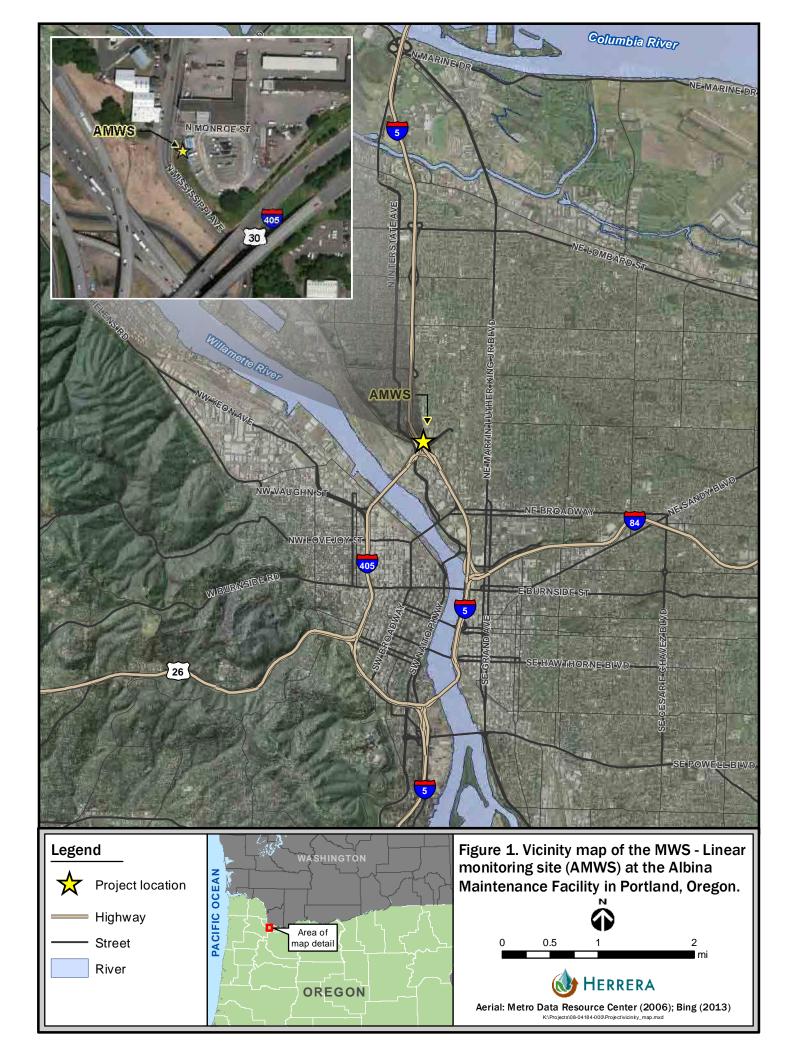
The Washington State Department of Ecology (Ecology) has established specific use level designations for emerging stormwater treatment technologies like the MWS-Linear in accordance with guidelines that are identified by Ecology (2011) in *Technical Guidance for Evaluating Emerging Stormwater Treatment Technologies: Technology Assessment Protocol - Ecology (TAPE)*.

There are three use level designations: pilot, conditional, and general. Pilot and conditional use level designations allow limited application of emerging stormwater treatment technologies in western Washington to facilitate field testing. If this testing shows that the treatment technology meets minimum treatment goals identified in the TAPE, Ecology may issue a general use level designation (GULD) for the technology, permitting its more widespread use in Washington.

TAPE guidelines indicate that a technical evaluation report (TER) must be completed for any stormwater treatment system under consideration for a GULD. Specifically, the TER should document treatment performance of a technology to show that it will achieve Ecology's performance goals for target pollutants, as demonstrated by field testing performed in accordance with the TAPE.

This document is the TER for the MWS-Linear, and was prepared by Herrera MWS-to demonstrate satisfactory performance of the MWS-Linear in meeting goals specified by Ecology (2011) for basic treatment and enhanced treatment. It specifically presents data from a test installation of an MWS-Linear installed at the Portland Maintenance Bureau Albina Maintenance Facility (Figure 1). This monitoring was performed over a 14-month period, from April 14, 2012, through March 31, 2013.





TECHNOLOGY DESCRIPTION

The MWS-Linear stormwater filtration system provides water quality treatment of captured flows through several physical, biological, and chemical unit processes. This section describes the system's physical components, treatment processes, sizing methods, expected treatment capabilities, expected design life, and maintenance procedures.

System Overview

The MWS-Linear can be used in a variety of configurations, including curb, grate, and vaulttype designs (Figures 2, 3, and 4). New construction and stormwater retrofit projects can utilize the modular design of the MWS-Linear, in place of standard catch basin structures, rain gardens, bioretention cells, media filters, or other treatment devices. A variety of inlet, bypass, and wetland chamber designs are available for the MWS-Linear that can be adapted for different stormwater drainage systems. However, the hydraulics within the system itself and the treatment processes are the same for each configuration.

Stormwater runoff enters the MWS-Linear via pipe, curb, or grate-type configurations. For the MWS-Linear with a grate or curb-type opening, a catch basin filter insert facilitates the removal of gross solids before stormwater enters a hydrodynamic separation (settling) chamber. For the MWS-Linear with pipe openings, stormwater enters the settling chamber directly, which is also designed to settle out trash and litter, gross solids, and suspended sediment. Stormwater is then treated by BioMediaGREEN filter cartridges, which remove several pollutants, fine TSS, and hydrocarbons. After the stormwater moves through the BioMediaGREEN filter media, it enters the wetland chamber, which acts as a bioretention filter. The MWS-Linear processes stormwater horizontally through the bioretention media. Within the wetland chamber, a combination of physical, chemical, and biological mechanisms remove additional particulate and dissolved pollutants. Runoff leaving the wetland chamber is controlled by a downstream orifice. The treated runoff leaves the system via the discharge chamber.

Physical Components

The MWS-Linear consists of a series of treatment components, beginning with a catch basin filter insert (for grate and curb-type configurations), a settling chamber, BioMediaGREEN filter cartridge, and finishing with a wetland chamber, which discharges to an outlet chamber. The outlet chamber collects flow from the wetland chamber and internal bypass pipes and routes stormwater to the outlet pipe. The BioMediaGREEN filter media can be removed and replaced to maintain the treatment performance within an acceptable range; the catch basin filter insert, settling chamber, and BioMediaGREEN filter cartridge improve the wetland chamber performance by minimizing the pollutant loading on the wetland media. The primary components of the MWS-Linear are described below.

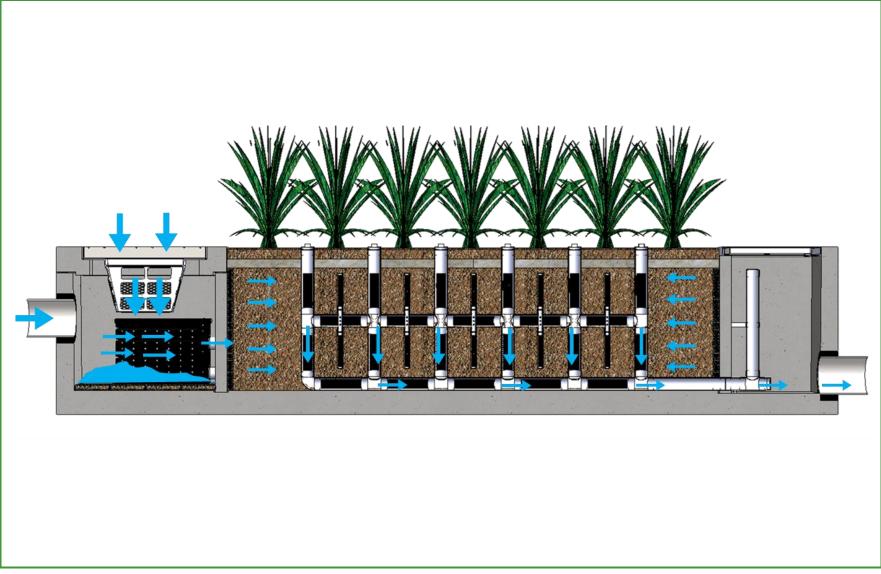


Figure 2. Cross-section of Typical Offline MWS-Linear System with Piped and Grated Inlet Flow.



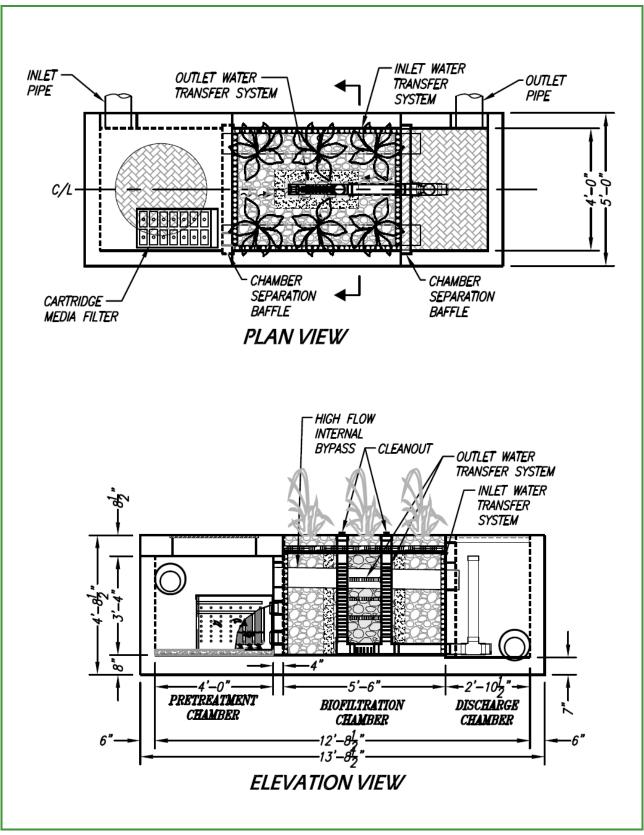


Figure 3. Design Details of Half Size MWS-Linear system with Piped Inlet Flow.

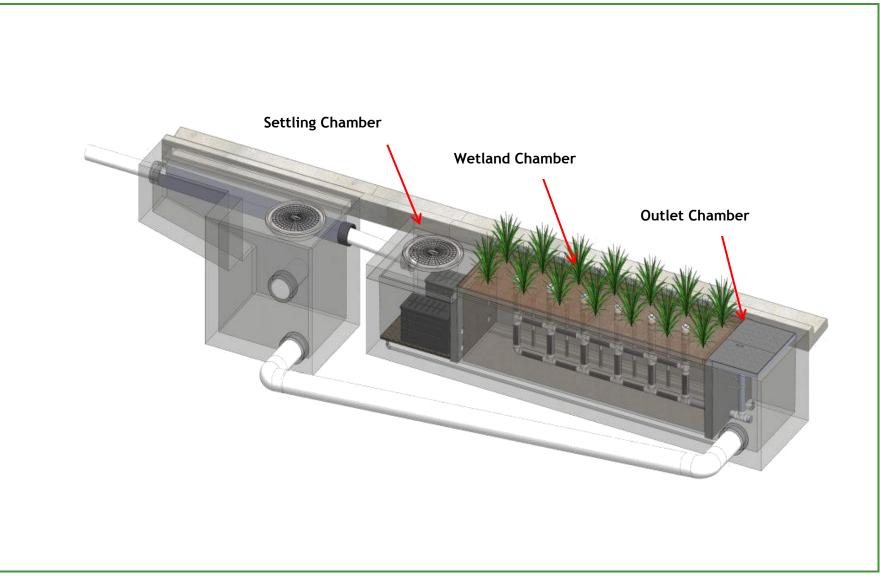


Figure 4. Perspective Rendering of Example MWS-Linear System with Piped Inflow and Upstream Structure.



Structure

The MWS-Linear is a modular, precast concrete structure. Each MWS-Linear concrete structure is available in numerous lengths and widths. There are several alternative configurations and the MWS-Linear can be adapted to a variety of site conditions. Each complete unit weighs approximately 9,000 to 70,000 pounds and requires a boom crane for installation.

Runoff can enter the system via built-in grate or curb inlet or can enter directly into the pretreatment chamber via pipe. The system can be designed at different depths without changing wetland media thickness or detention time. The system's unique horizontal flow biofilter also allows it to be used in volume-based configurations downstream of storage BMPs such as detention basins, ponds, or underground facilities.

The MWS-Linear is constructed with non-corrosive materials. All internal piping is SD35 or SD40 PVC. Catch basin filter insert components, including mounting hardware, fasteners, support brackets, filtration material, and support frame are constructed of non-corrosive materials (316 stainless steel and UV protected/marine grade fiberglass). Fasteners are stainless steel and the primary filter mesh is stainless steel welded screens. BioMediaGREEN filter cartridges are constructed of high strength rotocast HDPE. Mounts are constructed of stainless steel. BioMediaGREEN is an inert rock substrate and is non-corrosive. The drain down filter cover is constructed of high strength rotocast HDPE and stainless steel hinge and mount.

Inlet

The MWS-Linear is available with a built-in grate or curb opening and/or can accept runoff via pipe. In the grate or curb type configuration, a catch basin filter is mounted directly under the opening to intercept trash and debris along with large sediment. The catch basin filter is also fitter with an oil absorbent boom for removal of total petroleum hydrocarbons. The size and shape of the catch basin filter varies from model to model. The catch basin filter utilizes various size screens and an internal bypass for higher flows.

Settling Chamber

The settling chamber is located below the inlet. The settling chamber is designed to provide secondary treatment of stormwater to settle larger suspended solids.

BioMediaGREEN Cartridge Filter

BioMediaGREEN is a proprietary engineered filter media made of a unique combination of inert, naturally occurring materials. This product is non-combustible, stable, biodegradable, and has no known adverse effects on the environment.



BioMediaGREEN filter cubes also contain a high surface area to volume ratio, which promotes elevated levels of chemical and biological processes to treat stormwater. BioMediaGREEN filter cubes are designed to capture high levels of hydrocarbons, including oils and grease, gasoline, diesel, polycyclic aromatic hydrocarbons (PAHs), and other organic chemicals. BioMediaGREEN filter cubes also have the physical ability to block and filter trash, litter, vegetative matter, sediment, total suspended solids (TSS), total and dissolved metals, and bacteria.

Maintenance of the BioMediaGREEN filtration system is simple, and only requires access to the settling basin (each cartridge can easily be lifted by one person even when wet), the used cubes removed, the cartridge housing hosed down, new cubes added, and the cartridge replaced. This maintenance procedure can also be performed with removal of the cartridge. BioMediaGREEN filter cubes are light tan in color when new, and turn a darker color as pollutants are absorbed from stormwater, which allows maintenance crews to easily determine if the filter cubes need replacement. The filter cubes can typically be disposed of in an ordinary landfill (local regulations may apply).

The number of filter cartridges is customizable and can range from 1 to several hundred depending on the treatment flow rate.

Stormwater Conveyance into Wetland Chamber and High Flow Bypass

After stormwater has passed through the settling chamber and BioMediaGREEN cartridge filters, it enters a 4-inch diameter PVC SD35 manifold, which discharges the flow into a perimeter flow distribution matrix/pervious panel that surrounds the wetland chamber (described in the next section).

The MWS-Linear is also available with two high flow bypass pipes near the top of the pretreatment chamber to convey stormwater directly to the outlet chamber when the wetland chamber system capacity is exceeded. Alternative bypass configurations are also available such as an internal weir. Since the wetland chamber is separated from the pre-treatment and discharge chamber, internal bypass has no effect on performance.

Wetland Chamber

The wetland chamber is the final stage of water treatment for the MWS-Linear. The system employs an innovative peripheral (perimeter) void area on all four sides of the biofiltration media that extends the height of the chamber. Incoming stormwater surrounds the biofiltration media bed within the void space and migrates towards the center, vertically extending under drain. As such, it operates similar to a radial cartridge. The horizontal flow path through the media from an outside perimeter maximizes available surface area and treatment capacity. Because flow through the media is horizontal, the media thickness from influent point to effluent points remains constant regardless of the height of the wetland chamber. Therefore, shallower or deeper systems can be specified with minimal effort.

The wetland chamber is filled with a specially engineered 3- to 5-millimeter biofiltration media, which acts as a growing media for the plants and provides treatment of stormwater passing through it. For example, the MWS-Linear Model #MWS-L-4-21 has a wetland chamber

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that is 4 feet wide by 13.8 feet long and has a physical chamber height of 4 feet. The overall O.D. dimensions of this model including the concrete vault, pre-treatment, and discharge chamber is 5 by 22 by 4.8 feet. Radial subsurface flow through the wetland media provides a combination of physical, chemical, and biological water treatment processes to finish treatment of stormwater before it enters through the discharge chamber. As interstitial voids in the media begin to accrete slowly suspended solids from the stormwater, the media becomes more carbon and nutrient rich. This results in more vigorous plant growth and increased biological processing of the stormwater. The ecosystem that develops around the roots of the plants (or rhizosphere) is a complex combination of bacteria, fungi, and plants. These organisms metabolize and decompose influent pollutants and contribute to the treatment performance of the system.

After water passes through the wetland media it enters a series of perforated, 4-inch diameter, SD35 PVC outflow chamber transfer pipes are located along the chamber central axis. The vertically extending perforated under drain pipes join to a common solid horizontal pipe manifold along the bottom of the chamber. This pipe collects sub-surface flow from the wetland chamber and conveys the discharge into the outlet chamber through an orifice control structure that regulates flow and loading rates through the system.

Wetland Chamber Vegetation

A wide variety of plant species can be planted on the surface of the wetland chamber. Vegetation can be selected based on aesthetics, local climatic conditions, traffic safety, and maintenance considerations. However, adequate time is necessary to allow plant roots to colonize the entire wetland chamber before the MWS-Linear system reaches optimal performance, which is typically several months.

Outlet Chamber

The outlet chamber collects discharge from the PVC 4-inch diameter outflow chamber transfer pipe manifold and the internal high flow bypass pipes (if applicable). The manifold connects to the outlet chamber, which contains an orifice flow control structure. The orifice is set to discharge stormwater at a calculated rate equal to the target loading rate and available media surface area given a specific head value. Flows collected in the outlet chamber are routed to a discharge pipe, which can also be configured in different sizes based on individual site conditions and flow rates.

Treatment Mechanisms

The MWS-Linear system provides water quality treatment of captured flows through physical, chemical, and biologic unit processes. Runoff treatment is achieved through separation, sedimentation, filtration, adsorption, biological remediation.

Separation

For MWS-Linear grate-type systems, the grate and catch basin insert located at the inlet intercepts the majority of floatable gross solids, trash and litter, and sediment. In addition, the boom located around the upper perimeter of the catch basin filter insert intercepts

petroleum hydrocarbons before they enter the settling chamber. For curb-type MWS-Linear systems, the settling chamber serves a similar function to intercept trash and litter, gross solids, and sediment.

Sedimentation

The MWS-Linear contains a settling chamber below the inlet, which is designed to promote gravity settling of entrained particles. Settling of large particles in the settling chamber acts as a pretreatment mechanism that improves system performance and extends the life of the BioMediaGREEN filter cartridges and wetland chamber. The amount of sedimentation is a function of particle density, size, water density, turbulence, and residence time. Sedimentation also occurs in the wetland chamber, as the media decreases flow velocity as water moves through the system.

Filtration

Particulates are physically removed from suspension as they contact the BioMediaGREEN filter media. Pollutant removal rates achieved through the filtration cartridges are a function of the stormwater composition, flow, and pretreatment effectiveness. Filtration is also the primary unit process in the wetland chamber. The 3- to 5-millimeter gravel in the chamber creates a non-linear flow path and enhances contact between the stormwater and the media.

Adsorption

Unlike filtration, where physical processes control removal of sediment from suspension, adsorption relies on opposing surface charges of the BioMediaGREEN filter media and wetland chamber media and dissolved species to remove pollutants from stormwater. The BioMediaGREEN filter media is designed with a high surface area so that the binding sites are numerous and not easily exhausted. In addition, both the wetland media and the BioMediaGREEN filter media possess a high cation exchange capacity, which promotes the removal of positively charged dissolved pollutants (including metal ions) from solution.

Biological Remediation

Bacterial growth, supported by the root system in the wetland chamber, performs a number of treatment processes. These vary as a function of moisture, temperature, pH, salinity, and pollutant concentrations. Biologically available forms of nitrogen, phosphorus, and carbon are actively taken into the cells of vegetation and bacteria, and used for metabolic processes (i.e., energy production and growth). Nitrogen and phosphorus are actively taken up as nutrients that are vital for a number of cell functions, growth, and energy production. These processes remove metabolites from the media during and between storm events, making the media available to capture more nutrients from subsequent storms.

Soil organisms in the wetland chamber can break down a wide array of organic compounds into less toxic forms or completely break them down into carbon dioxide and water (Means and Hinchee 1994). Bacteria can also cause metals to precipitate out as salts, bind them within organic material, and accumulate metals in nodules within the cells. Finally, plant growth may metabolize many pollutants, sequester them or rendering them less toxic (Reeves and Baker 2000).

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Site Requirements

Necessary Soil Characteristics

Specific underlying soil characteristics are not required for the MWS-Linear, since it is a selfcontained, watertight system and is fully enclosed. However, the manufacturer does require that the MWS-Linear system be installed on a level bed of gravel 6 inches in depth.

Hydraulic Grade Requirements

The MWS-Linear is completely passive and requires minimum of 3.57 feet (curb-type) or 4.13 feet (grate-type) of fall between the surface flow line and the discharge pipe invert. This amount of fall will ensure that the MWS-Linear creates no standing water. For projects where this amount of fall is not available, an alternate configuration may be possible.

Depth to Groundwater Limitations

Since it is fully enclosed, the MWS-Linear does not have depth to groundwater limitations. The MWS-Linear system is configured with a drain down mechanism, thus any groundwater entering the system will drain away and will not affect the BioMediaGREEN filter media or wetland chamber performance.

Utility Requirements

The MWS-Linear system is a passive system that requires no power, and has a free-draining outfall to an appropriate water conveyance or storage system (i.e., wet pond, storm sewer, or underground infiltration).

Intended Application

The MWS-Linear is intended to be used for stormwater filtration in applications ranging from industrial and commercial to high and low density residential settings. Depending on the land use, maintenance frequency may have to be adjusted accordingly. For instance, the BioMediaGREEN prefilter will have to be changed more frequently when treating highway runoff versus residential street runoff.

Pretreatment Requirements

There are no pretreatment requirements for the MWS-Linear. However, in applications where heavy sediment loading is anticipated, pretreatment will reduce maintenance requirements of the MWS-Linear.

Current Installations

As of March 2013, there are 127 MWS-Linear installations nationwide. Appendix A provides the location, land use, and size of each of these installations.

Sizing Methodology

Laboratory testing of the MWS-Linear indicates high levels of pollutant removal performance at a loading rate of 100 inches an hour or 1.03 gallons per minute per square foot (gpm/sq ft) of surface area of the wetland media inside the wetland chamber. The BioMediaGREEN filter cartridge operates at a loading rate of up to 3 gpm/sq ft of surface area when providing pre-treatment for the wetland chamber. The MWS-Linear is sized based upon total wetland media surface area similar to other biofiltration or cartridge type systems. The MWS-Linear is available in over nine standard models, each model containing different size wetland chambers. Since the MWS-Linear is a horizontal flow biofilter, its operation is similar to a radial cartridge. Influent stormwater fills the void area around the biofiltration bed up to a specific height. The surface area of the biofiltration bed is calculated by multiplying the perimeter by the height of the biofiltration bed. An orifice restrictor is placed downstream of the biofiltration bed in the under drain assembly. The size of the orifice is calculated based upon a target-loading rate of 1.03 gpm/sq ft of surface area, and not to exceed a loading rate of 3 gpm/sq ft for the BioMediaGREEN cartridge. The maximum water level before bypass occurs is used to determine the head over the media and thus the proper size of the orifice.

For preliminary sizing purposes, a sizing table was developed that provides maximum contributing areas for each of the standard sizes of MWS-Linear for both western (Table 1) and eastern Washington (Table 2). The following sections describe the modeling used to generate the tables.

Western Washington

MWS-Linear systems designed for use in western Washington are sized using the Western Washington Hydrology Model, Version 2012 (WWHM2012), or another continuous hydrologic model approved by Ecology, to treat 91 percent of the annual stormwater volume. The remaining 9 percent of the annual stormwater volume bypasses the treatment system through either an external or an internal bypass. The design calculations for the MWS-Linear system determined that the hydraulic loading rate was 1 gpm/sq ft.

For preliminary sizing purposes, a sizing table was developed that provides maximum contributing areas for each of the standard sizes of MWS-Linear systems (Table 1). The sizing table was generated based on a developed ("mitigated") basin that consists of a flat parking area located in a region represented by the SeaTac rain gage with a precipitation-scaling factor of 1.0. The sizing table is to be used for planning level use only. The design engineer must use a continuous model with the site-specific drainage area and precipitation to confirm that the unit will treat the required volume.

Eastern Washington

MWS-Linear systems designed for use in eastern Washington are sized to treat the 6-month, 3-hour storm. For preliminary sizing purposes, a sizing table was developed that provides maximum contributing areas for each of the standard sizes of MWS-Linear systems in Region 3 - Spokane (Table 2). The sizing table is to be used for planning level use only. The design



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engineer must use an approved single event model with the site-specific drainage area and precipitation to confirm that the unit will treat the required volume.

Table 1. MWS-Linear Sizing Table for Western Washington.					
Available MWS Box Sizes (feet)	Total Wetland Media Surface Area (sf)	Water Quality Design Flow Rate Target (cfs)	Maximum Contributing Drainage Area (acres)	15-minute Offline Water Quality Flow Rate (cfs)	15-minute Offline Water Quality Flow Rate (gpm)
4 x 4	22.1	0.049	0.53	0.0486	21.8
3 x 6	34.2	0.076	0.82	0.0752	33.8
4 x 8	50.3	0.112	1.22	0.1119	50.2
4 x 13	62.6	0.139	1.51	0.1386	62.2
4 x 15	76.2	0.170	1.85	0.1698	76.2
4 x 17	89.8	0.200	2.18	0.2001	89.8
4 x 19	103	0.230	2.50	0.2294	103
4 x 21	117	0.261	2.84	0.2607	117
8 x 16	201	0.448	4.88	0.4479	201

Notes:

1. Sizing table intended for planning level use. The design engineer must use WWHM2012 or approved equivalent and the site location mapping to calculate the appropriate facility size for each installation in western Washington.

2. Sizing table meets the offline 15-minute water quality flow rate specified in the Stormwater Management Manual for Western Washington (Ecology 2012).

3. Sizing table based on WWHM2012 parking/flat basin (100 percent impervious) and SeaTac rain gage with precipitation factor of 1.0.

Table 2. MWS-Linear Sizing Table for Eastern Washington.						
Available MWS Box Sizes (feet)	Total Wetland Media Surface Area (sf)	Water Quality Design Flow Rate Target (cfs)	Maximum Contributing Drainage Area (acres)	6-month, 3-hour Flow Rate (cfs)	6-month, 3-hour Flow Rate (gpm)	
4 x 4	22.1	0.049	0.09	0.0471	21.1	
3 x 6	34.2	0.076	0.14	0.0724	32.5	
4 x 8	50.3	0.112	0.21	0.1071	48.1	
4 x 13	62.6	0.139	0.27	0.1359	61.0	
4 x 15	76.2	0.170	0.34	0.1688	75.8	
4 x 17	89.8	0.200	0.40	0.1972	88.5	
4 x 19	103	0.230	0.46	0.2253	101	
4 x 21	117	0.261	0.54	0.2609	117	
8 x 16	201	0.448	0.96	0.4450	200	

Notes:

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1. Sizing table intended for planning level use. The design engineer must use an accepted single event model to calculate the appropriate facility size for each installation in eastern Washington.

2. Sizing table treats the 6-month, 3-hour storm as specified in the Stormwater Management Manual for Eastern Washington (Ecology 2004).

3. Sizing table based on a 100 percent impervious basin (CN = 98) and Region 3 - Spokane precipitation.



Expected Treatment Capabilities

The MWS-Linear is designed to remove suspended solids, gross solids, heavy metals, petroleum hydrocarbons, and nutrients from stormwater. A combination of field and laboratory tests has been conducted on the MWS-Linear and the BioMediaGREEN filter. Specifically, in 2007 a scaled-down laboratory test was conducted to assess the performance of the MWS-Linear system, the same year a separate laboratory test was conducted to assess the performance of the BioMediaGREEN filter alone. Subsequent to these tests, a full-scale field test of the MWS-Linear system was conducted in California to evaluate removal of several stormwater pollutants of concern, including total suspended solids, phosphorus, and total and dissolved metals. The results from these experiments indicated that the combination of the BioMediaGREEN and MWS-Linear filter may remove greater than 80 percent total suspended solids, 70 percent dissolved copper, 88 percent dissolved zinc, and 70 percent total phosphorus. Additional information about previous studies of the MWS-Linear and BioMediaGREEN can be found in the Conditional Use Level Designation (Herrera 2011a) for the MWS-Linear, which was filed with the Washington State Department of Ecology in May 2011.

Estimated Design Life

The non-consumable structural components of the MWS-Linear system are designed to last 25 years before needing maintenance or replacement. The manufacturer recommends that, on average, the BioMediaGREEN media be replaced every 6 to 12 months. If pollutant loading is abnormally high, however (e.g., due to roadway sanding or construction runoff), cartridges may need more frequent replacement.

Installation

The MWS-Linear is a precast watertight concrete structure. The internal components are pre-assembled prior to delivery to the installation site. The system is delivered on a flatbed truck. The installer or contractor will need to provide a crane capable of off-loading the unit and placing it into the ground. Prior to delivery, the appropriate hole dimensions should be excavated, and the bottom 6 inches backfilled and leveled using the appropriate and recommended material compacted to 95 percent of maximum density. If the system is not installed on a level surface, water will not drain properly from the unit, which will result in standing water and sedimentation within the unit.

Prior to installation, the grate inlet and wetland chamber and its internal components must be covered to prevent any contamination from the site. The unit is to remain covered during installation and backfilling to prevent material from entering the unit. Backfilling should be performed in a careful manner, bringing the appropriate fill material up in 6-inch lifts on all sides. Precast sections shall be set in a manner that will result in a watertight joint. In all instances, installation of the MWS-Linear shall conform to ASTM specification C891 *Standard Practice for Installation of Underground Precast Utility Structures*, unless directed otherwise in contract documents.



Operation and Maintenance Requirements

Every installed MWS-Linear unit is to be maintained by the Supplier, or a Supplier approved contractor. The cost of this service varies among providers. The MWS-Linear is a multi-stage self-contained treatment train for stormwater treatment. Each stage protects subsequent stages from clogging. Stages include screening, separation, cartridge media filtration, and biofiltration. The biofiltration stage contains various types of vegetation, which will require annual evaluation and trimming. The maintenance procedures are described below.

- 1. Clean Bio Clean® Catch Basin Filter Screening is provided by a catch basin filter. The filter has a trash and sediment capacity of 2 (curb type) and 4 (grate type) cubic feet. The filter removes gross solids, including litter, and sediments greater than 200 microns. This procedure is easily done by hand or with a small industrial vacuum device. This filter is located directly under the manhole or grate access cover.
- 2. Clean Settling Chamber separation occurs in the pretreatment (settling) chamber located directly under the curb or grated inlet. This chamber has a capacity of approximately 21 cubic feet for trash, debris, and sediments. The chamber targets total suspended solids, and particulate metals and nutrients. Cleaning the settling chamber can be performed with a standard vacuum truck. This chamber is located directly under the manhole or grate access cover.
- 3. Replace Cartridge Filter Media (BioMediaGREEN™) Primary filtration is provided by a horizontal flow cartridge filter utilizing BioMediaGREEN media. Media life depends on local loading conditions and can easily be replaced and disposed of without any equipment. The filters are located in the pre-treatment chamber. Entry into chamber is required to replace BioMediaGREEN media.
- 4. Replace Drain Down Filter Media (BioMediaGREEN™) A drain down filter, similar in function to the cartridge filter is located in the discharge chamber. This filter allows standing water to be drained and filtered out of the separation chamber. This addresses any vector issues, by eliminating all standing water within this system. Replacement of media takes approximately 5 minutes, and is performed without any equipment.
- 5. Trim Vegetation The system utilizes multiple plants in the biofiltration chamber to provide enhanced treatment for dissolved pollutants including nutrients and metals. The vegetation will need to be maintained (trimmed) as needed. This can be done as part of regular landscape maintenance. Be sure never to fertilize the plants growing in the filter.
- 6. Evaluate Wetland Media Flow Hydraulic Conductivity The system's flow can be assessed from the discharge chamber. This should be done during a rain event. By viewing into the discharge chamber, the flow out of the system can be observed. If little to no flow is observed from the lower valve or orifice plate, there may be potential wetland media (biofiltration) maintenance needs.
- 7. Wetland Media Replacement biofiltration is provided by an advance horizontal flow vegetated wetland. This natural filter contains a mix of sorptive media that supports

abundant plant life. The life of this media can be up to 20 years. Replacement of the media is simple. Removal of spent media can be done with a shovel of a vacuum truck.

Reliability

The MWS-Linear is a robust system designed to withstand a variety of conditions in the field. The BioMediaGREEN prefilter is designed to clog well before the media in the wetland chamber. Once the prefilter clogs all influent water is routed to the dual internal bypass pipes, where it safely flows through the system (without treatment) until the unit is maintained. There have been no documented cases of the system releasing pollutants. The likelihood of this occurring is reduced by the design of the bypass. That is, if a very old system begins to clog it will go into bypass before flushing built up pollutants from the media. The system is designed to drain through a drain down between events; this prevents the growth of biofilms on the media, which could affect performance. The frequency of bypass can easily be monitored by checking the high waterline in the pretreatment chamber after an event. If the high waterline is at or above the internal bypass pipes even after modest events, then the prefilter requires changing.

Modular Wetlands Systems, Inc. warranties that the materials used to manufacture its products will be able to withstand and remain durable to environmental conditions for a period of 5 years from the date of purchase.

Other Benefits and Challenges

Unlike many precast stormwater treatment devices, the MWS-Linear has a vegetative component that can add character to the streetscape. The plants in the wetland cell perform an important filtration function, but also are aesthetically pleasing and create a microhabitat in what may otherwise be a barren urban context. Though the aesthetic aspects of the technology are in no way assessed herein, they are mentioned here as an element that may be of interest to municipalities serving the many interests of their citizens.



SAMPLING PROCEDURES

This section describes the sampling procedures that were used to evaluate the performance of the MWS-Linear. It begins with a general overview of the monitoring design and describes the specific goals Ecology has established for the types of treatment that are being sought under the GULD. Separate sections then describe in more detail the site location, test system, monitoring schedule, and the specific procedures used to obtain the hydrologic and water guality data, respectively. Analytical methods, guality assurance and control measures, data management procedures, and data analysis procedures are also discussed.

Monitoring Design

To facilitate performance monitoring pursuant to the TAPE procedures, a 4- by 13-foot internal diameter (ID) MWS-Linear unit was installed for testing purposes at the Portland Bureau of Maintenance Albina Maintenance Facility, which is located at North Albina Avenue and North Monroe Street in Portland, Oregon (Figure 1). This system is identified herein as the Albina Modular Wetland System (AMWS).

Automated equipment was installed in conjunction with the AMWS system to facilitate continuous monitoring of influent, effluent, and bypass flow volumes over a 14-month period extending from April 14, 2012, through May 31, 2013. In association with this hydrologic monitoring, automated samplers were also employed to collect flow-weighted composite samples of the influent and effluent during discrete storm events for subsequent water quality analyses.

Using the data obtained from this monitoring, removal efficiencies and effluent concentrations were characterized for targeted monitoring parameters. These data were subsequently compared to goals identified in the TAPE to support the issuance of a GULD for the MWS-Linear.

These treatment goals are described below for the three types of treatment that are under consideration for inclusion in the GULD:

- 1. Basic Treatment 80 percent removal of total suspended solids for influent concentrations that are greater than 100 mg/L, but less than 200 mg/L. For influent concentrations greater than 200 mg/L, a higher treatment goal may be appropriate. For influent concentrations less than 100 mg/L, the facilities are intended to achieve an effluent goal of 20 mg/L total suspended solids.
- 2. Phosphorus Treatment 50 percent removal of total phosphorus for influent concentrations ranging from 0.1 to 0.5 mg/L
- 3. Dissolved Metals Treatment 30 percent removal of dissolved copper when influent concentrations range from 0.005 to 0.02 mg/L and 60 percent removal of dissolved zinc when influent concentrations range from 0.02 to 0.3 mg/L

Site Location

The AMWS system was installed at the Portland Bureau of Maintenance Albina Maintenance Facility, which is located at North Albina Avenue and North Monroe Street in Portland, Oregon (Figure 1). The Facility includes a parking lot for trucks and heavy equipment as well as outdoor storage of stockpiles of rock and dirt debris and miscellaneous equipment. Stormwater from parking areas for truck and heavy equipment on the south side of the facility is collected in a series of catch basins along the western edge of the lot. Water is conveyed from this system to Portland's municipal drainage system. The AMWS system received stormwater runoff from this parking area, and the treated effluent from the system then discharged into the municipal drainage system.

The drainage area for this parking lot and storage areas is approximately 0.45 acres (see site map in Figure 5 for delineation), and generally slopes from the east to the west with a grade of approximately 5.0 percent. The installation location for the MWS-Linear system within this drainage basin is designated "AMWS" in Figure 5.

Monitoring Schedule

Hydrologic and water quality monitoring were conducted at the AMWS test system over a 14-month period April 14, 2012, through March 31, 2013. During this monitoring period, 28 separate storm events were successfully sampled.

Test System Description

The AMWS test system consists of a 4- by 13-foot ID vault with a piped inflow configuration (Figure 3). The system was constructed with an 8-inch smooth-walled PVC inlet pipe that enters the northeast wall of the pretreatment chamber. Water exits the system through a 12-inch smooth-walled PVC outlet pipe located on the northeast wall of the discharge chamber.

In order to simplify monitoring, the AMWS was installed with an external bypass (Figures 6 and 7). This configuration made it possible to segregate treated and bypassed flows for quantity and quality monitoring. The bypass weir was adjustable in order to maintain required driving head in the AMWS. The weir was adjusted to route the design flow rate of 41 gpm to the system before bypass occurred. The internal bypass weir was capped to prevent internal bypass flows from affecting estimates of treated effluent flow rates and chemistry.

Test System Sizing

The WWHM2012 was used to estimate water quality design flow rates for the study basin. The WWHM2012 model was run for a moderate sloped basin (5 to 15 percent) and with a 15-minute time step. The resultant model run indicated that the water quality design flow rate for the basin was 0.0676 cubic feet per second. However, preliminary flow monitoring indicated that a 1.5-inch storm generated a flow rate of 1.1 cubic feet per second. This is an indication that additional flow was entering the basin. The basin is complex due to potential



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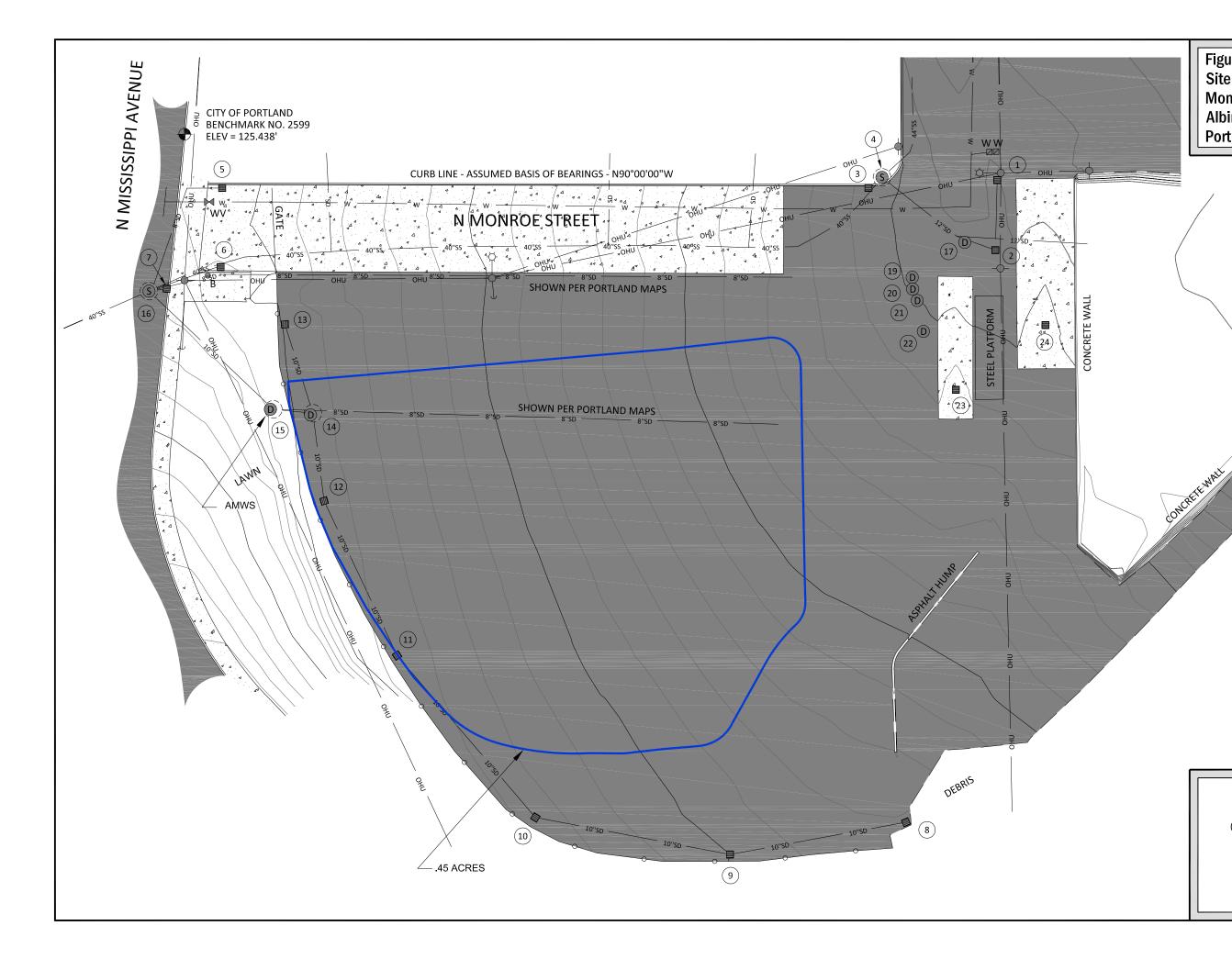
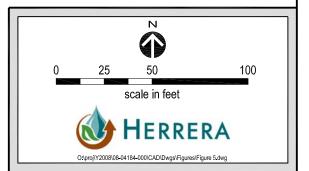
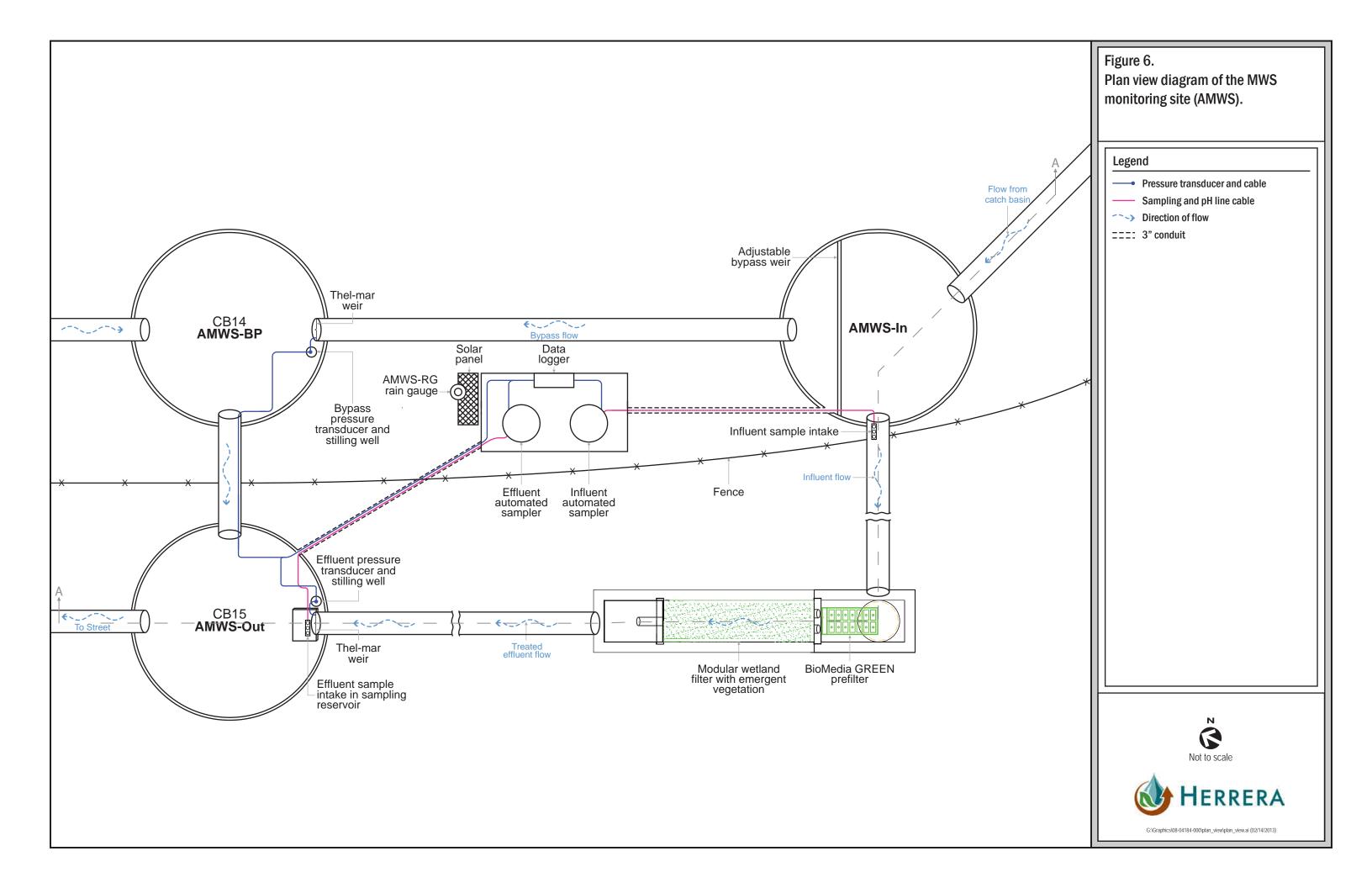
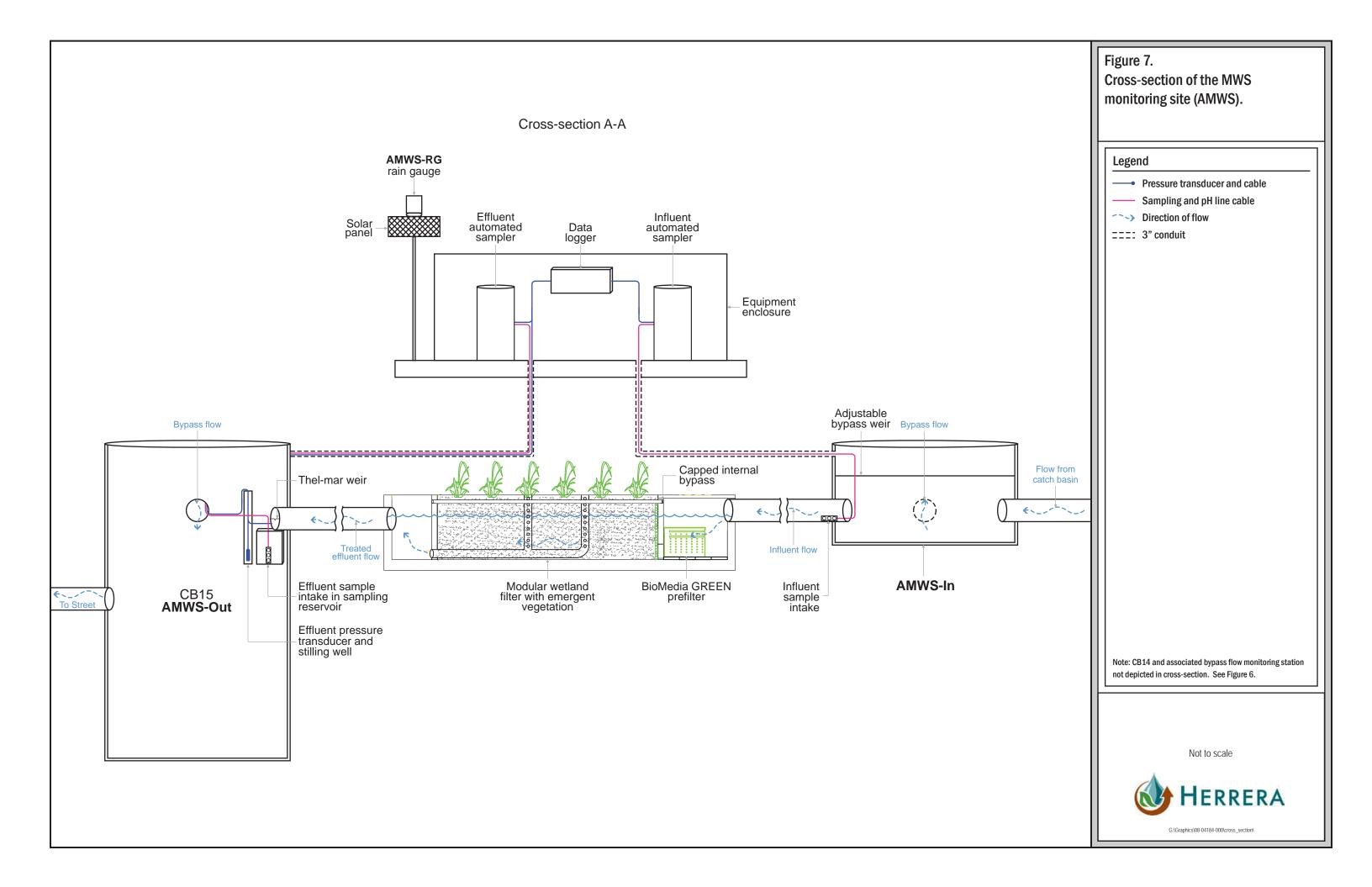


Figure 5. Site map of the MWS -Monitoring site (AMWS) at the Albina Maintenance Facility in Portland, Oregon.

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upslope contributions and the absence of a curb along the base of the basin. Due to the complexity of the drainage, it is exceedingly difficult to estimate the basin size for accurate WWHM3 modeling; consequently, the system was sized based on treating 91 percent of monitored 1.5-inch storms in the study basin. As mentioned above, the design flow rate for the test system was 0.091 cfs (41 gpm).

Maintenance Schedule

Maintenance of the MWS-Linear consists of vactoring the pretreatment chamber and replacing the BioMediaGreen prefilter cartridges. The frequency of these maintenance activities will be a function of solids loading from the site. The Albina Maintenance Facility was a challenging environment for stormwater filtration due to the high degree of fine sediment in the runoff (likely sourced from the debris piles in the yard). The fines (Figure 8) clogged the BioMediaGREEN more quickly relative to what would be expected from suspended solids with a more typical particle size distribution. Numerous steps were taken to alter the design of the BioMediaGreen to decrease maintenance frequency. These steps are described in this section.

Initially solid BioMediaGREEN filters were installed in the pretreatment chamber on April 12, 2012. After noting that the filter was clogging too quickly (Figure 8), it was replaced on May 2, 2012, with a second BioMediaGREEN prefilter that had ribs cut into the filter to increase the surface area (Figure 8). This filter was in place through a dry period during which one sample was collected, but again flow rates through the media became unacceptably low and the BioMediaGREEN media was replaced again on August 8, 2012. As a stopgap, perlite media (Figure 8) was installed for 2 months during which time two samples were collected. On October 26, 2012, cubed BioMediaGREEN was installed (Figure 8), this media provided similar resistance to surface occlusion (blinding) as the perlite but with a more reactive surface. The cubed BioMediaGREEN prefilter lasted until January 27, 2013 (3 months), during which 13 samples were collected. It is anticipated that the cubed BioMediaGREEN prefilter would last 6 to 12 months under normal stormwater loading conditions. Per the current TAPE protocol, maintenance interval will be determined on a site-by-site basis after issuance of a GULD. Analysis of the potential effect of the various prefilters on the final data set is presented below in the Water Quality Results section.

Hydrologic Monitoring Procedures

Generalized schematics of the equipment that was installed in association with the AMWS test system are provided in Figures 6 and 7. The equipment installation was completed on April 22, 2011. Continuous hydrologic monitoring was performed in conjunction with the AMWS test system at four separate monitoring stations: AMWS-BP, AMWS-OUT, AMWS-RG, and AMWS-IN (Figures 6 and 7). AMWS-BP was a bypass flow monitoring station, AMWS-OUT was an effluent flow monitoring station located at the outlet that was used to characterize influent flows since there are no water losses through the system, and AMWS-RG was a precipitation monitoring station. AMWS-IN was only used for sample collection and no hydrologic monitoring was conducted at the station. These hydrologic monitoring stations are discussed in separate subsections below, followed by a summary of the maintenance procedures performed on the monitoring equipment. These monitoring procedures are also described in greater detail

within the quality assurance project plan (QAPP) that were prepared for this study (Herrera 2011b) (Appendix B).

Hydrologic monitoring instruments at each of the stations discussed below were all interfaced with a Campbell Scientific CR1000 datalogger, which served to record data, run simple algorithms based on those data, and control the automated sampling equipment. The datalogger was programmed to scan every 10 seconds and record average readings on a 5-minute time step. The datalogger was interfaced with an Airlink Raven XTV digital cellular modem (Appendix B). This communication system was configured to automatically download data on a 5-minute basis and send text message alarms to field technicians and project managers. Power to the system was supplied using a 12-volt sealed, rechargeable battery that was charged using an 80-watt solar panel installed at the site.

The datalogger, battery, digital cell phone link, and automated samplers were housed in a Knaack box model 69 enclosure (Appendix B). Conduit was installed to convey pressure transducer cabling and autosampler suction lines from the base of the enclosure to each station.

Bypass Flow Monitoring (AMWS-BP)

In order to simplify monitoring, the AMWS was installed with an external bypass (Figures 6 and 7). This configuration made it possible to segregate treated and bypassed flows for quantity and quality monitoring. The bypass weir was adjustable in order to maintain required driving head in the MWS-Linear. The weir was adjusted to route the design flow rate of 0.091 cfs (41 gpm) to the system before bypass occurred. The internal bypass pipes were capped to prevent internal bypass flows from affecting estimates of treated effluent flow rates and chemistry. Engineering design plans for the AMWS system are provided in Appendix C.

Water that passed over the diversion weir was routed through a 10-inch pipe to CB-14 (Figure 6). A 10-inch Thel-Mar weir was installed at the end of this pipe and a hole was drilled through the face of the weir for connecting a section of reinforced 3/8-inch ID polyethylene tubing. The other end of the tubing was connected to a stilling well that was constructed from 3-inch diameter PVC pipe. An Instrumentation Northwest PS9805 submersible pressure transducer (0 to 2.5 psi) was installed in the stilling well to measure water levels behind the Thel-Mar weir. The pressure transducer was interfaced with the Campbell Scientific CR1000 datalogger described above. When bypass occurred, the datalogger converted bypass weir water level readings to estimates of discharge based on standard hydraulic equations (Walkowiak 2006).

Influent/Effluent Flow Monitoring Station (AMWS-OUT)

To facilitate continuous monitoring of influent and effluent flow rates, a monitoring station, designated AMWS-OUT, was established at the end of the 12-inch outlet pipe (Figures 6 and 7). It was assumed that, given the small size and associated low water residence time for the AMWS, the effluent flow would be essentially equivalent to influent. A 12-inch Thel-Mar was installed at the end of the outlet pipe in CB15 and a hole was drilled through the face of





Highly turbid inflow



Solid BioMediaGREEN coated with fines



Installation of temporary perlite prefilter with new cartridge design



Cubed BioMediaGREEN ready for installation

Photos of Sediment Loading and Prefilters Used at the AMWS Monitoring Site. Figure 8.



Ribbed BioMediaGREEN coated with fines



the weir for connecting a section of reinforced 3/8-inch ID polyethylene tubing. The other end of the tubing was connected to a stilling well that was constructed from 3-inch diameter PVC pipe. An Instrumentation Northwest PS9805 submersible pressure transducer (0 to 2.5 psi) was installed in the stilling well to measure water levels behind the Thel-Mar weir.

The AMWS-OUT pressure transducer was interfaced with the same Campbell Scientific CR1000 datalogger described above. The datalogger converted water level readings in the stilling well (which were equivalent water levels behind the Thel-Mar weir) to estimates of discharge based on standard hydraulic equations (Walkowiak 2006).

Precipitation Monitoring Station (AMWS-RG)

In addition to the two pressure transducer stations, a third hydrologic monitoring station, designated AMWS-RG, was installed adjacent to the equipment enclosure (Figures 6 and 7) to facilitate continuous monitoring of precipitation depths. The station was equipped with a Hydrological Services TB4-L60 rain gauge (Appendix B) that was mounted on an 8-foot steel pole and interfaced with the same Campbell Scientific CR1000 datalogger described above.

Monitoring Equipment Maintenance and Calibration

Maintenance and calibration of the rain gauge and flow monitoring equipment was conducted on a routine basis during pre- and post-storm checks. Instrument maintenance and calibration activities were documented on standardized field forms. Rain gauge and level calibration data can be found in the hydrologic data quality assurance memorandum in Appendix D. In addition, on February 14, 2013, a dynamic flow test was conducted using known flow rates from a nearby fire hydrant. The hydrant flows were used to calibrate the Thel-Mar weir equations at AMWS-OUT and AMWS-BP. Results from the dynamic flow testing are presented in Appendix D.

Water Quality Monitoring Procedures

To evaluate the water quality treatment performance of the AMWS test system, water quality sampling was conducted at the influent (AMWS-IN) and effluent (AMWS-OUT) stations (Figures 6 and 7) during 28 discrete storm events over the period from April 2012 through May 2013. A general description of the procedures used for this monitoring is provided herein. A more detailed description of these procedures can also be obtained from the QAPP that was prepared for this study (Herrera 2011b). To facilitate water quality sampling for this study, Isco 6712 portable automated samplers were installed in association with the AMWS-IN and AMWS-OUT stations. The intake strainer for the automated sampler at the AMWS-IN station was positioned in the outlet pipe of the bypass structure (Figures 6 and 7); the intake strainer for the automated sampler intakes were positioned to ensure the homogeneity and representativeness of the collected samples. Specifically, sampler intakes were installed to make sure adequate depth was available for sampling and to avoid capture of litter, debris, and other gross solids that might be present. The sampler suction lines consisted of Teflon tubing with a 3/8-inch inner diameter.

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The following conditions served as guidelines in defining the acceptability of specific storm events for sampling:

- Target storm depth: A minimum of 0.15 inches of precipitation over a 24-hour period
- Antecedent conditions: A period of at least 6 hours preceding the event with less than 0.04 inches of precipitation
- End of storm: A continuous period of at least 6 hours after the event with less than 0.04 inches of precipitation

Antecedent conditions and storm predictions were monitored via the Internet, and a determination was made as to whether to target an approaching storm. Once a storm was targeted, field staff visited each station to verify that the equipment was operational and to start the sampling program. A clean 20-liter polyethylene carboy and crushed ice were also placed in the sampling equipment at this time. The speed and intensity of incoming storm events were tracked using Internet-accessible Doppler radar images. Actual rainfall totals during sampled storm events were quantified based on data from the rain gauge installed at the site. During the storm event sampling, the datalogger was programmed to enable the sampling routine in response to a predefined increase in water level (stage) at AMWS-OUT. The automated samplers were then programmed to collect 220-milliliter sample aliquots at preset flow increments. Based on the expected size of the storm, the flow increment was adjusted to ensure that the following criteria for acceptable composite samples were met at each station:

- A minimum of **10 aliquots**
- Sampling was targeted to capture **at least 75 percent** of the hydrograph
- Due to sample holding time considerations, the maximum duration of automated sample collection was **36 hours**.

After each targeted storm event, field personnel returned to each station, made visual and operational checks of the sampling equipment, and determined the total number of aliquots composited. Pursuant to the sampling goals identified above, the minimum number of composites that constituted an acceptable sample was 10. If the sample was determined to be acceptable, the carboy was immediately capped, removed from the automated sampler, and kept below 6°C using ice during transport to the laboratory. All samples were delivered to the laboratory with appropriate chain-of-custody documentation. Collected flow-weighted composite samples were then analyzed for the following parameters:

- Total suspended solids (TSS)
- Particle size distribution (PSD)
- Total phosphorus (TP)
- Orthophosphorus
- Total and dissolved copper

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- Total and dissolved zinc •
- pН
- Hardness

Additional parameters were measured, but this report only addresses those parameters that are pertinent to the basic, phosphorus, and enhanced treatment GULD.

Sediment Monitoring Procedures

In addition to water sampling, TAPE guidance calls for the assessment of sediment accumulation and sediment particle size distribution within the monitored treatment technology. However, under normal operating conditions, sediment will settle in the pretreatment chamber of MWS-Linear system, the cartridge-based media filter, and within the biofiltration chamber. Each pool of sediment will have a different volume and particle size distribution. To assess the particle size distribution and sediment volume within the each of these areas would be exceedingly difficult. This process would also likely be prohibitively expensive and, due to the difficulty of differentiating between media and accumulated sediment, would result in an inaccurate assessment of accumulated sediment volume and particle size distribution. Due to these considerations, field technicians only recorded sediment depth within the pre-treatment chamber. Particle size distribution of these accumulated sediments was not conducted because it would not provide an assessment of total system treatment; rather, it would only provide an assessment of the setting unitprocess aspect of the pre-treatment.

Analytical Methods

Analytical methods for this project are summarized in Table 3. Test America in Portland, Oregon, was the initial laboratory used for this project. However, due to performance issues with the lab that did not affect data quality, ALS, Inc. in Kelso, Washington, was used for the final 17 collected composite samples. Both laboratories are certified by Ecology, and participate in audits and inter-laboratory studies by Ecology and EPA. These performance and system audits have verified the adequacy of the laboratory's standard operating procedures, which include preventive maintenance and data reduction procedures. Chemoptix Laboratories in West Linn, Oregon was initially used for PSD analysis; when the lab switch occurred, PSD was analyzed at Analytical Resources, Inc. in Tukwila, Washington.

Quality Assurance and Control Measures

Field and laboratory quality control procedures used for the MWS-Linear evaluation are discussed in the following sections. Quality assurance memorandums discussing hydrologic and water quality data can be found in Appendices C and D, respectively.

Field Quality Assurance/Quality Control

This section summarizes the quality assurance/quality control (QA/QC) procedures that were implemented by field personnel to evaluate sample contamination and sampling precision.

		Table 3.	Methods and De	etection Lim	its for Wa	ter Quality	Analyses.		
Parameter	Analytical Method	Method Number ^a	Field Sample Container	Pre-Filtration Holding Time	Total Holding Time ^b	Field Preservation	Laboratory Preservation	Reporting Limit/ Resolution	Units
Total suspended solids	Gravimetric ^c	SM 2540D	20 L HDPE bottle	7 days	7 days	Maintain	Maintain ≤ 4°C	1.0	mg/L
Total phosphorus	Automated ascorbic acid	EPA 365.3		NA	28 days	≤ 6°C	Maintain $\le 4^{\circ}C$, H ₂ SO ₄ to pH < 2	0.002	mg/L
Orthophosphorus	Automated ascorbic acid	EPA 365.3		24 hours ^d	48 hours ^d		Maintain $\leq 4^{\circ}C$, H ₂ SO ₄ to pH < 2	0.001	mg P/L
Hardness	Titration	SM 2340B		28 days	28 days		Maintain ≤ 4°C, HNO3 to pH < 2	0.1	mg/L as CaCO ₃
pН	Potentiometric	SM 4500-H⁺		24 hours ^d	24 hours ^d		Maintain ≤ 4°C	0.01	std. unit
Particle Size Distribution	Sieve and filter	TAPE App. F		7 days	7 days		Maintain ≤ 4°C	NA	microns
Copper, dissolved	ICP-MS	EPA 200.8		18 hours ^f	6 months		Maintain \leq 4°C, HNO ₃ to pH < 2 after filtration ^g	0.002	mg/L
Copper, total				NA			Maintain $\le 4^{\circ}$ C, HNO ₃ to pH < 2	0.002	
Zinc, dissolved	ICP-MS	EPA 200.8		18 hours ^f	6 months		Maintain \leq 4°C, HNO ₃ to pH < 2 after filtration ^g	0.01	mg/L
Zinc, total				NA			Maintain \leq 4°C, HNO ₃ to pH < 2	0.01]

^a SM method numbers are from APHA et al. (1998); EPA method numbers are from US EPA (1983, 1984). The 18th edition of Standard Methods for the Examination of Water and Wastewater (APHA et al. 1992) is the current legally adopted version in the Code of Federal Regulations.

^b Holding time specified in US EPA guidance (US EPA 1983, 1984) or referenced in APHA et al. (1992) for equivalent method.

^c A G4 glass fiber filter will be used for the total suspended solids filtration.

^d EPA requires filtering for dissolved metals within 15 minutes of the collection of the last aliquot. This goal is exceedingly difficult to meet when conducting flow-weighted sampling. A more practical proxy goal for this study is 24 hours.

C = Celsius.

mg/L = milligrams per liter.

HDPE = High-Density Polyethylene

NA = not applicable.

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Field Blanks

Automated sampler tubing was cleaned before the collection of each aliquot using an automated double rinse cycle. In addition, deionized water was back flushed through the sample tubing before each monitored event. Field blanks were collected on November 10, 2011, prior to the first sampled storm event at both monitoring locations. A second set of field blanks was collected on March 1, 2012, after a few storm events had been sampled. The field blanks were collected by pumping reagent-grade water through the intake tubing into a pre-cleaned sample container. The volume of reagent grade water pumped through the sampler for the field blank was similar to the volume of water collected during a typical storm event.

Field Duplicate Samples

Field duplicates were collected for approximately 10 percent of the samples. The station where the field duplicates were collected was chosen at random in advance of the storm event. To collect the field duplicates, a separate automated sampler (i.e., ISCO 6712 Full Size Portable Sampler) with a 9.4-liter bottle was set up at the selected monitoring station with a separate set of sample tubing. The automated sampler was wired to the Campbell Scientific datalogger, and each time the flow trigger occurred, both samplers would draw a stormwater sample at the same time. Sample tubing was staggered, so the two pumps would not affect sample volume if sufficient flow were present. The resultant data from these samples was used to assess variation in the analytical results that is attributable to environmental (natural) and analytical variability.

Flow Measurements

The accuracy and precision of the automated flow measurement equipment were tested prior to the first monitoring round and periodically throughout the project. Level calibration data can be found in the hydrologic data quality assurance memorandum in Appendix D.

Laboratory Quality Control

Accuracy of the laboratory analyses was verified with blank analyses, duplicate analyses, laboratory control spikes, and matrix spikes in accordance with the analytical methods employed. Test America, Inc. and ALS, Inc. were responsible for conducting internal quality control and quality assurance measures in accordance with their own quality assurance plans.

Water quality results were first reviewed at the laboratory for errors or omissions, and to verify compliance with acceptance criteria. The laboratories also validated the results by examining the completeness of the data package to determine whether method procedures and laboratory quality assurance procedures were followed. The review, verification, and validation by the laboratory were documented in a case narrative that accompanied the analytical results.

Data were also reviewed and validated by Herrera within 7 days of receiving the results from the laboratory. This review was performed to ensure that all data were consistent, correct, and complete, and that all required quality control information was provided. Specific quality control elements for the data were also examined to determine if the method quality objectives (MQOs) for the project were met. Results from these data validation reviews were summarized in quality assurance worksheets prepared for each sample batch. Values associated with minor quality control problems were considered estimates and assigned J qualifiers. Values associated with major quality control problems were rejected and qualified with an R. Estimated values were used for evaluation purposes, but rejected values were not used.

Data Management Procedures

Flow and precipitation data was uploaded after each storm event remotely using telemetry systems (i.e., Raven cell link modem) and transferred to a database (LoggerNet and Aquarius software) for all subsequent data management tasks.

Test America, Inc. and ALS, Inc. reported the analytical results within 30 days of receipt of the samples. The laboratories provided sample and quality control data in standardized reports suitable for evaluating project data. These reports included all quality control results associated with the data, a case narrative summarizing any problems encountered in the analyses, corrective actions taken, any changes to the referenced method, and an explanation of data qualifiers. Laboratory data was subsequently entered into a Microsoft Access database for all subsequent data management and archiving tasks.

Data Management Quality Control

An independent review was performed to ensure that the data were entered into the database without error. Specifically, all of the sample values in the database were crosschecked to confirm they were consistent with the laboratory reports.

Data Analysis Procedures

Analysis procedures that were used for the hydrologic and water quality data are summarized below.

Hydrologic Data Analysis Procedures

The compiled hydrologic data were analyzed to obtain the following information for each sampled and unsampled storm during the monitoring study:

- Precipitation depth
- Average precipitation intensity
- Peak precipitation intensity
- Antecedent dry period
- Precipitation duration

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- Bypass flow duration
- Effluent flow duration
- Bypass peak discharge rate
- Effluent peak discharge rate
- Bypass discharge volume
- Effluent discharge volume

A subset of this information was examined in conjunction with sample collection data to determine if individual storm events met the TAPE guidelines for valid storm events. Bypass frequency data was also used to assess when BioMediaGREEN cartridges required replacement.

Water Quality Data Analysis Procedures

Data analyses were performed to evaluate the water quality treatment performance of the test system. The specific procedures that were used in these analyses are as follows:

- Statistical comparison of influent and effluent concentrations
- Calculation of pollutant removal efficiency using bootstrap analysis
- Calculation of pollutant removal efficiency as a function of flow

Each of these procedures is described in more detail in the following subsections.

Statistical Comparisons of Influent and Effluent Concentrations

Pollutant concentrations were compared for paired influent and effluent across all storm events using a 1-tailed Wilcoxon signed-rank test (Helsel and Hirsch 2002). Using a paired test, differences in the influent and effluent concentrations could be more efficiently assessed, because the noise (or variance) associated with monitoring over a range of storm sizes can be factored out of the statistical analyses. A 1-tailed test was used to evaluate the specific hypothesis that effluent pollutant concentrations were significantly lower than those in the influent were. In all cases, the statistical significance was evaluated at an alpha level (α) of 0.05.

Calculation of the Pollutant Removal Efficiency using Bootstrap Analysis

The removal (in percent) in pollutant concentration during each individual storm (ΔC) was calculated as:

$$\Delta C = 100 \times \frac{\left(C_{in} - C_{eff}\right)}{C_{in}}$$

Where: C_{in} = Flow-weighted influent pollutant concentration

 C_{eff} = Flow-weighted effluent pollutant concentration

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After the percent removal for each qualifying event was calculated, the mean percent removal values and 95 percent confidence interval about the mean were estimated using a bootstrapping approach (Davison and Hinkley 1997). Bootstrapping offers a distribution-free method for estimates of confidence intervals of a measure of central tendency. The generality of bootstrapped confidence intervals means they are well suited to non-normally distributed data or datasets not numerous enough for a powerful test of normality.

To perform the bootstrapping analysis, the percent removal values for each valid event were sampled randomly with replacement until a new synthetic percent removal dataset of equivalent size was generated. The median percent removal was then calculated on the synthetic dataset and the process was repeated. Repetition generates a distribution of possible values for the mean. Quantiles of this distribution are confidence intervals of the statistic. For example, in the analysis the mean was replicated 10,001 times; after sorting the replications, the 250th and 9,750th elements constituted the 95 percent confidence interval of the median, while the reported mean was the 5,000th ranked value.

The results from this test were used to determine if the mean percent removal was significantly different from percent removal thresholds presented in TAPE (e.g., 80 percent total suspended solids removal).

Calculation of Pollutant Removal Efficiency as a Function of Flow

To determine pollutant removal performance as a function of flow rate the sampled flow rate must first be calculated. Specifically, for composite samples the instantaneous flow rates associated with each aliquot were averaged over the sampled event to generate an average sampled flow rate. This value was then compared with the percent pollutant removal for the event. This process was repeated for each sampled event, the results were plotted on a percent removal versus sampled flow rate graph, and a regression analysis conducted to determine if system performance varied as a function of influent flow rate.



DATA SUMMARIES AND ANALYSIS

This section summarizes data collected during the 2012-2013 monitoring period. The presentation of these data is organized under separate subsections for the hydrologic and water quality monitoring results, respectively. A memorandum discussing the quality of the hydrologic data is presented in Appendix D, while Appendix E presents a quality assessment of the water quality data.

Hydrologic Data

To provide some context for interpreting the data, this section begins with a comparison of rainfall totals measured during the monitoring period relative to historical data. Appendix D summarizes results from the quality assurance review that was performed on hydrologic data prior to their analysis herein.

Historical Rainfall Data Comparison

To provide some context for interpreting the hydrologic performance of the MWS-Linear, an analysis was performed on rainfall data collected at the National Weather Service (NWS) rain gauge at Portland Airport (PDX) to determine if rainfall totals from the monitoring period (i.e., April 1, 2012, through May 31, 2013) were anomalous. The NWS rain gauge is located at Portland International Airport, approximately 4.9 miles northeast of the AMWS rain gauge. The analysis specifically involved a comparison of rainfall totals measured at the PDX rain gauge over the monitoring period to averaged totals for the same gauge from the past 73 years. These data are summarized in Table 4 along with data from the rain gauge associated with the AMWS monitoring site.

Results from this analysis showed the average annual rainfall total at the Portland Airport rain gauge from 1940 through 2013 was 42.9 inches. In comparison, the rainfall total at the same rain gauge over the monitoring period was 41.3 inches. This value is within the normal range of rainfall (i.e., 25th to 75th percentile) for the Portland Airport rain gauge based on the 73-year rainfall record, thus the rainfall total during the monitoring year is generally representative of rainfall during an average year.

Table 4 also indicates that precipitation measured at the Albina Maintenance Facility Bureau of Environmental Services gauge were similar to rainfall measurements at PDX during the monitoring period. However, rain data collected with the project rain gauge at AMWS-RG were approximately 17 percent greater than at the Albina Maintenance Facility Bureau of Environmental Services or PDX gauge. This discrepancy is discussed further in the hydrologic quality assurance assessment (Appendix D).

Table 4. Li	Table 4.Monthly and Annual Precipitation Totals (in inches) for 2012-2013 at the MWS- Linear Monitoring Site, Compared to Historical Totals at Portland Airport.								
Month	AMWS Rainfall Data (2012-2013) ^a	Portland Albina Maintenance Facility BES Gauge Rainfall Data (2012-2013) ^b	Portland Airport NWS Station PDX Rainfall Data (2012-2013)	Portland Airport NWS Station PDX Rainfall Data (1940-2013) ^c					
April	4.09	3.18	3.25	2.73					
Мау	3.83	3.11	3.37	2.47					
June	3.45	2.98	4.10	1.70					
July	0.39	0.29	0.21	0.65					
August	0.00	0.01	0.00	0.67					
September	0.02	0.01	0.04	1.47					
October	6.41	5.61	6.14	3.00					
November	9.35	8.32	8.23	5.63					
December	9.6	8.54	7.56	9.63					
January	3.09	2.83	3.49	4.88					
February	3.22	1.48	1.26	3.66					
March	2.19	2.09	1.46	3.68					
April	2.67	2.38	2.19	2.73					
May	5.19	4.21	4.57	3.35					
Total	53.5	45.04	45.87	46.25					

AMWS: Albina Modular Wetland System

BES: Bureau of Environmental Services

^a Source: AMWS RG precipitation monitoring station for the AWMS

^b Source: Portland Bureau of Environmental Services

^c Source: Portland Airport rain gauge (<u>http://www.wrh.noaa.gov/pqr/pdxclimate/index.php</u>). Based on average monthly and annual precipitation totals measured over the period from 1940 to 2013.

Water Budget

The water budget for the AMWS test system was analyzed to determine bypass frequency and volume (Table 5). WWHM modeling indicated that with the estimated basin area of 0.45 acres, the water quality design flow rate is 0.091 cfs or 41 gpm.

Separate analyses of hydrologic data were performed to meet the following objectives:

- Determine whether treatment goals for the test system were met based on the volume treated and bypassed
- Determine whether bypass frequency and volume varied as a function of storm rainfall depth, storm rainfall intensity, influent flow volume, and sampling date
- Determine site specific maintenance frequency by examining bypass over the course of the study

The data used in these analyses are presented in their entirety in Appendix F.

Storm Start Date & Time	Storm Depth (inches)	Peak Storm Intensity (in/hr)	Total Volume (gpm)	Bypass Volume (gallons)	% of Total Volume Bypassed	Peak Treated Flow Rate during Bypass (gpm)
		New Pre-Filter Ins	stalled 4/12/2012 (Solic	BioMediaGREEN)		
4/17/2012 21:20	0.31	0.03	1168	407	26	24.1
4/19/2012 8:30	0.68	0.02	1499	991	40	12.0
4/29/2012 22:50	0.33	0.01	1786	112	6	19.5
5/1/2012 13:10	0.15	0.03	902	98	10	13.4
		New Pre-Filter Ins	talled 5/2/2012 (Ribbe	d BioMediaGREEN)		
5/4/2012 5:10	0.41	0.08	2133	4179	66	45.3
5/22/2012 8:35	0.37	0.03	3689	497	12	38.5
5/24/2012 19:10	0.15	0.03	1330	165	11	29.6
5/25/2012 19:35	0.21	0.02	1249	254	17	26.7
6/4/2012 20:20	0.63	0.04	2836	1885	40	8.7
6/7/2012 3:10	0.52	0.02	1802	1286	42	5.7
6/8/2012 7:10	0.57	0.1	839	2806	77	3.9
6/22/2012 18:40	0.5	0.04	1428	281	16	10.1
6/24/2012 3:45	0.23	0.02	388	188	33	2.4
		New Pre-	Filter Installed 8/28/20	12 (Perlite)		
10/14/2012 19:15	0.65	0.05	6309	190	3	41.8
10/15/2012 12:30	0.58	0.06	5210	2370	31	41.8
10/19/2012 13:00	0.39	0.08	3286	33	1	40.6
		New Pre-Filter Inst	alled 10/26/2012 (Cube	ed BioMediaGREEN)	1	1
10/27/2012 6:50	0.61	0.03	4834	272	5	46.7
10/28/2012 6:15	1.04	0.03	10302	399	4	48.0
10/29/2012 22:45	0.65	0.05	5786	572	9	48.0
11/11/2012 13:20	1.41	0.02	12362	84	1	42.3
11/17/2012 3:05	0.72	0.04	5820	267	4	40.6
11/18/2012 16:10	2.27	0.08	24874	8491	25	37.0
11/20/2012 3:50	0.58	0.1	5170	2710	34	30.0
11/20/2012 19:25	0.28	0.02	2251	789	26	26.1
11/21/2012 9:15	0.19	0.03	1519	154	9	23.4
11/23/2012 8:25	1.61	0.03	16628	6982	30	23.4
11/29/2012 6:15	0.57	0.03	4597	762	14	20.4
11/30/2012 17:35	0.7	0.04	5181	6085	54	21.0
12/1/2012 14:10	0.86	0.03	8123	2694	25	16.3
12/3/2012 22:30	0.51	0.03	2937	5052	63	12.0
12/4/2012 9:45	0.82	0.05	8116	2437	23	42.9
12/11/2012 11:20	0.33	0.03	3119	918	23	30.9
12/15/2012 9:10 12/16/2012 3:15	0.38	0.03	2600 11554	490 4597	16 28	24.3 23.9
12/19/2012 3:15	1.37	0.03	20266	8113	28	23.9
12/19/2012 2:10	0.44	0.03	4298	61	1	17.8
12/25/2012 3:10	1.13	0.02	10044	2620	21	17.0
1/6/2013 19:50	0.56	0.02	4812	226	4	25.7
1/24/2013 17:50	0.5	0.02	3096	51	2	25.0
2/22/2010 0:00	0.07		talled 1/27/2013 (Cube			00.0
2/22/2013 9:30	0.67	0.03	9208	1442	14	38.6
3/19/2013 15:35	1.03	0.04	11259	3555	24	31.8
4/5/2013 14:20	0.63	0.09	4349	2182	33	32.3
4/6/2013 16:45	0.71	0.02	6524	131	2	18.2
4/10/2013 8:50	0.15	0.05	1468	157	10	26.1
			talled 5/6/2013 (Cubec			
5/16/2013 12:15	0.17	0.08	1422	440	24	47.6
5/21/2013 11:15	0.43	0.06	3522	543	13	45.6
5/22/2013 5:40	2.78	0.05	22799	24475	52	31.8
5/27/2013 2:20	0.76	0.1	8473	1213	13	21.9

gpm: gallons per minute

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Performance in Relation to Design Treatment Goal

The water quality treatment goal for the AMWS test system was to capture and treat 91 percent of the average annual runoff volume. Precipitation and flow data measured during storms that produced bypass flow are presented in Table 5. These data indicate that the AMWS test system bypassed during 49 out of 81 qualifying storm events that occurred from April 1, 2012, through May 31, 2013. The system was able to treat 75 percent of the total 14-month volume. Consequently, the goal of treating 91 percent of the volume from the site was not achieved. This was most likely due to the high clay content of the runoff rapidly clogging the pre-filtration system in the Settling Chamber (see Maintenance Schedule section above). The maintenance frequency is discussed in more detail below.

Treated Flow Rate during Bypass

In order to investigate system performance over the course of the study period, peak treated flow rate during bypass was assessed as a function of time. During bypass, the full 2.3 feet of wetland media are activated, so the peak treated flow rate during bypass should be at or above the water quality design flow rate. If this flow rate consistently falls below the design flow rate, it is likely that the pre-filter media are clogging. Figure 9 presents a plot of treated bypass flow rate through the course of the 14-month study. As is apparent, the treated flow rate decreases between each pre-filter change. In the three periods during which the cubed BioMediaGREEN was installed, the time it took for the treated flow rate to drop to 50 percent of the design flow rate ranged from 1 month to 3 months. These data indicate that for an industrial site with fine TSS loading such as that observed at the Albina Maintenance Facility testing site, a maintenance interval of about 2 months would be appropriate. If the MWS system is granted TAPE approval, site-specific maintenance intervals will be determined for each installation. Under more typical loading conditions, the manufacturer expects the maintenance interval to be around 6 months.

Water Quality Data

This section summarizes water quality data collected during the monitoring period at the AMWS, including a comparison of data compiled over this period with guidelines identified by Ecology (2011) for assessing data acceptability. Monitoring results for each parameter are summarized and discussed in separate sections. Field forms completed by staff during each sampling visit are presented in Appendix G. Individual Storm Reports showing sample collection times in relation to influent and effluent hydrographs are presented in Appendix H for all sampled storm events. In addition, laboratory reports for each sampled event are presented in Appendix I.

Comparison of Data to TAPE Guidelines

Ecology (2011) provides guidelines for determining data acceptability based on the characteristics of sampled storm events and the collected samples. The data collected through this monitoring effort are evaluated relative to these guidelines in the following subsections. In this section, only the data that are being submitted as valid for TAPE

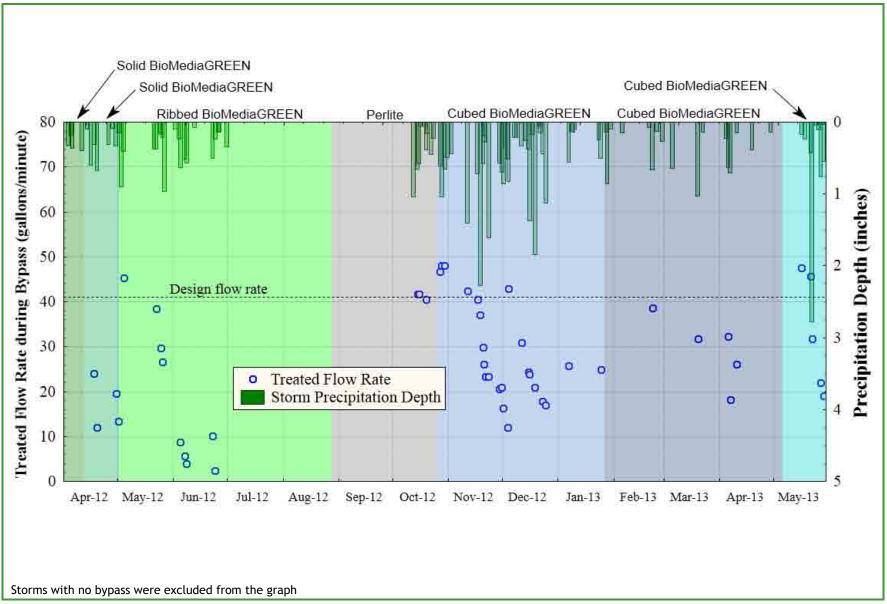


Figure 9. Temporal Plot of Peak Treated Flow Rate during Bypass and Storm Precipitation Depth.

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certification are presented. Water quality and hydrologic data from all events, including those that did not meet the TAPE criteria, are presented in Appendix F.

Storm Event Guidelines

During the April 14, 2012, through March 31, 2013 monitoring period, 28 storm events were sampled to characterize the water quality treatment performance of the AMWS Filter test system. Precipitation data from the sampled storm events was compared to the following TAPE storm event guidelines:

- Minimum precipitation depth: 0.15 inches
- Minimum antecedent dry period: 6 hours with less than 0.04 inches of rain
- Minimum storm duration: 1 hour
- **Minimum average storm intensity:** 0.03 inches per hour for at least half the sampled • storms

Summary data related to these guidelines are presented in Table 6 for each of the 28 sampled storm events. These data show the guideline for minimum precipitation depth (0.15 inch) was met during all storm events except the April 29, 2013, event. Because it was determined that the precipitation gauge may have been overestimating rainfall by 17 percent, two additional storms may have not met the minimum storm depth requirement of 0.15 inches: the April 10, 2013, and the May 16, 2013, event (Table 6). All three of these events had precipitation intensities that exceeded 0.03 inches/hour, so they were included in the final data set and analyzed herein. The minimum, median, and maximum precipitation depths across all 28 sampled storm events were 0.14, 0.51, and 2.27 inches, respectively. The guideline for minimum antecedent dry period (6 hours) was met for all 28 of the events. The storm duration criteria (1 hour) was also met for all 28 storm events except the April 19, 2013, event which was a short intense event lasting 0.3 hours. The April 19, 2013, event was included in the final analysis because it met other storm and sampling requirements. Antecedent dry periods during the sampled storm events ranged from 9.5 to 416.8 hours, with a median value of 33.3 hours. Storm durations ranged from 0.3 to 35.2 hours, with a median value of 10.0 hours (Table 6).

The minimum average storm intensity of 0.03 inches per hour was achieved for 80 percent of the sampled storm events (Table 6). The TAPE storm event guidelines recommend this threshold for at least half of the sampled storms; consequently this criterion was also met.

Sample Collection Guidelines

As described in the methods section, automated samplers were programmed with the goal of meeting the following criteria for acceptable composite samples that are identified by Ecology (Ecology 2011):

- A minimum of 10 aliguots were collected for each event.
- Sampling was targeted to capture at least 75 percent of the hydrograph.
- Due to sample holding time considerations, the maximum duration of automated sample collection at all stations was 36 hours.

Storm Start Date & Time	System to St Storm Precipitation Depth (in)	Storm Antecedent Dry Period (hours)	Storm Precipitation Duration (hours)	Average Storm Intensity (inches/hour) ^b
	0.60		10.1	0.06
4/15/2012 22:45 4/17/2012 21:20	0.80	51.4 36.8	9.2	0.08
				0.034
4/19/2012 8:30	0.68	28.6	9.3	
4/25/2012 20:50	0.31	13	9.8	0.032
5/2/2012 21:50	0.90	29.8	15.4	0.058
5/21/2012 4:45	0.38	16.8	13.4	0.028
10/14/2012 19:15	0.65	45.9	6.7	0.097
10/15/2012 12:30	0.58	10.9	8.5	0.068
10/28/2012 6:15	1.04	10	23.3	0.045
10/29/2012 22:45	0.65	18.8	17.2	0.038
10/31/2012 5:25	0.49	16.1	33.3	0.015
11/23/2012 8:25	1.61	44.5	17.8	0.091
11/29/2012 6:15	0.57	20	31.2	0.018
12/2/2012 14:10	0.35	9.5	25.8	0.014
12/3/2012 22:30	0.51	13	4.3	0.118
12/11/2012 11:20	0.33	44.5	7.4	0.044
12/19/2012 2:10	1.85	17.4	35.2	0.052
1/23/2013 12:15	0.25	214.1	4.7	0.054
1/24/2013 17:50	0.50	25.7	16.8	0.03
2/22/2013 9:30 ^a	0.67	41.6	6.4	0.104
3/19/2013 15:35 ^a	1.03	71.7	16	0.064
4/4/2013 8:00	0.22	305.2	7.5	0.029
4/6/2013 16:45	0.71	10.5	30.8	0.023
4/10/2013 8:50	0.15	63.5	3.2	0.047
4/18/2013 20:45	0.39	69.9	10.9	0.036
4/29/2013 3:15	0.14	236.4	0.3	0.420
5/16/2013 12:15 ^a	0.17	416.8	4.8	0.036
5/21/2013 11:15 ^a	0.43	67	6.3	0.068
Minimum	0.14	9.5	0.3	0.014
Median	0.51	33.3	9.95	0.046
Maximum	2.27	416.8	35.2	0.420

Values in **bold** do not meet storm event guidelines recommended in the TAPE (Ecology 2011).

Values in *italics* indicate the events which may not meet the TAPE guidelines for precipitation depth because the project precipitation gauge may not have been properly calibrated.

^a All sampled events were flow-weighted composite sampled except these events, which consisted of samples collected above a high flow rate threshold.

^b Majority of events exceeded the 0.03 in/hr rainfall intensity criteria

The guideline for minimum number of sample aliquots (10) was met for all of the sampled storm events (see Table 7). It should be noted that 4 of the 28 sampled events were peak

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flow sample events, not flow weighted composites. The TAPE (2011) indicates that samples must represent a wide range of treated flows; in order to get samples representative of the highest treated flow rates discrete peak flow sampling is required.

Storm Start Date & Time	Influent and Effluent Sample Aliquots (#)	Influent and Effluent Storm Coverage (%)	Influent and Effluent Sampling Duration
4/15/2012 22:45	18	92.3	8.6
4/17/2012 21:20	31	97.9	8
4/19/2012 8:30	32	95.1	6.8
4/25/2012 20:50	50	98	5.4
5/2/2012 21:50	75	81.4	10.4
5/21/2012 4:45	53	96.7	9.7
10/14/2012 19:15	35	96.5	6.5
10/15/2012 12:30	39	98	5.9
10/28/2012 6:15	74	94.9	16.1
10/29/2012 22:45	31	95.3	14.7
10/31/2012 5:25	33	94.4	23.9
11/23/2012 8:25	80	77.3	12.9
11/29/2012 6:15	63	98.4	24.1
12/2/2012 14:10	24	77.5	19.2
12/3/2012 22:30	10	83.4	3.8
12/11/2012 11:20	69	97.3	4.2
12/19/2012 2:10	80	71	23.7
1/23/2013 12:15	32	99.2	6.1
1/24/2013 17:50	20	88.7	12.8
2/22/2013 9:30 ^a	20	NA	0.4
3/19/2013 15:35 ^a	55	NA	0.8
4/4/2013 8:00	12	89.4	5.3
4/6/2013 16:45	36	96.8	27.8
4/10/2013 8:50	41	95.6	5.3
4/18/2013 20:45	56	96.6	7.3
4/29/2013 3:15	24	91.2	3.3
5/16/2013 12:15 ^a	20	NA	0.4
5/21/2013 11:15 ^a	12	NA	0.2
Minimum	10	71	0.2
Median	35	95.2	7.3
Maximum	80	99.2	27.8

Values in **bold** do not meet storm event guidelines recommended in the TAPE (Ecology 2011) NA = not applicable

^a All sampled events were flow-weighted composite sampled except these events, which consisted of samples collected above a high flow rate threshold

The criterion for minimum portion of storm volume covered by sampling (75 percent) was met for all but one of the sampled flow-weighted storm events (see Table 7). The December 19, 2012, event had 71 percent sampling coverage. This was deemed close enough to 75 percent and the sample was included for analysis.

PERFORMANCE EVALUATION

This section evaluates water quality data based on treatment goals addressed in this TER.

Particle Size Distribution

The TAPE guidelines state that Pacific Northwest stormwater typically contains mostly siltsized particles; thus, PSD results should be provided to indicate whether the stormwater runoff analyzed is consistent with particle sizes typically found in urban runoff in this region.

Two separate laboratories were used for PSD analysis. For the first 18 events, Chemoptix, Inc. was used, while Analytical Resources, Inc. was used for the last 10 events. The laboratories where switched due to inadequate service from the first laboratory and the fact that they could not bin the PSD data in the desired format. The separate PSD results obtained from the Chemoptix, Inc. and Analytical Resources, Inc. are shown in Figures 10 and 11, respectively.

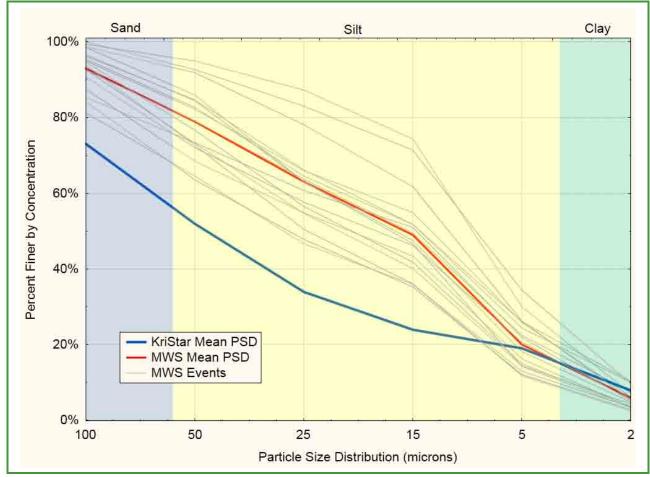


Figure 10. Influent PSD Results from Chemoptix (First 18 Samples).

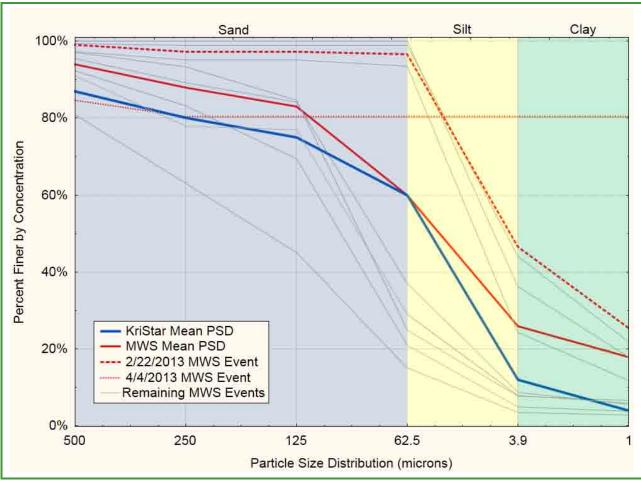


Figure 11. Influent PSD Results from Analytical Resources, Inc. (Last 10 Samples).

In Figure 10, it is apparent that the suspended solids in the stormwater are mostly comprised of silt sized particles. As was indicated in the *Maintenance Schedule* section above, the stormwater at the AMWS test site was unusually turbid. In order to quantify this, the mean PSD from a previous TAPE monitoring project (KriStar Perk Filter) was plotted with the AMWS data in Figure 10. As is apparent there is 25 percent more silt at the AMWS site and an equivalent amount of clay. A somewhat similar pattern was observed with the PSD results from Analytical Resources, Inc. (Figure 11). Figure 11 shows there is, on average, equivalent silt content between AWMS and the KriStar data and 14 percent more clay at the AMWS site. In both cases, there appears to be more fine sediment (either silt or clay) being exported from the AMWS site than from the KriStar site.

This likely explains why the pre-filters were rapidly clogging at the AMWS site (see *Maintenance Schedule* and *Treated Flow Rate during Bypass* sections above). Figure 11 also highlights two events that produced PSD results that are considered outliers. The PSD results from the February 22, 2013, event indicated that 80 percent of the suspended solids were finer than clay (colloidal). This was deemed a spurious result and the PSD results were not used in calculating the mean PSD for the site; however, the chemistry results for the same sample appeared typical so they were included in the final analyses. Also noted on Figure 11 is the PSD result from February 22, 2013. This sample exhibited the highest clay content

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(47 percent) of any of the accepted samples and was characterized by only 61 percent TSS removal (see Basic Treatment section below).

Basic Treatment

The basic treatment goal listed in the TAPE guidelines indicate that the bootstrapped 95 percent lower confidence interval (LCL95) of the mean total suspended solids (TSS) removal must be greater than or equal to 80 percent for influent concentrations ranging from 100 to 200 mg/L. For influent TSS concentrations less than or equal to 100 mg/L but greater than 20 mg/L, the upper 95 percent confidence interval (UCL95) of the mean effluent concentration must be less than or equal to 20 mg/L. There is no specified criterion for influent TSS concentrations less than 20 mg/L; consequently, those sample pairs (influent and effluent) cannot be used for assessment of TSS removal performance. For influent concentration that exceed 200 mg/L, the treatment goal is an LCL95 of greater than an 80 percent reduction. Additionally, it must be shown that a statistically significant difference between influent and effluent concentrations exists. Finally, pollutant removals that meet the TAPE goals must be shown for sample pairs across a range of treated flow rates up to and including the design flow rate. This section describes the sampling results in relation to these criteria based on data from 24 events where influent concentrations were greater than 20 mg/L.

Before any performance analyses were conducted, the dataset was analyzed in relation to the different pre-filters that were installed during monitoring. Due to issues associated with the high clay content of the runoff, the pre-filter design had to be altered during the course of the monitoring project. This resulted in samples being collected with four different types of pre-filters: solid BioMediaGREEN, ribbed BioMediaGREEN, perlite, and finally cubed BioMediaGREEN. The manufacturer plans to use cubed BioMediaGREEN for all future MWS installations; consequently, a statistical test was run to indicate if the cubed BioMediaGREEN performed differently than the other pre-filters. Specifically, a Mann-Whitney U-test was run on the 16 TSS percent removal results collected with the cubed BioMediaGREEN versus the 8 collected with the other pre-filter configurations. The test indicated that there was no significant difference between the datasets (p = 0.110). Consequently, the data collected under all prefilter configurations were combined for use in the following analyses.

A one-tailed Wilcoxon signed-rank test performed on the total suspended solids data with influent concentrations $\geq 20 \text{ mg/L}$ (n = 24) indicated there was a statistically significant (p < 0.001) decrease in effluent total suspended solids concentrations compared to influent total suspended solids concentrations. Consequently, this aspect of the Basic Treatment criteria for TAPE was met.

The majority of the samples collected at AMWS had influent concentrations below 100 mg/L (Table 8). Of the 28 sampled events, 17 had influent concentrations between 20 and 100 mg/L. The UCL95 mean concentration for these 17 samples was 12.8 mg/L, which is below the 20 mg/L threshold and consequently these samples also show the Basic Treatment criteria for TAPE was met.

Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c
4/15/2012 22:45	26		2.8			7
4/17/2012 21:20	100		2.3		98	13
4/19/2012 8:30	46		4.8			6
4/25/2012 20:50	20		3.2			10
5/2/2012 21:50	32		3			15
5/21/2012 4:45	70		12			22
10/14/2012 19:15	26		7.4			28
10/15/2012 12:30	67		17			28
10/28/2012 6:15	22		4.1			28
10/29/2012 22:45	57		12			23
10/31/2012 5:25	30		11			6
11/23/2012 8:25	6.5		1.7			19
11/29/2012 6:15	34.2		16			10
12/2/2012 14:10	6.7		2.6			5
12/3/2012 22:30	22.8		5.7			11
12/11/2012 11:20	6.7		5			19
12/19/2012 2:10	48.7		5.5			17
1/23/2013 12:15	42		26.7			6
1/24/2013 17:50	41.2		14.3			8
2/22/2013 9:30 ^a	339		132		61	40
3/19/2013 15:35 ^a	209		47		78	28
4/4/2013 8:00	145	J	19		87	3
4/6/2013 16:45	12		2.1			11
4/10/2013 8:50	153		17		89	13
4/18/2013 20:45	20.6		2.6			9
4/29/2013 3:15	186		21		89	20
5/16/2013 12:15 ^a	251		20.8		92	50
5/21/2013 11:15 ^a	79		20.5			28
Minimum	6.5		1.7		61	3
UCL95 Mean ^d			12.8			



	Table 8 (continued).Total Suspended Solids Concentrations and Removal EfficiencyEstimates for Valid Sampling Events at the AMWS Test System.										
Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c					
Mean	75.0		15.7		84.9	17.3					
LCL95 Mean ^e											
Maximum	339		132		98	50					

^a All sampled events were flow-weighted composite sampled except these events, which consisted of samples collected above a high flow rate threshold

^b Percent removal is only calculated for sample pairs with influent \geq 100 mg/L.

^c Sampled flow rate is calculated by averaging the flow rate associated with each aliquot in the composite sample.

^d Bootstrapped estimate of the upper 95% confidence limit of the mean. Only calculated for effluent concentration with influent between 20 and 100 mg/L per the TAPE (Ecology 2011).

^e Bootstrapped estimate of the lower 95% confidence limit of the mean. Only calculated for percent removal when influent ≥100 mg/L per the TAPE (Ecology 2011). Not calculated for this data set because n value was too low for bootstrap procedure.

Bold values met influent screening criteria and were used in performance analyses.

J = estimated value based on water quality data (Appendix E) gpm = gallons/minute

mg/L = milligram/liter

Seven of the sampled events were characterized by influent concentrations greater than 100 mg/L, with two events exceeding 200 mg/L (Table 8). The mean TSS removal for these events was 84.9 percent (above the 80 percent reduction criteria). An LCL95 mean removal was not calculable since at least 10 samples are required for a bootstrap analysis. However, these samples were used in the assessment of removal efficiency at various treatment flow rates.

To determine with what flow rates the TSS removals were associated, the flow rate at the point when each aliquot was collected was calculated. These flow rates were then averaged for each sampled event. As shown in Table 8, these results indicate the mean sampled treated flow rate was 17.3 gpm. As described in the *Test System Sizing* section above, the design flow rate for the system is 41 gpm. Figure 12 displays percent removal versus average treated flow rate for all of the 24 qualifying TSS sample pairs. For reference, the open blue dots on the figure are sample pairs with influent less than 100 mg/L while the solid red dots are sample pairs with influent TSS greater than or equal to 100 mg/L. The TAPE (Ecology 2011) indicates that a regression analysis should be conducted to determine the treatment efficiency varies as function of treated flow rate. The results of the regression analysis indicated there is no significant relationship between treatment efficiency and treated flow rate (p = 0.822).

Visual examinations of the relationship between treatment efficiency and treated flow rate in Figure 12 highlight the anomalous results from the February 22, 2013, event. As indicated in the *Particle Size Distribution* section above, the influent sample for this event was characterized by 47 percent suspended clay, 21 percent more clay than the average for the site. This may explain why the TSS removal for this sample pair was so low. If this data point is removed, it is clear that the TSS removal is above 80 percent up to and through the design flow rate of 41 gpm.

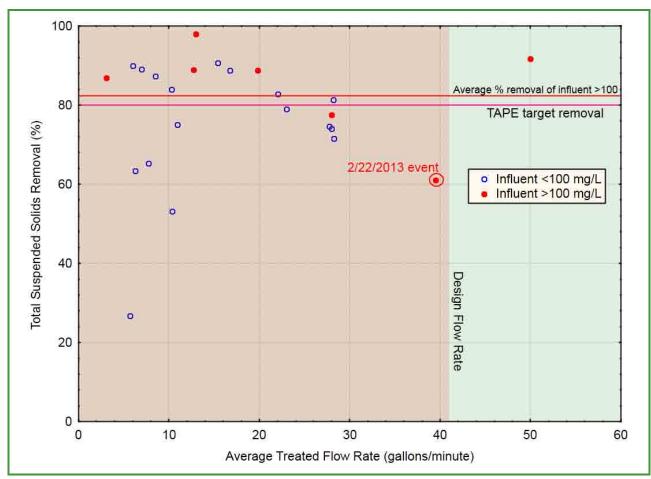


Figure 12. TSS Removal (%) as a Function of Average Treated Flow Rate.

Taken together, the above analyses indicate that the Basic Treatment criteria were met based on the data collected at the AMWS test site.

Phosphorus Treatment

The phosphorus treatment goal listed in the TAPE guidelines indicates that the LCL95 of the mean removal must be greater than or equal to 50 percent for influent total phosphorus (TP) concentrations ranging from 0.1 to 0.5 mg/L. In addition, it must be shown that a statistically significant difference between influent and effluent concentrations exists. Finally, pollutant removals that meet the TAPE goals must be shown for sample pairs across a range of treated flow rates up to and including the design flow rate. This section describes the sampling results in relation to this criterion based on data from 19 events where influent concentrations were within the specified target range.

Before any performance analyses were conducted, the dataset was analyzed in relation to the pre-filters that were installed during monitoring. Specifically, a Mann-Whitney U-test was run on the 12 qualifying TP percent removal results collected with the cubed BioMediaGREEN versus the 7 collected with the other pre-filter configurations. The test indicated that there was no significant difference between the datasets (p = 0.482). Consequently, the data collected under all prefilter configurations were combined for use in the following analyses.

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It should also be noted that one of the data points used in the analyses presented herein is an orthophosphorus result instead of a TP result. A high flow rate sample was collected on May 16, 2013, but the sample was mistakenly not analyzed for TP. Orthophosphorus was used in lieu of TP for this event, which is a conservative approach as orthophosphorus is more difficult to treat than TP. This substitution was approved be Ecology in a meeting held on June 5, 2013.

A one-tailed Wilcoxon signed-rank test performed on the TP data with influent concentrations from 0.1 to 0.5 mg/L (n = 19) indicated there was a statistically significant (p < 0.001) decrease in effluent TP concentrations compared to influent concentrations. Consequently, this aspect of the Phosphorus Treatment criteria for TAPE was met.

The LCL95 mean percent reduction for the 19 gualifying TP sample pairs was 61.7 percent (Table 9), which is above the goal of \geq 50 percent; consequently, these samples also show the Phosphorus Treatment criteria for TAPE was met.

To determine with what flow rates the TP removals were associated, the flow rate at the point when each aliquot was collected was calculated. These flow rates were then averaged for each sampled event. As shown in Table 9, these results indicate the mean sampled treated flow rate was 17.3 gpm. As described in the *Test System Sizing* section above, the design flow rate for the system is 41 gpm. Figure 13 displays percent removal versus average treated flow rate for all of the 19 qualifying TP sample pairs. Figure 13 indicates the high flow rate orthophosphorus result as well as all of the qualifying TP results. As is apparent, only one result fell below the 50 percent reduction threshold.

The results of the regression analysis on the percent removal versus flow rate data indicated there is no significant linear relationship between these variables (p = 0.834). A visual assessment of the data in Figure 13 also indicate treatment efficiency greater than 50 percent is evident up to and through the design flow rate; therefore, it can be safely assumed that the system can reduce TP by greater than 50 percent at the design flow rate of 41 gpm.

Taken together, the above analyses indicate that the Phosphorus Treatment criteria were met based on the data collected at the AMWS test site.

Enhanced Treatment

The TAPE enhanced treatment criteria indicate that the LCL95 of the mean dissolved zinc removal must be greater than 60 percent for influent concentrations ranging from 0.02 to 0.3 mg/L. In addition, the LCL95 of the mean dissolved copper removal must be greater than 30 percent for influent concentrations ranging from 0.005 to 0.02 mg/L. In addition, it must be shown that a statistically significant difference between influent and effluent concentrations exists. Finally, pollutant removals that meet the TAPE goals must be shown for sample pairs across a range of treated flow rates up to and including the design flow rate. Separate subsections below describe the sampling results in relation to these criteria based on data from 11 and 14 events where influent concentrations were within the specified ranges for dissolved zinc and copper, respectively.

Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c
4/15/2012 22:45	0.092		0.026		72	7
4/17/2012 21:20	0.14	J	0.02	U	86	13
4/19/2012 8:30	0.087	J	0.1	U		6
4/25/2012 20:50	0.15		0.062		59	10
5/2/2012 21:50	0.090		0.038		58	15
5/21/2012 4:45	0.18		0.062		66	22
10/14/2012 19:15	0.18		0.079		56	28
10/15/2012 12:30	0.098		0.01		90	28
10/28/2012 6:15	0.066		0.039			28
10/29/2012 22:45	0.13		0.041		68	23
10/31/2012 5:25	0.1		0.039		61	6
11/23/2012 8:25	0.026		0.1	U		19
11/29/2012 6:15	0.093		0.036		61	10
12/2/2012 14:10	0.027		0.01			5
12/3/2012 22:30	0.075		0.023			11
12/11/2012 11:20	0.257		0.054		79	19
12/19/2012 2:10	0.073		0.025			17
1/23/2013 12:15	0.103		0.083		19	6
1/24/2013 17:50	0.098		0.039		60	8
2/22/2013 9:30 ^a	0.56		0.26		54	40
3/19/2013 15:35 ^a	0.398		0.13		67	28
4/4/2013 8:00	2.15	J	0.4		81	3
4/6/2013 16:45	0.165		0.041		75	11
4/10/2013 8:50						13
4/18/2013 20:45						9
4/29/2013 3:15						20
5/16/2013 12:15 ^a	0.114 ^f		0.05 ^f		56 ^f	50
5/21/2013 11:15 ^a	0.212		0.1		53	28
Minimum	0.026		0.01		19	3
UCL95 Mean ^d						
Mean	0.227		0.074		64.3	17.3



	Table 9 (continued).Total Phosphorus Concentrations and Removal EfficiencyEstimates for Valid Sampling Events at the AMWS Test System.								
Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c			
LCL95 Mean ^e					61.7				
Maximum	2.15		0.4		90	50			

All sampled events were flow-weighted composite sampled except these events, which consisted of samples а collected above a high flow rate threshold.

b Percent removal is only calculated for sample pairs with influent $\ge 0.1 \text{ mg/L}$.

с Sampled flow rate is calculated by averaging the flow rate associated with each aliquot in the composite sample.

d Bootstrapped estimate of the upper 95% confidence limit of the mean. Only calculated for TSS effluent concentrations.

Bootstrapped estimate of the lower 95% confidence limit of the mean. Used to compare to the TAPE TP criteria of at least 50 percent removal.

f Orthophosphorus results used in lieu of TP results for this event (due to missing TP data).

Bold values met influent screening criteria and were used in performance analyses

J = estimated value based on water quality data (Appendix E)

U = result at or below the reporting limitgpm = gallons/minute

mg/L = milligram/liter

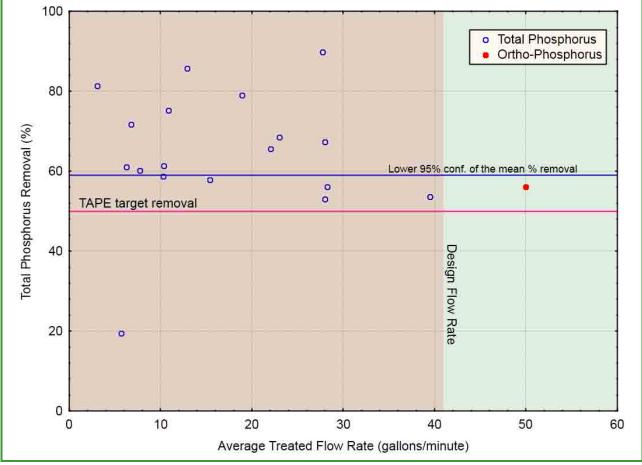


Figure 13. TP Removal (%) as a Function of Average Treated Flow Rate.

Dissolved Zinc Treatment

Before any performance analyses were conducted, the dissolved zinc dataset was analyzed in relation to the pre-filters, which were installed during monitoring. Specifically, a Mann-Whitney U-test was run on the 11 qualifying dissolved zinc percent removal results collected with the cubed BioMediaGREEN versus the 7 collected with the other pre-filter configurations. The test indicated that there was a significant difference between the datasets (p = 0.004). Consequently, only the data collected when the cubed BioMediaGREEN was installed were used in the final assessment. This results in a dataset with only 11 qualifying events. The TAPE indicates that 12 events are required. However, based on conversations with Douglas Howie of Ecology (June 5, 2013) and due to the challenging site conditions, 11 events was deemed adequate for this TER.

A one-tailed Wilcoxon signed-rank test performed on the dissolved zinc data with influent concentrations from 0.02 to 0.3 mg/L (n = 11) indicated there was a statistically significant (p < 0.001) decrease in effluent dissolved zinc concentrations compared to influent concentrations. Consequently, this aspect of the Enhanced Treatment criteria for TAPE was met.

The LCL95 mean percent reduction for the 11 qualifying dissolved zinc sample pairs was 60.5 percent (Table 10), which is above the goal of \geq 60 percent; consequently, these samples also show the Enhanced Treatment criteria for TAPE was met.

To determine what flow rates were associated with the dissolved zinc removals, the flow rate was calculated at the point when each aliquot was collected. These flow rates were averaged for each sampled event. As shown in Table 10, these results indicate the mean sampled treated flow rate was 17.3 gpm. As described in the *Test System Sizing* section above, the design flow rate for the system is 41 gpm. Figure 14 displays percent removal versus average treated flow rate for all of the 11 qualifying dissolved zinc sample pairs (closed red dots). Figure 14 indicates the results from when the other pre-filters were installed (open blue circles) for reference purposes only. As is apparent, only three results from when the cubed BioMediaGREEN was installed fell below the 50 percent reduction threshold. These three results occurred at lower sampled flow rates. Closer to and through the design flow rate, the percent reduction results exceed 60 percent. The results of the regression analysis on the percent removal versus flow rate data also indicated there is no significant relationship between these variables (p = 0.707). Therefore, it can be safely assumed that the system can reduce dissolved zinc by greater than 60 percent at the design flow rate of 41 gpm.

Taken together, the above analyses indicate that the Enhanced treatment criterion for dissolved zinc in TAPE was met based on the data collected at the AMWS test site.



Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c
4/15/2012 22:45	0.029		0.02		31 (NA)	7
4/17/2012 21:20	0.020		0.011		45 (NA)	13
4/19/2012 8:30	0.011		0.01	U		6
4/25/2012 20:50	0.060		0.056		7 (NA)	10
5/2/2012 21:50	0.022		0.012		45 (NA)	15
5/21/2012 4:45	0.06		0.033		45 (NA)	22
10/14/2012 19:15	0.031		0.012		61 (NA)	28
10/15/2012 12:30	0.022		0.011		50 (NA)	28
10/28/2012 6:15	0.015		0.0046			28
10/29/2012 22:45	0.020		0.0074		63	23
10/31/2012 5:25	0.015		0.0068			6
11/23/2012 8:25	0.0107		0.0034			19
11/29/2012 6:15	0.0108		0.0099			10
12/2/2012 14:10	0.0148		0.006			5
12/3/2012 22:30	0.013		0.0109			11
12/11/2012 11:20	0.045		0.0133		70	19
12/19/2012 2:10	0.0314		0.0072		77	17
1/23/2013 12:15	0.0156		0.0076			6
1/24/2013 17:50	0.0198		0.0069		65	8
2/22/2013 9:30 ^a	0.0022		0.0060			40
3/19/2013 15:35 ^a	0.0104		0.0122			28
4/4/2013 8:00	0.352		0.1940		45	3
4/6/2013 16:45	0.0338		0.0156		54	11
4/10/2013 8:50	0.152		0.0652		57	13
4/18/2013 20:45	0.299		0.0312		90	9
4/29/2013 3:15	0.315		0.0610		81	20
5/16/2013 12:15 ^a	0.0715		0.0238		67	50
5/21/2013 11:15 ^a	0.0349		0.0136		61	28
Minimum	0.0022		0.0034		45	3
UCL95 Mean ^d						
Mean	0.0620		0.0240		66.3	17.3

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Table 10 (continued).Dissolved Zinc Concentrations and Removal Efficiency Estimatesfor Valid Sampling Events at the AMWS Test System.								
Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c		
LCL95 Mean ^e					60.5			
Maximum	0.3520		0.1940		90	50		

а All sampled events were flow-weighted composite sampled except these events, which consisted of samples collected above a high flow rate threshold.

b Percent removal is only calculated for sample pairs with influent $\ge 0.02 \text{ mg/L}$.

с Sampled flow rate is calculated by averaging the flow rate associated with each aliquot in the composite sample.

d Bootstrapped estimate of the upper 95% confidence limit of the mean. Only calculated for TSS effluent concentrations.

е Bootstrapped estimate of the lower 95% confidence limit of the mean. Used to compare to the TAPE dissolved zinc criteria of at least 60 percent removal.

Bold values met influent screening criteria and were used in performance analyses

NA = not applicable. Percent reduction results are associated with pre-filters which performed statistically worse than the cubed BioMediaGREEN. These results were not used in the final analysis. U = result at or below the reporting limit

gpm = gallons/minute

mg/L = milligram/liter

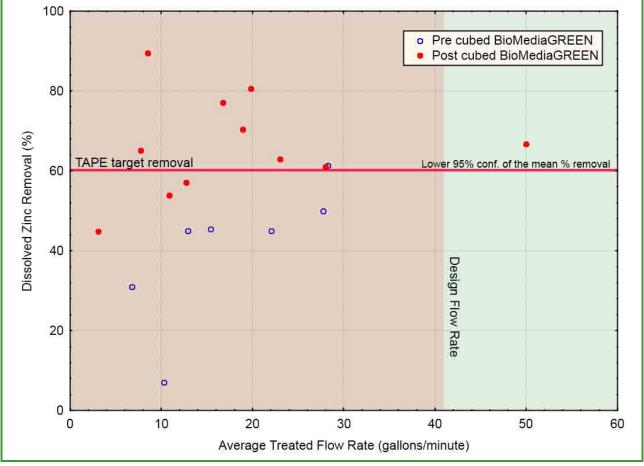


Figure 14. Dissolved Zinc Removal (%) as a Function of Average Treated Flow Rate.

Dissolved Copper Treatment

Before any performance analyses were conducted, the dissolved copper dataset was analyzed in relation to the pre-filters, which were installed during monitoring. Specifically, a Mann-Whitney U-test was run on the nine qualifying dissolved copper percent removal results collected with the cubed BioMediaGREEN versus the five collected with the other pre-filter configurations. The test indicated that there was no significant difference between the datasets (p = 0.797). Consequently, the data collected under all prefilter configurations were combined for use in the following analyses.

A one-tailed Wilcoxon signed-rank test performed on the dissolved copper data with influent concentrations from 0.005 to 0.02 mg/L (n = 14) indicated there was a statistically significant (p < 0.001) decrease in effluent dissolved copper concentrations compared to influent concentrations. Consequently, this aspect of the Enhanced Treatment criteria for dissolved copper in TAPE was met.

The LCL95 mean percent reduction for the 14 qualifying dissolved copper sample pairs was 32.5 percent (Table 11), which is above the goal of \geq 30 percent; consequently, these samples also show the Enhanced Treatment criterion for dissolved copper in TAPE was met.

To determine with flow rates were associated with dissolved copper removals, the flow rate at the point when each aliguot was collected was calculated. These flow rates were then averaged for each sampled event. As shown in Table 11, these results indicate the mean sampled treated flow rate was 17.3 gpm. As described in the Test System Sizing section above, the design flow rate for the system is 41 gpm. Figure 15 displays percent removal versus average treated flow rate for all of the 14 qualifying dissolved copper sample pairs (open blue circles). In addition, a data point from lab data collected in 2007 is included as a high flow rate reference point (red closed dot). The lab study data are summarized in the CULD application for the Modular Wetland System (Herrera 2011a). The TAPE indicates that lab data can be used to augment field data when determining performance at different flow rates.

The results of the regression analysis on the percent removal versus flow rate data indicated there is no significant relationship between these variables (p = 0.079); a visual assessment of the data in Figure 15 also show treatment above the TAPE target of 30 percent removal is evident until approximately 28 gpm. However, when the lab data point is included in the assessment, it is evident that the system (under less adverse conditions) can treat at a much higher efficiency at the design flow rate of 41 gpm. Given this, and considering the challenging site conditions at the Albina Maintenance Facility, we propose that Ecology grant dissolved copper removal certification at 41 gpm.

Taken together, the above analyses indicate that the Enhanced Treatment criteria for dissolved copper in TAPE was met. The flow rate at which dissolved copper is approved needs to be investigated further, but we propose 41 gpm because lab data indicate there is high removal at that flow rate.

Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c
4/15/2012 22:45	0.0053		0.0027		49	7
4/17/2012 21:20	0.0026		0.002	U		13
4/19/2012 8:30	0.0021		0.002	U		6
4/25/2012 20:50	0.011		0.0073		34	10
5/2/2012 21:50	0.0025		0.0021			15
5/21/2012 4:45	0.0066		0.0038		42	22
10/14/2012 19:15	0.0057		0.0043		25	28
10/15/2012 12:30	0.0049		0.0034		31	28
10/28/2012 6:15	0.0018		0.0016			28
10/29/2012 22:45	0.0028		0.0021			23
10/31/2012 5:25	0.0018		0.0011			6
11/23/2012 8:25	0.0012		0.0016			19
11/29/2012 6:15	0.0027		0.0019			10
12/2/2012 14:10	0.0032		0.0046			5
12/3/2012 22:30	0.0024		0.0028			11
12/11/2012 11:20	0.0051		0.0024		53	19
12/19/2012 2:10	0.001		0.0009			17
1/23/2013 12:15	0.0041	J	0.0035			6
1/24/2013 17:50	0.0117		0.0053		54	8
2/22/2013 9:30 ^a	0.0025		0.0024			40
3/19/2013 15:35 ^a	0.0026		0.0022			28
4/4/2013 8:00	0.034	J	0.0275		19	3
4/6/2013 16:45	0.0144		0.0086		40	11
4/10/2013 8:50	0.0205		0.0090		56	13
4/18/2013 20:45	0.0225		0.0090		60	9
4/29/2013 3:15	0.0471		0.0354		25	20
5/16/2013 12:15 ^a	0.012		0.0093		23	50
5/21/2013 11:15 ^a	0.0076		0.0056		26	28
Minimum	0.001		0.0009		19	3
UCL95 Mean ^d						



	Table 11 (continued).Dissolved Copper Concentrations and Removal EfficiencyEstimates for Valid Sampling Events at the AMWS Test System.									
Storm Start Date & Time	Influent Concentration (mg/L)	Qualifier	Effluent Concentration (mg/L)	Qualifier	Percent Removal ^b	Sampled Flow Rate (gpm) ^c				
Mean	0.0086		0.0059		38.3	17.3				
LCL95 Mean ^e					32.5					
Maximum	0.0471		0.0354		60	50				

а All sampled events were flow-weighted composite sampled except these events that consisted of samples collected above a high flow rate threshold.

b Percent removal is only calculated for sample pairs with influent ≥ 0.005 mg/L.

с Sampled flow rate is calculated by averaging the flow rate associated with each aliquot in the composite sample. d

Bootstrapped estimate of the upper 95% confidence limit of the mean. Only calculated for TSS effluent concentrations.

e Bootstrapped estimate of the lower 95% confidence limit of the mean. Used to compare to the TAPE dissolved copper criteria of at least 30 percent removal.

Bold values met influent screening criteria and were used in performance analyses

J = estimated value based on water quality data (Appendix E)

U = result at or below the reporting limit

gpm = gallons/minute

mg/L = milligram/liter

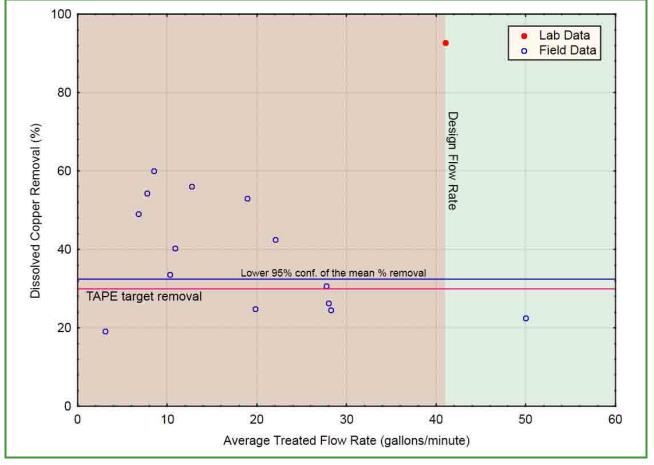


Figure 15. Dissolved Copper Removal (%) as a Function of Average Treated Flow Rate.

Other Parameters

The TAPE (Ecology 2011)indicates that in addition to required parameters mentioned above, screening parameters should be analyzed. The screening parameters consist of hardness, pH, and orthophosphate. The results for these parameters are presented in Table 12. The AMWS system had a negligible effect on hardness and pH. The average hardness concentrations were 37.6 and 40.6 mg $CaCO_3/L$ at the inlet and outlet, respectively. The average pH concentrations were 7.6 and 7.5 at the inlet and outlet, respectively. TAPE guidelines indicate that the test system should not increase of decrease pH by more than one unit for any given event or export concentration less than 4 or greater than 9. The pH data presented in Table 12 indicate that these conditions were met for each sampled event.

The orthophosphorus data indicated that the AMWS system reduced orthophosphorus by 67 percent, on average. When compared with other treatment systems (Herrera 2006, 2009, 2010, 2011c), this is a relatively high orthophosphorus removal rate.



		-	Table 12. Su	mma	ry Results for	Scre	ening Parame	eters.				
Storm Start Date & Time	Influent Hardness (mg CaCO₃ /L)	QA	Effluent Hardness (mg CaCO₃ /L)	QA	Influent pH (std. units)	QA	Effluent pH (std. units)	QA	Influent ortho-P (std. units)	QA	Effluent ortho-P (std. units)	QA
4/15/2012 22:45	31		43		7.53		6.17		0.01		0.01	U
4/17/2012 21:20	37		51		7.54		7.51		0.01	U	0.01	U
4/19/2012 8:30	26		33		7.46		7.41		0.01	U	0.01	U
4/25/2012 20:50	39		48		7.51		7.54		0.069		0.024	
5/2/2012 21:50	26		31		7.4		7.29		0.016		0.01	U
5/21/2012 4:45	37		44		7.48		7.45		0.047		0.013	
10/14/2012 19:15	30		48		7.13		6.82		0.073		0.05	U
10/15/2012 12:30	35		42		7.3		7.2		0.059		0.08	
10/28/2012 6:15	29		31		7.57		7.45		0.05	н	0.05	UH
10/29/2012 22:45	35		35		7.41		7.36		0.05	U	0.05	U
10/31/2012 5:25	45		46		7.52		7.56		0.05	U	0.05	U
11/23/2012 8:25					7.29	J	7.41	J				
11/29/2012 6:15	33.2		30.4		7.74		7.32		0.05	U	0.05	U
12/2/2012 14:10	29.2		30		7.15		7.19		0.05	U	0.05	U
12/3/2012 22:30									0.05	U	0.05	U
12/11/2012 11:20	27.2		29.6		7.88	J	7.92	J	0.05	U	0.05	U
12/19/2012 2:10	19.6		25.2		7.86		7.71		0.05	U	0.05	U
1/23/2013 12:15	40		41.2		8.06		7.72		0.05	U	0.05	U
1/24/2013 17:50	38		34.8		7.71		7.81		0.05	U	0.05	U
2/22/2013 9:30 ^a	62.8		50.8		8.84		8.14		0.05	U	0.05	U
3/19/2013 15:35 ^a	36.8		39.2		7.86		7.77		0.05	U	0.05	U



	Та	able 1	2 (continued). S	ummary Res	ults fo	or Screening I	Param	eters.			
Storm Start Date & Time	Influent Hardness (mg CaCO ₃ /L)	QA	Effluent Hardness (mg CaCO ₃ /L)	QA	Influent pH (std. units)	QA	Effluent pH (std. units)	QA	Influent ortho-P (std. units)	QA	Effluent ortho-P (std. units)	QA
4/4/2013 8:00	76		58.8		7.09	J	7.69	J	0.96		0.199	
4/6/2013 16:45	36		38.4		7.67		6.96		0.123		0.05	U
4/10/2013 8:50	43.2		41.6		7.83		8.13		0.426		0.05	U
4/18/2013 20:45	48		47.2		7.66		7.69		0.06		0.05	U
4/29/2013 3:15	42.4		47.6		7.33		7.52		0.156		0.05	U
5/16/2013 12:15 ^a	47.2		53.2		7.32		7.41		0.114		0.05	U
5/21/2013 11:15 ^a	28.4		34.4		7.65	J	7.57	J	0.062		0.05	U
Minimum	19.6		25.2		7.09		6.17		0.01	υ	0.01	U
Mean	37.6		40.6		7.6		7.5		0.093		0.031	
Maximum	76		58.8		8.84		8.14		0.960		0.199	

^a All sampled events were flow-weighted composite sampled except these events, which consisted of samples collected above a high flow rate threshold. Ortho-P = Orthophosphorus

J = estimated value based on water quality data (Appendix E)

QA = quality assurance



CONCLUSIONS

To obtain performance data to support the issuance of a GULD for the Modular Wetland System - Linear stormwater filtration system, Herrera conducted hydrologic and water quality monitoring at a test system in Portland, Oregon from April 14, 2012, to May 31, 2013. During this monitoring period, 28 separate storm events were sampled.

Of the 28 sampled events, 24 qualified for total suspended solids analysis. The data were segregated into sample pairs with influent concentration greater than and less than 100 mg/L. The UCL95 mean effluent concentration for the data with influent less than 100 mg/L was 12.8 mg/L, below the 20 mg/L threshold. In addition, the system exhibited TSS removal greater than 80 percent at flow rates up to and including the design flow rate of 41 gpm. Based on these results we recommend the system be granted Basic Treatment certification at 41 gpm (equivalent to 1 gpm/ft² of media).

Nineteen of the 28 sampled events qualified for total phosphorus analysis. The LCL95 mean percent removal was 61.7, well above the TAPE goal of 50 percent. Treatment above 50 percent was evident at flow rates up to and including the design flow rate of 41 gpm. Consequently, the MWS-Linear met the Phosphorus Treatment criterion for TAPE at the design flow rate.

Eleven of the 28 sampled events qualified for assessment for dissolved zinc removal. The LCL95 mean removal was 60.5 percent while the TAPE goal is greater than 60 percent removal. Treatment above 60 percent was evident at flow rates up to and including the design flow rate of 41 gpm. Consequently, the MWS-Linear met the Enhanced Treatment criterion specified for dissolved zinc in TAPE at the design flow rate.

Fourteen of the 28 sampled events qualified for assessment for dissolved copper removal. The LCL95 mean removal was 32.5 percent while the TAPE goal is greater than 30 percent removal. Treatment above 30 percent was evident at flow rates up to 28 gpm. When lab data are used to augment the dataset, the results indicate the MWS Linear met the Enhanced Treatment criterion specified for dissolved copper in TAPE at flow rates up to and including the design flow rate of 41 gpm.



REFERENCES

APHA, AWWA, and WEF. 1992. Standard Methods for the Examination of Water and Wastewater. 18th edition. Edited by A. Greenberg, A.D. Eaton, and L. Clesceri. American Public Health Association, American Water Works Association, Water Environment Federation, Washington, D.C.

APHA, AWWA, and WEF. 1998. Standard Methods for the Examination of Water and Wastewater. 20th edition. Edited by A. Greenberg, A.D. Eaton, and L. Clesceri. American Public Health Association, American Water Works Association, Water Environment Federation, Washington, D.C.

Davison, A.C. and D.V. Hinkley. 1997. Bootstrap Methods and Their Application. Cambridge University Press, Cambridge; New York.

Ecology. 2004. Stormwater Management Manual for Eastern Washington. Washington State Department of Ecology, Olympia, Washington.

Ecology. 2011. Technical Guidance for Evaluating Emerging Stormwater Treatment Technologies: Technology Assessment Protocol - Ecology (Tape). Publication No. 11-10-061, Washington State Department of Ecology, Olympia, Washington.

Ecology. 2012. 2012 Stormwater Management Manual for Western Washington: Volume III -Hydrologic Analysis and Flow Control Design/BMPs. Washington State Department of Ecology, Olympia, Washington.

Helsel, D.R. and R.M. Hirsch. 2002. Statistical Methods in Water Resources. Elsevier, Amsterdam.

Herrera. 2006. Technology Evaluation and Engineering Report: WSDOT Ecology Embankment. Prepared for Washington Department of Transportation by Herrera Environmental Consultants, Inc., Seattle, Washington.

Herrera. 2009. Technical Evaluation Report: Filterra Bioretention Filtration System Performance Monitoring. Prepared for Americast, Inc., by Herrera Environmental Consultants, Inc., Seattle, Washington.

Herrera. 2010. Technical Evaluation Report: Kristar Perk Filter Stormwater Treatment System Performance Monitoring. Prepared for KriStar Enterprises, Inc., by Herrera Environmental Consultants, Inc., Seattle, Washington.

Herrera. 2011a. Application for Conditional Use Level Designation: Modular Wetland System -Linear Stormwater Filtration System. Prepared for Modular Wetland Systems, Inc., by Herrera Environmental Consultants, Inc., Seattle, Washington.

Herrera. 2011b. Quality Assurance Project Plan: Modular Wetland System - Linear Treatment System Performance Monitoring Project. Prepared for Modular Wetland Systems, Inc., by Herrera Environmental Consultants, Inc., Seattle, Washington.

Herrera. 2011c. Technical Evaluation Report: Compost-Amended Biofiltration Swale Evaluation. Prepared for Washington Department of Transportation, by Herrera Environmental Consultants, Inc., Seattle, Washington.

Means, J. and R. Hinchee. 1994. Emerging Technology for Bioremediation of Metals. Battelle, Columbus, Ohio.

Reeves, R.D. and A.J.M. Baker. 2000. Metal-Accumulating Plants. In: I. Raskin and B. Ensley (Editors), Phytoremediation of Toxic Metals. John Wiley & Sons, New York, New York. pp. 193-230.

US EPA. 1983. Methods for Chemical Analysis of Water and Wastes. EPA 600/4-79-020, US Environmental Protection Agency, Environmental Monitoring and Support Laboratory, Washington, D.C.

US EPA. 1984. Guidelines Establishing Test Procedures for the Analysis of Pollutants under the Clean Water Act; Final Rule and Interim Final Rule. CFR Part 136. US Environmental Protection Agency, Washington, D.C.

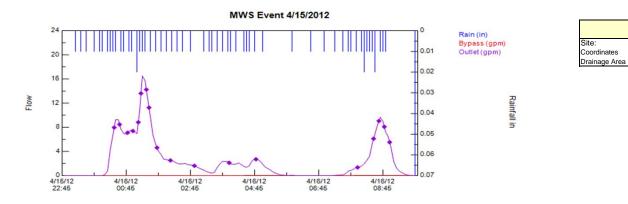
Walkowiak, D.K. (Editor), 2006. Isco Open Channel Flow Measurement Handbook. Teledyne Isco, Inc., Lincoln, Nebraska. 520 pp.



APPENDIX H

Individual Storm Reports





	Precipitation In	formation		
	Goal	Result	QA	Notes
Precipitation Total (in)	≥0.15	0.60		
Precipitation Duration (hr)	≥1	10.1		
Max Precip. Intensity (in/5 min)	NA	0.02		
Mean Precip. Intensity (in/hr)	0.03	0.06		
Antecedent Dry Period (hr)	≥6	51.4		

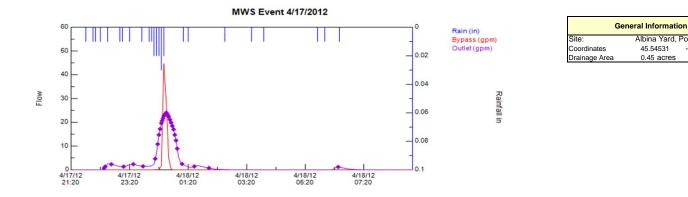
		Sampling	Informat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	18				
% Storm Sampled	≥75	92				
Sampling Duration (hr)	≤36	9				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	16.5		0.0		
Duration (hr)	NA	9.0		7.7		
Volume (gal)	NA	1594.9		10.6		

General Information

Albina Yard, Portland, OR 45.54531 -122.67559 0.45 acres

Т

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.09		0.03				72
Ortho-Phosphorus	mg/L	0.01		0.01	U			0
Hardness	mg/L	31.0		43.0				-38.7
Total Suspend Solids	mg/L	26.0		2.8				89
Total Kjedahl Nitrogen	mg/L	0.66		0.51				23
Nitrate + Nitrite	mg/L	0.17		0.13				23.5
pН	std units	7.53		6.17				18
Copper Total	ug/L	5.50		2.90				47
Copper Dissolved	ug/L	5.30		2.70				49
Lead Total	ug/L	4.10		1.00	U			76
Lead Dissolved	ug/L	0.30	J	0.35	J			-17
Zinc Total	ug/L	45.00		19.00				58
Zinc Dissolved	ug/L	29.00		20.00				31
Particle Size Distribution 1-2 µm	%	7.54		8.13				
Particle Size Distribution 2-5 µm	%	14.92		19.54				
Particle Size Distribution 5-15 µm	%	27.10		44.86				
Particle Size Distribution 15-25 µm	%	14.23		13.93				
Particle Size Distribution 25-50 µm	%	15.27		11.02				
Particle Size Distribution 50-100 µm	%	13.53		1.60				
Particle Size Distribution >100 µm	%	7.42		0.91				
Suspended Sediment Coarse	mg/L	11.9		3.8				68
Suspended Sediment Fine	mg/L	24.8		6.9				72
				ts - Grab				
	Units	IN	QA	OUT	QA	MDL	notes	-
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA



	Precipitation Inf	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.31			
Precipitation Duration (hr)	≥1	9.2			
Max Precip. Intensity (in/5 min)	NA	0.03			
Mean Precip. Intensity (in/hr)	0.03	0.03			
Antecedent Dry Period (hr)	≥6	36.8			

		Sampling	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	31				
% Storm Sampled	≥75	98				
Sampling Duration (hr)	≤36	8				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	24.1		44.6		
Duration (hr)	NA	10.7		3.5		
Volume (gal)	NA	1167.9		406.6		

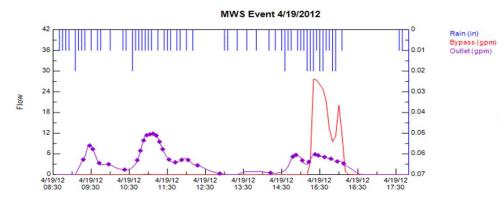
Albina Yard, Portland, OR 45.54531 -122.67559

1

0.45 acres

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.14		0.02	U			86
Ortho-Phosphorus	mg/L	0.01	U	0.01	U			0
Hardness	mg/L	37.0		51.0				-37.8
Total Suspend Solids	mg/L	100.0		2.3				98
Total Kjedahl Nitrogen	mg/L	1.40		0.50	U			64
Nitrate + Nitrite	mg/L	0.16		0.09				45.6
pH	std units	7.54		7.51				0
Copper Total	ug/L	2.60		2.20				15
Copper Dissolved	ug/L	2.60		2.00	U			23
Lead Total	ug/L	13.00		1.00	U			92
Lead Dissolved	ug/L	1.00	U	1.00	U			0
Zinc Total	ug/L	12.00		11.00				8
Zinc Dissolved	ug/L	20.00		10.00				50
Particle Size Distribution 1-2 µm	%	4.27		4.69				
Particle Size Distribution 2-5 µm	%	10.17		15.24				
Particle Size Distribution 5-15 µm	%	25.80		32.04				
Particle Size Distribution 15-25 µm	%	14.47		11.71				
Particle Size Distribution 25-50 µm	%	18.48		17.77				
Particle Size Distribution 50-100 µm	%	19.49		14.43				
Particle Size Distribution >100 µm	%	7.32		4.13				
Suspended Sediment Coarse	mg/L	53.3		1.4				97
Suspended Sediment Fine	mg/L	53.4		3.8				93
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

Rainfall in



Ge	eneral Information	on
Site:	Albina Yard,	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

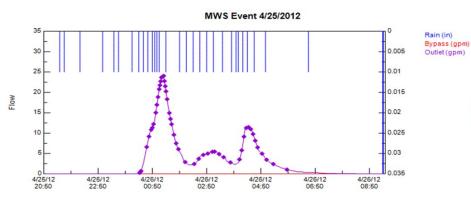
Т

	Precipitation Inf	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.68			
Precipitation Duration (hr)	≥1	9.3			
Max Precip. Intensity (in/5 min)	NA	0.02			
Mean Precip. Intensity (in/hr)	0.03	0.07			
Antecedent Dry Period (hr)	≥6	28.6			
					-

		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	32				
% Storm Sampled	≥75	95				
Sampling Duration (hr)	≤36	7				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	12.0		27.6		
Duration (hr)	NA	7.7		3.0		
Volume (gal)	NA	1498.7		990.7		

	Sa	ample Res	ults - Fl	ow Com	posite			
	Units	. IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.09	J	0.10	U			-15
Ortho-Phosphorus	mg/L	0.01	U	0.01	U			0
Hardness	mg/L	26.0		33.0				-26.9
Total Suspend Solids	mg/L	46.0		4.8				90
Total Kjedahl Nitrogen	mg/L	0.46		0.38				18
Nitrate + Nitrite	mg/L	0.08	J	0.07	J			16.5
pH	std units	7.46		7.41				1
Copper Total	ug/L	5.50		2.30				58
Copper Dissolved	ug/L	2.10		2.00	U			5
Lead Total	ug/L	6.60		1.00	U			85
Lead Dissolved	ug/L	1.00	U	1.00	U			0
Zinc Total	ug/L	46.00		10.00	U			78
Zinc Dissolved	ug/L	11.00		10.00	U			9
Particle Size Distribution 1-2 µm	%	10.45		15.52				
Particle Size Distribution 2-5 µm	%	15.58		26.34				
Particle Size Distribution 5-15 µm	%	25.65		38.14				
Particle Size Distribution 15-25 µm	%	12.78		13.49				
Particle Size Distribution 25-50 µm	%	18.21		5.83				
Particle Size Distribution 50-100 µm	%	12.70		0.26				
Particle Size Distribution >100 µm	%	4.61		0.42				
Suspended Sediment Coarse	mg/L	12.4		1.1				91
Suspended Sediment Fine	mg/L	39.9		7.3				82
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	11		4				64
E. Coli	MPN/100 ml	16		1				94
Total Petroleum Hydrocarbons -Diesel	mg/L	1.40		0.73				47.9
Total Petroleum Hydrocarbons -Oil	mg/L	1.50		0.60				60
Oil and Grease	mg/L	4.7	U	5.7	U			-21

Rainfall in



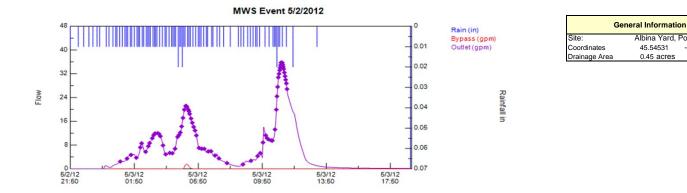
Ge	neral Informati	on
Site:	Albina Yard,	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

1

	Precipitation Inf	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.31			
Precipitation Duration (hr)	≥1	9.8			
Max Precip. Intensity (in/5 min)	NA	0.01			
Mean Precip. Intensity (in/hr)	0.03	0.03			
Antecedent Dry Period (hr)	≥6	13.0			

		Sampling	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	50				
% Storm Sampled	≥75	98				
Sampling Duration (hr)	≤36	5				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA r	notes
Max Discharge (gpm)	NA	24.1		0.0		
Duration (hr)	NA	9.2		5.3		
Volume (gal)	NA	2171.1		5.0		

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.15		0.06				59
Ortho-Phosphorus	mg/L	0.07		0.02				65
Hardness	mg/L	39.0		48.0				-23.1
Total Suspend Solids	mg/L	20.0		3.2				84
Total Kjedahl Nitrogen	mg/L	0.77		0.67				13
Nitrate + Nitrite	mg/L	0.37		0.35				5.4
pН	std units	7.51		7.54				0
Copper Total	ug/L	13.00		11.00				15
Copper Dissolved	ug/L	11.00		7.30				34
Lead Total	ug/L	5.60		2.60				54
Lead Dissolved	ug/L	2.70		2.30				15
Zinc Total	ug/L	73.00		56.00				23
Zinc Dissolved	ug/L	60.00		56.00				7
Particle Size Distribution 1-2 µm	%	4.84		11.42				
Particle Size Distribution 2-5 µm	%	13.43		33.18				
Particle Size Distribution 5-15 µm	%	29.33		42.22				
Particle Size Distribution 15-25 µm	%	15.49		8.24				
Particle Size Distribution 25-50 µm	%	22.86		3.77				
Particle Size Distribution 50-100 µm	%	12.63		1.18				
Particle Size Distribution >100 µm	%	1.43		0.10				
Suspended Sediment Coarse	mg/L	16.7		0.7				96
Suspended Sediment Fine	mg/L	14.0		5.5				61
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA



Goal	Result	QA	Notes
≥0.15	0.90		
≥1	15.4		
NA	0.02		
0.03	0.06		
≥6	29.8		
	≥0.15 ≥1 NA 0.03	≥0.15 0.90 ≥1 15.4 NA 0.02 0.03 0.06	≥0.15 0.90 ≥1 15.4 NA 0.02 0.03 0.06

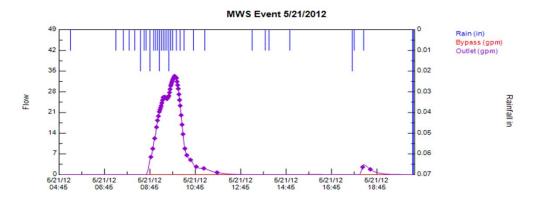
		Sampling I	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	75				
% Storm Sampled	≥75	81				
Sampling Duration (hr)	≤36	10				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	35.8		1.6		
Duration (hr)	NA	19.3		7.1		
Volume (gal)	NA	6570.0		39.0		

Albina Yard, Portland, OR 45.54531 -122.67559

1

0.45 acres

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.09		0.04				58
Ortho-Phosphorus	mg/L	0.02		0.01	U			38
Hardness	mg/L	26.0		31.0				-19.2
Total Suspend Solids	mg/L	32.0		3.0				91
Total Kjedahl Nitrogen	mg/L	0.73		0.51				30
Nitrate + Nitrite	mg/L	0.15		0.12				20.0
pH	std units	7.40		7.29				1
Copper Total	ug/L	5.20		2.30				56
Copper Dissolved	ug/L	2.50		2.10				16
Lead Total	ug/L	5.20		1.00	U			81
Lead Dissolved	ug/L	0.18	JF	0.25	JF			-39
Zinc Total	ug/L	38.00		12.00				68
Zinc Dissolved	ug/L	22.00		12.00				45
Particle Size Distribution 1-2 µm	%	10.08		8.86				
Particle Size Distribution 2-5 µm	%	14.38		19.80				
Particle Size Distribution 5-15 µm	%	27.27		44.74				
Particle Size Distribution 15-25 µm	%	14.50		14.19				
Particle Size Distribution 25-50 µm	%	18.50		10.19				
Particle Size Distribution 50-100 µm	%	11.50		2.23				
Particle Size Distribution >100 µm	%	3.76		0.00				
Suspended Sediment Coarse	mg/L	23.7		4.8				80
Suspended Sediment Fine	mg/L	33.9		2.0				94
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	1600	G	900				44
E. Coli	MPN/100 ml	770		490				36
Total Petroleum Hydrocarbons -Diesel	mg/L	1.10		0.46				58.2
Total Petroleum Hydrocarbons -Oil	mg/L	2.30		0.73				68
Oil and Grease	mg/L	5.6	U	5.8	U			-4



Ge	neral Informatio	on
Site:	Albina Yard, I	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

Т

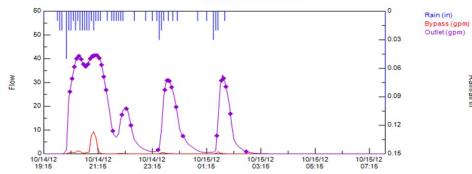
Precipitation Inf	ormation			
Goal	Result	QA	Notes	
≥0.15	0.38			
≥1	13.4			
NA	0.02			
0.03	0.03			
≥6	16.8			
	Goal ≥0.15 ≥1 NA 0.03	≥0.15 0.38 ≥1 13.4 NA 0.02 0.03 0.03	Goal Result QA ≥0.15 0.38 ≥1 13.4 NA 0.02 0.03 0.03	Goal Result QA Notes ≥0.15 0.38 ≥1 13.4 NA 0.02 0.03 0.03

		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	53				
% Storm Sampled	≥75	97				
Sampling Duration (hr)	≤36	10				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	33.3		0.0		
Duration (hr)	NA	8.8		0.0		
Volume (gal)	NA	2426.0		0.0		

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.18		0.06				66
Ortho-Phosphorus	mg/L	0.05		0.01				72
Hardness	mg/L	37.0		44.0				-18.9
Total Suspend Solids	mg/L	70.0		12.0				83
Total Kjedahl Nitrogen	mg/L	1.20		0.92				23
Nitrate + Nitrite	mg/L	0.74		0.57				23.0
рН	std units	7.48		7.45				0
Copper Total	ug/L	12.00		6.10				49
Copper Dissolved	ug/L	6.60		3.80				42
Lead Total	ug/L	12.00		3.10				74
Lead Dissolved	ug/L	2.20		1.30				41
Zinc Total	ug/L	92.00		34.00				63
Zinc Dissolved	ug/L	60.00		33.00				45
Particle Size Distribution 1-2 µm	%	7.08		3.03				
Particle Size Distribution 2-5 µm	%	22.92		7.35				
Particle Size Distribution 5-15 µm	%	44.34		23.49				
Particle Size Distribution 15-25 µm	%	12.98		14.96				
Particle Size Distribution 25-50 µm	%	7.72		22.39				
Particle Size Distribution 50-100 µm	%	4.31		20.44				
Particle Size Distribution >100 µm	%	0.66		8.33				
Suspended Sediment Coarse	mg/L	11.7		16.0				-37
Suspended Sediment Fine	mg/L	78.4		16.2				79
				ts - Grat				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

Rainfall in





Site:
Coordinates
Drainage Are

General Information

0.45 acres

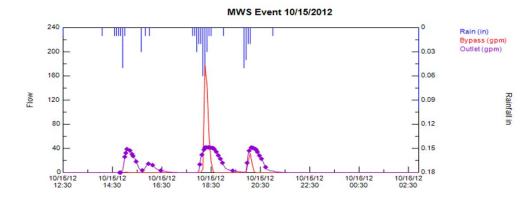
Albina Yard, Portland, OR 45.54531 -122.67559

1

	Precipitation In	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.65			
Precipitation Duration (hr)	≥1	6.7			
Max Precip. Intensity (in/5 min)	NA	0.05			
Mean Precip. Intensity (in/hr)	0.03	0.10			
Antecedent Dry Period (hr)	≥6	45.9			

		Sampling	Informat	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	35				
% Storm Sampled	≥75	97				
Sampling Duration (hr)	≤36	7				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	41.8		9.3		
Duration (hr)	NA	11.9		6.9		
Volume (gal)	NA	6308.7		189.6		

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.18	В	0.08	В			56
Ortho-Phosphorus	mg/L	0.07		0.05	U			32
Hardness	mg/L	30.0		48.0				-60.0
Total Suspend Solids	mg/L	26.0		7.4				72
Total Kjedahl Nitrogen	mg/L	0.75	J	0.53	J			29
Nitrate + Nitrite	mg/L	1.40		2.80				-100.0
pH	std units	7.13		6.82				4
Copper Total	ug/L	9.30		4.90				47
Copper Dissolved	ug/L	5.70		4.30				25
Lead Total	ug/L	4.60		0.95	J			79
Lead Dissolved	ug/L	0.13	J	0.11	J			15
Zinc Total	ug/L	53.00		14.00				74
Zinc Dissolved	ug/L	31.00		12.00				61
Particle Size Distribution 1-2 µm	%	3.54		8.02				
Particle Size Distribution 2-5 µm	%	12.67		24.35				
Particle Size Distribution 5-15 µm	%	27.25		43.35				
Particle Size Distribution 15-25 µm	%	11.47		14.23				
Particle Size Distribution 25-50 µm	%	13.62		8.53				
Particle Size Distribution 50-100 µm	%	18.83		0.83				
Particle Size Distribution >100 µm	%	12.62		0.68				
Suspended Sediment Coarse	mg/L	11.7		0.9				92
Suspended Sediment Fine	mg/L	31.8		11.8				63
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA



Ge	eneral Information	on
Site:	Albina Yard,	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

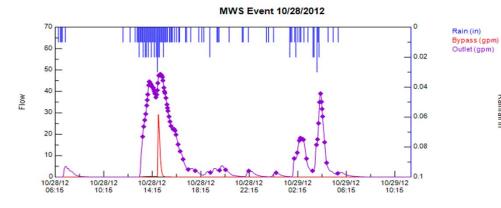
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	Precipitation Information									
	Goal	Result	QA	Notes						
Precipitation Total (in)	≥0.15	0.58								
Precipitation Duration (hr)	≥1	8.5								
Max Precip. Intensity (in/5 min)	NA	0.06								
Mean Precip. Intensity (in/hr)	0.03	0.07								
Antecedent Dry Period (hr)	≥6	10.9								

	Sampling Information							
	Goal	Result	QA	notes				
Number of Aliquots	≥10	39						
% Storm Sampled	≥75	98						
Sampling Duration (hr)	≤36	6						
		Flow Inf	ormatio	n				
	Goal	Treated	QA	Bypass	QA	notes		
Max Discharge (gpm)	NA	41.8		177.3				
Duration (hr)	NA	12.2		2.9				
Volume (gal)	NA	5209.6		2369.9				

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.10		0.01	ſ			90
Ortho-Phosphorus	mg/L	0.06		0.08				-36
Hardness	mg/L	35.0		42.0				-20.0
Total Suspend Solids	mg/L	67.0		17.0				75
Total Kjedahl Nitrogen	mg/L	0.66	J	0.55	J			17
Nitrate + Nitrite	mg/L	0.16		0.45				-181.3
рН	std units	7.30		7.20				1
Copper Total	ug/L	10.00		5.00				50
Copper Dissolved	ug/L	4.90		3.40				31
Lead Total	ug/L	9.10		3.20				65
Lead Dissolved	ug/L	0.14	J	0.14	J			0
Zinc Total	ug/L	76.00		26.00				66
Zinc Dissolved	ug/L	22.00		11.00				50
Particle Size Distribution 1-2 µm	%	3.45		5.05				
Particle Size Distribution 2-5 µm	%	9.51		13.92				
Particle Size Distribution 5-15 µm	%	22.94		32.83				
Particle Size Distribution 15-25 µm	%	10.78		14.94				
Particle Size Distribution 25-50 µm	%	17.86		13.75				
Particle Size Distribution 50-100 µm	%	16.77		15.05				
Particle Size Distribution >100 µm	%	18.70		4.45				
Suspended Sediment Coarse	mg/L	27.7		3.1				89
Suspended Sediment Fine	mg/L	63.0		30.3				52
				ts - Grab				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

Rainfall in



Ger	General Information										
Site:	Albina Yard,	Portland, OR									
Coordinates	45.54531	-122.67559									
Drainage Area	0.45 acres										

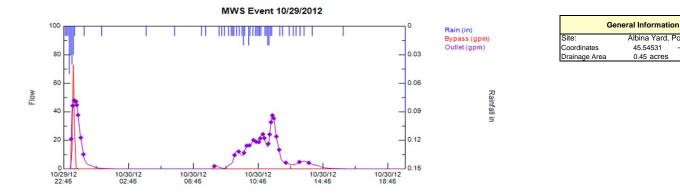
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	Precipitation Information									
	Goal	Result	QA	Notes						
Precipitation Total (in)	≥0.15	1.04								
Precipitation Duration (hr)	≥1	23.3								
Max Precip. Intensity (in/5 min)	NA	0.03								
Mean Precip. Intensity (in/hr)	0.03	0.05								
Antecedent Dry Period (hr)	≥6	10.0								

	Sampling Information							
	Goal	Result	QA	notes				
Number of Aliquots	≥10	74						
% Storm Sampled	≥75	95						
Sampling Duration (hr)	≤36	16						
		Flow Infe	ormatio	n				
	Goal	Treated	QA	Bypass	QA	notes		
Max Discharge (gpm)	NA	48.0		29.1				
Duration (hr)	NA	28.4		24.8				
Volume (gal)	NA	10302.0		399.4				

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.07		0.04	ſ			41
Ortho-Phosphorus	mg/L	0.05	Н	0.05	UH			0
Hardness	mg/L	29.0		31.0				-6.9
Total Suspend Solids	mg/L	22.0		4.1				81
Total Kjedahl Nitrogen	mg/L	0.40	J	0.50	J			-25
Nitrate + Nitrite	mg/L	0.06		0.13				-116.7
pH	std units	7.57		7.45				2
Copper Total	ug/L	3.70		2.30				38
Copper Dissolved	ug/L	1.80	J	1.60	J			11
Lead Total	ug/L	3.50		0.64	J			82
Lead Dissolved	ug/L	1.00	U	1.00	U			0
Zinc Total	ug/L	28.00		6.90	J			75
Zinc Dissolved	ug/L	15.00		4.60	J			69
Particle Size Distribution 1-2 µm	%	6.37		7.80				
Particle Size Distribution 2-5 µm	%	19.57		29.52				
Particle Size Distribution 5-15 µm	%	28.99		45.38				
Particle Size Distribution 15-25 µm	%	11.11		10.52				
Particle Size Distribution 25-50 µm	%	16.22		4.65				
Particle Size Distribution 50-100 µm	%	12.72		1.06				
Particle Size Distribution >100 µm	%	5.03		1.06				
Suspended Sediment Coarse	mg/L	9.8		0.7				93
Suspended Sediment Fine	mg/L	12.7		5.4				57
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

R = rejected (chemical analysis criteria); U = at or below detection limit; G = value greater than max. detection limit; NA = not applicable



Precipitation Inf	ormation			
Goal	Result	QA	Notes	
≥0.15	0.65			
≥1	17.2			
NA	0.05			
0.03	0.04			
≥6	18.8			
	Goal ≥0.15 ≥1 NA 0.03	≥0.15 0.65 ≥1 17.2 NA 0.05 0.03 0.04	Goal Result QA ≥0.15 0.65 ≥1 17.2 NA 0.05 0.03 0.04	Goal Result QA Notes ≥0.15 0.65 ≥1 17.2 NA 0.05 0.05 0.03 0.04 0.04

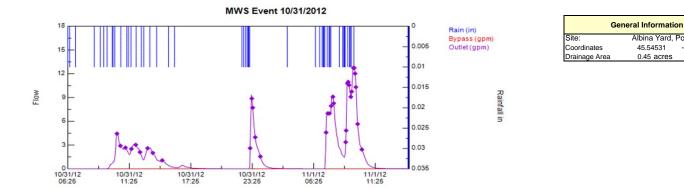
		Sampling	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	31				
% Storm Sampled	≥75	95				
Sampling Duration (hr)	≤36	15				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	48.0		72.8		
Duration (hr)	NA	18.5		3.1		
Volume (gal)	NA	5785.8		571.6		

Albina Yard, Portland, OR 45.54531 -122.67559

Т

0.45 acres

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.13		0.04	ſ			68
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	35.0		35.0				0.0
Total Suspend Solids	mg/L	57.0		12.0				79
Total Kjedahl Nitrogen	mg/L	0.73	J	0.45	J			38
Nitrate + Nitrite	mg/L	1.40	В	1.20	В			14.3
pН	std units	7.41		7.36				1
Copper Total	ug/L	7.10		3.00				58
Copper Dissolved	ug/L	2.80		2.10				25
Lead Total	ug/L	10.00		2.10				79
Lead Dissolved	ug/L	1.00	U	1.00	U			0
Zinc Total	ug/L	66.00		17.00				74
Zinc Dissolved	ug/L	20.00		7.40	J			63
Particle Size Distribution 1-2 µm	%	3.38		4.32				
Particle Size Distribution 2-5 µm	%	10.86		12.22				
Particle Size Distribution 5-15 µm	%	32.47		27.12				
Particle Size Distribution 15-25 µm	%	16.37		14.30				
Particle Size Distribution 25-50 µm	%	21.48		20.74				
Particle Size Distribution 50-100 µm	%	12.03		13.16				
Particle Size Distribution >100 µm	%	3.41		8.15				
Suspended Sediment Coarse	mg/L	8.9		0.4				96
Suspended Sediment Fine	mg/L	51.6		11.0				79
				ts - Gral				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	140		70				50
E. Coli	MPN/100 ml	116		150				-29
Total Petroleum Hydrocarbons -Diesel	mg/L	21.00		0.25				98.8
Total Petroleum Hydrocarbons -Oil	mg/L	90.00		0.80				99
Oil and Grease	mg/L	10.0		5.0	U			50



Precipitation Information							
	Goal	Result	QA	Notes			
Precipitation Total (in)	≥0.15	0.49					
Precipitation Duration (hr)	≥1	33.3					
Max Precip. Intensity (in/5 min)	NA	0.01					
Mean Precip. Intensity (in/hr)	0.03	0.02					
Antecedent Dry Period (hr)	≥6	16.1					

Sampling Information								
Goal Result QA notes								
Number of Aliquots	≥10	33						
% Storm Sampled	≥75	94						
Sampling Duration (hr)	≤36	24						
		Flow Inf	ormatio	n				
	Goal	Treated	QA	Bypass	QA notes			
Max Discharge (gpm)	NA	12.7		0.0				
Duration (hr)	NA	25.4		0.0				
Volume (gal)	NA	2491.4		0.0				

Albina Yard, Portland, OR 45.54531 -122.67559

1

0.45 acres

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.10		0.04	J			61
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	45.0		46.0				-2.2
Total Suspend Solids	mg/L	30.0		11.0				63
Total Kjedahl Nitrogen	mg/L	0.69	J	0.43	J			38
Nitrate + Nitrite	mg/L	0.47	В	0.61	В			-29.8
pH	std units	7.52		7.56				-1
Copper Total	ug/L	5.10		2.90				43
Copper Dissolved	ug/L	1.80	J	1.10	J			39
Lead Total	ug/L	6.00		2.50				58
Lead Dissolved	ug/L	1.00	U	1.00	U			0
Zinc Total	ug/L	46.00		18.00				61
Zinc Dissolved	ug/L	15.00		6.80	J			55
Particle Size Distribution 1-2 µm	%	3.71		5.25				
Particle Size Distribution 2-5 µm	%	11.27		17.00				
Particle Size Distribution 5-15 µm	%	26.76		32.31				
Particle Size Distribution 15-25 µm	%	14.84		17.51				
Particle Size Distribution 25-50 µm	%	19.97		20.47				
Particle Size Distribution 50-100 µm	%	18.11		7.04				
Particle Size Distribution >100 µm	%	5.33		0.41				
Suspended Sediment Coarse	mg/L	5.7		0.5				91
Suspended Sediment Fine	mg/L	30.1		14.7				51
		Sampl	e Resul	ts - Gral	b			
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	1300		80				94
E. Coli	MPN/100 ml	225		108				52
Total Petroleum Hydrocarbons -Diesel	mg/L	3.40		0.51				85.0
Total Petroleum Hydrocarbons -Oil	mg/L	15.00		1.80				88
Oil and Grease	mg/L	8.5		5.0	U			41

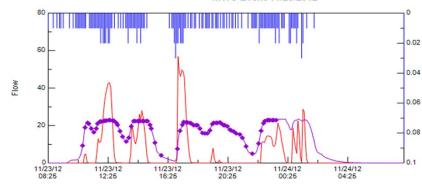
 $\frac{1}{R} = rejected (chemical analysis criteria); U = at or below detection limit; G = value greater than max. detection limit; NA = not applicable$

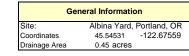
Rainfall in

Rain (in)

Bypass (gpm) Outlet (gpm)

MWS Event 11/23/2012





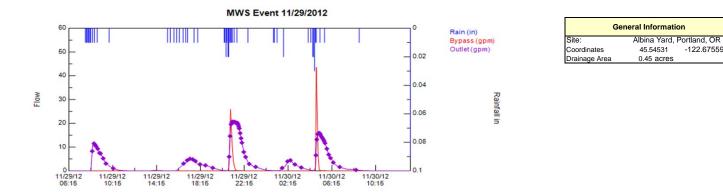
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	Precipitation Inf	formation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	1.61			
Precipitation Duration (hr)	≥1	17.8			
Max Precip. Intensity (in/5 min)	NA	0.03			
Mean Precip. Intensity (in/hr)	0.03	0.09			
Antecedent Dry Period (hr)	≥6	44.5			
					-

		Sampling I	nformat	ion		Sampling Information									
	Goal	Result	QA	notes											
Number of Aliquots	≥10	80													
% Storm Sampled	≥75	77													
Sampling Duration (hr)	≤36	13													
Flow Information															
	Goal	Treated	QA	Bypass	QA	notes									
Max Discharge (gpm)	NA	23.4		56.8											
Duration (hr)	NA	22.7		18.7											
/olume (gal)	NA	16627.8		6981.6											

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.03		0.01	U			62
Ortho-Phosphorus	mg/L							NA
Hardness	mg/L							NA
Total Suspend Solids	mg/L	6.5		1.7				74
Total Kjedahl Nitrogen	mg/L	0.77		0.84				-9
Nitrate + Nitrite	mg/L	0.22		0.27				-21.1
pH	std units	7.29		7.41				-2
Copper Total	ug/L	1.70		1.90				-12
Copper Dissolved	ug/L	1.20		1.60				-33
Lead Total	ug/L	0.92		0.22				76
Lead Dissolved	ug/L	0.02		0.03				-50
Zinc Total	ug/L	15.20		4.00				74
Zinc Dissolved	ug/L	10.70		3.40				68
Particle Size Distribution 1-2 µm	%	9.80		7.66				
Particle Size Distribution 2-5 µm	%	24.68		24.67				
Particle Size Distribution 5-15 µm	%	36.99		44.28				
Particle Size Distribution 15-25 µm	%	11.50		13.44				
Particle Size Distribution 25-50 µm	%	9.74		7.47				
Particle Size Distribution 50-100 µm	%	7.28		1.90				
Particle Size Distribution >100 µm	%	0.00		0.57				
Suspended Sediment Coarse	mg/L							NA
Suspended Sediment Fine	mg/L							NA
				ts - Gral	b			
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

R = rejected (chemical analysis criteria); U = at or below detection limit; G = value greater than max. detection limit; NA = not applicable



	Precipitation Inf	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.57			
Precipitation Duration (hr)	≥1	31.2			
Max Precip. Intensity (in/5 min)	NA	0.03			
Mean Precip. Intensity (in/hr)	0.03	0.02			
Antecedent Dry Period (hr)	≥6	20.0			

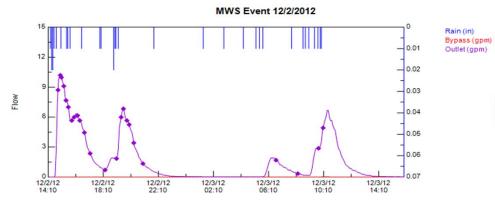
Sampling Information								
	Goal	Result	QA	notes				
Number of Aliquots	≥10	63						
% Storm Sampled	≥75	98						
Sampling Duration (hr)	≤36	24						
Flow Information								
	Goal	Treated	QA	Bypass	QA	notes		
Max Discharge (gpm)	NA	20.6		43.5				
Duration (hr)	NA	29.2		25.8				
Volume (gal)	NA	4597.3		762.3				

-122.67559

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	Sample Results - Flow Composite										
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction			
Total Phosphorus	mg/L	0.09		0.04				61			
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0			
Hardness	mg/L	33.2		30.4				8.4			
Total Suspend Solids	mg/L	34.2		16.0				53			
Total Kjedahl Nitrogen	mg/L	0.90		1.08				-20			
Nitrate + Nitrite	mg/L	0.12		3.58				-2858.7			
pH	std units	7.74		7.32				5			
Copper Total	ug/L	5.80		3.30				43			
Copper Dissolved	ug/L	2.70		1.90				30			
Lead Total	ug/L	7.05		3.69				48			
Lead Dissolved	ug/L	0.04		0.06				-50			
Zinc Total	ug/L	44.30		18.70				58			
Zinc Dissolved	ug/L	10.80		9.90				8			
Particle Size Distribution 1-2 µm	%	5.43		6.24							
Particle Size Distribution 2-5 µm	%	15.33		17.82							
Particle Size Distribution 5-15 µm	%	25.44		30.33							
Particle Size Distribution 15-25 µm	%	11.54		12.39							
Particle Size Distribution 25-50 µm	%	14.41		15.82							
Particle Size Distribution 50-100 µm	%	18.51		13.78							
Particle Size Distribution >100 µm	%	9.35		3.63							
Suspended Sediment Coarse	mg/L							NA			
Suspended Sediment Fine	mg/L							NA			
		Sampl	e Resul	ts - Gral	b						
	Units	IN	QA	OUT	QA	MDL	notes				
Fecal Coliform	MPN/100 ml							NA			
E. Coli	MPN/100 ml							NA			
Total Petroleum Hydrocarbons -Diesel	mg/L							NA			
Total Petroleum Hydrocarbons -Oil	mg/L							NA			
Oil and Grease	mg/L							NA			

Rainfall in



General Information										
Site:	Albina Yard,	Portland, OR								
Coordinates	45.54531	-122.67559								
Drainage Area	0.45 acres									

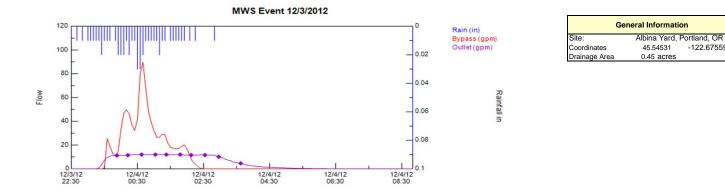
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	Precipitation Inf	ormation								
	Goal	Result	QA	Notes						
Precipitation Total (in)	≥0.15	0.35								
Precipitation Duration (hr)	≥1	25.8								
Max Precip. Intensity (in/5 min)	NA	0.02								
Mean Precip. Intensity (in/hr)	0.03	0.01								
Antecedent Dry Period (hr)	≥6	9.5								

		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	24				
% Storm Sampled	≥75	78				
Sampling Duration (hr)	≤36	19				
		Flow Infe	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	10.2		0.0		
Duration (hr)	NA	25.6		0.8		
Volume (gal)	NA	2434.0		0.8		

Sample Results - Flow Composite											
	Units	- IN	QA	OUT	QA	MDL	notes	% Reduction			
Total Phosphorus	mg/L	0.03		0.01				63			
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0			
Hardness	mg/L	29.2		30.0				-2.7			
Total Suspend Solids	mg/L	6.7		2.6				61			
Total Kjedahl Nitrogen	mg/L	0.94		0.79				16			
Nitrate + Nitrite	mg/L	2.84		2.79				1.8			
pH	std units	7.15		7.19				-1			
Copper Total	ug/L	4.60		6.10				-33			
Copper Dissolved	ug/L	3.20		4.60				-44			
Lead Total	ug/L	0.96		0.46				52			
Lead Dissolved	ug/L	0.05		0.04				20			
Zinc Total	ug/L	16.50		6.80				59			
Zinc Dissolved	ug/L	14.80		6.00				59			
Particle Size Distribution 1-2 µm	%	5.50		6.24							
Particle Size Distribution 2-5 µm	%	20.84		17.82							
Particle Size Distribution 5-15 µm	%	35.40		30.33							
Particle Size Distribution 15-25 µm	%	16.32		12.39							
Particle Size Distribution 25-50 µm	%	13.80		15.82							
Particle Size Distribution 50-100 µm	%	6.80		13.78							
Particle Size Distribution >100 µm	%	1.33		3.63							
Suspended Sediment Coarse	mg/L							NA			
Suspended Sediment Fine	mg/L							NA			
				ts - Gra							
	Units	IN	QA	OUT	QA	MDL	notes				
Fecal Coliform	MPN/100 ml							NA			
E. Coli	MPN/100 ml	350		110				69			
Total Petroleum Hydrocarbons -Diesel	mg/L	1.40	Н	0.26	н			81.4			
Total Petroleum Hydrocarbons -Oil	mg/L	7.30	0	1.10	0			85			
Oil and Grease	mg/L	5.6		4.7	U			16			

R = rejected (chemical analysis criteria); U = at or below detection limit; G = value greater than max. detection limit; NA = not applicable



	Precipitation Information										
	Goal	Result	QA	Notes							
Precipitation Total (in)	≥0.15	0.51									
Precipitation Duration (hr)	≥1	4.3									
Max Precip. Intensity (in/5 min)	NA	0.03									
Mean Precip. Intensity (in/hr)	0.03	0.12									
Antecedent Dry Period (hr)	≥6	13.0									

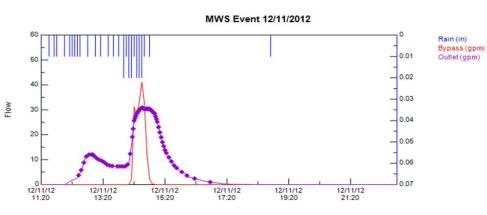
Sampling Information											
	Goal	Result	QA	notes							
Number of Aliquots	≥10	10									
% Storm Sampled	≥75	83									
Sampling Duration (hr)	≤36	4									
	Flow Information										
	Goal	Treated	QA	Bypass	QA	notes					
Max Discharge (gpm)	NA	12.0		89.7							
Duration (hr)	NA	9.7		4.5							
Volume (gal)	NA	2936.6		5052.3							

-122.67559

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Sample Results - Flow Composite										
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction		
Total Phosphorus	mg/L	0.08		0.02				69		
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0		
Hardness	mg/L							NA		
Total Suspend Solids	mg/L	22.8		5.7				75		
Total Kjedahl Nitrogen	mg/L							NA		
Nitrate + Nitrite	mg/L							NA		
рН	std units							NA		
Copper Total	ug/L	5.60		5.90				-5		
Copper Dissolved	ug/L	2.40		2.80				-17		
Lead Total	ug/L	3.83		0.70				82		
Lead Dissolved	ug/L	0.03		0.02	U			33		
Zinc Total	ug/L	34.40		28.60				17		
Zinc Dissolved	ug/L	13.00		10.90				16		
Particle Size Distribution 1-2 µm	%	2.80		3.27						
Particle Size Distribution 2-5 µm	%	9.44		11.45						
Particle Size Distribution 5-15 µm	%	22.97		28.94						
Particle Size Distribution 15-25 µm	%	12.71		17.29						
Particle Size Distribution 25-50 µm	%	15.61		21.11						
Particle Size Distribution 50-100 µm	%	20.66		15.70						
Particle Size Distribution >100 µm	%	15.82		2.23						
Suspended Sediment Coarse	mg/L							NA		
Suspended Sediment Fine	mg/L							NA		
				lts - Grat						
	Units	IN	QA	OUT	QA	MDL	notes			
Fecal Coliform	MPN/100 ml							NA		
E. Coli	MPN/100 ml							NA		
Total Petroleum Hydrocarbons -Diesel	mg/L							NA		
Total Petroleum Hydrocarbons -Oil	mg/L							NA		
Oil and Grease	mg/L							NA		

Rainfall in



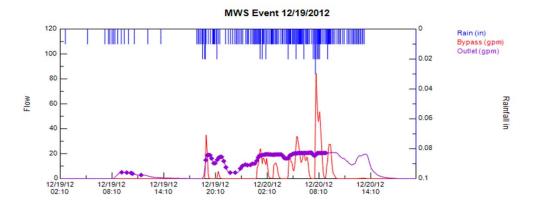
Ge	neral Informatio	on
Site:	Albina Yard,	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

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Sampling Information									
	Goal	Result	QA	notes					
Number of Aliquots	≥10	69							
% Storm Sampled	≥75	97							
Sampling Duration (hr)	≤36	4							
		Flow Infe	ormatio	n					
	Goal	Treated	QA	Bypass	QA	notes			
Max Discharge (gpm)	NA	30.9		30.9					
Duration (hr)	NA	10.8		4.5					
Volume (gal)	NA	3119.4		918.1					

Sample Results - Flow Composite										
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction		
Total Phosphorus	mg/L	0.26		0.05				79		
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0		
Hardness	mg/L	27.2		29.6				-8.8		
Total Suspend Solids	mg/L	45.3		14.0				69		
Total Kjedahl Nitrogen	mg/L	1.08		0.65				40		
Nitrate + Nitrite	mg/L	0.10		0.09				8.7		
pН	std units	7.88		7.92				-1		
Copper Total	ug/L	6.10		2.70				56		
Copper Dissolved	ug/L	5.10		2.40				53		
Lead Total	ug/L	7.10		2.47				65		
Lead Dissolved	ug/L	4.93		2.09				58		
Zinc Total	ug/L	51.70		14.70				72		
Zinc Dissolved	ug/L	45.00		13.30				70		
Sediment < 1 µm	%	6.24		10.03						
Sediment 1 - 3.9 µm	%	7.79		5.37						
Sediment 3.9 - 62.5 µm	%	32.91		0.00						
Sediment 62.5 - 125 µm	%	0.00		0.00						
Sediment 125 -250 µm	%	0.00		0.00						
Sediment 250 -500 µm	%	1.58		0.49						
Sediment > 500 µm	%	0.79		0.79						
Total Sediment	mg/L	41.5		10.7				74		
Sample Results - Grab										
	Units	IN	QA	OUT	QA	MDL	notes			
Fecal Coliform	MPN/100 ml							NA		
E. Coli	MPN/100 ml							NA		
Total Petroleum Hydrocarbons -Diesel	mg/L							NA		
Total Petroleum Hydrocarbons -Oil	mg/L							NA		
Oil and Grease	mg/L							NA		



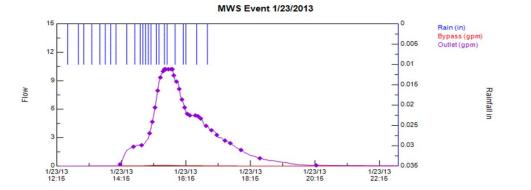
Gei	neral Information
Site:	Albina Yard, Portland, OR
Coordinates	45.54531 -122.67559
Drainage Area	0.45 acres

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Precipitation Information									
	Goal	Result	QA	Notes					
Precipitation Total (in)	≥0.15	1.85							
Precipitation Duration (hr)	≥1	35.2							
Max Precip. Intensity (in/5 min)	NA	0.03							
Mean Precip. Intensity (in/hr)	0.03	0.05							
Antecedent Dry Period (hr)	≥6	17.4							

Sampling Information									
	Goal	Result	QA	notes					
Number of Aliquots	≥10	80							
% Storm Sampled	≥75	71							
Sampling Duration (hr)	≤36	24							
		Flow Infe	ormatio	n					
	Goal	Treated	QA	Bypass	QA	notes			
Max Discharge (gpm)	NA	21.0		21.0					
Duration (hr)	NA	39.9		19.2					
Volume (gal)	NA	20265.8		8112.6					

	Sa	mple Res	ults - Fl	ow Con	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.07		0.03				66
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	19.6		25.2				-28.6
Total Suspend Solids	mg/L	48.7		5.5				89
Total Kjedahl Nitrogen	mg/L	0.40	U	0.40	U			0
Nitrate + Nitrite	mg/L	0.07		0.05	U			23.1
pH	std units	7.86		7.71				2
Copper Total	ug/L	3.10		1.50				52
Copper Dissolved	ug/L	1.00		0.90				10
Lead Total	ug/L	3.54		0.84				76
Lead Dissolved	ug/L	0.02	U	0.02	U			0
Zinc Total	ug/L	31.40		7.20				77
Zinc Dissolved	ug/L	13.10		4.20				68
Sediment < 1 µm	%	3.27		4.85				
Sediment 1 - 3.9 µm	%	4.60		2.67				
Sediment 3.9 - 62.5 µm	%	3.27		0.00				
Sediment 62.5 - 125 µm	%	0.00		0.00				
Sediment 125 -250 µm	%	0.00		0.00				
Sediment 250 -500 µm	%	0.59		0.10				
Sediment > 500 µm	%	0.49		0.00				
Total Sediment	mg/L	50.2		4.2				92
				ts - Gra				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	NaN		NaN				NA
E. Coli	MPN/100 ml	540		350				35
Total Petroleum Hydrocarbons -Diesel	mg/L	0.44	н	0.25	U			43.2
Total Petroleum Hydrocarbons -Oil	mg/L	2.20	0	0.50	U			77
Oil and Grease	mg/L	4.7	U	4.7	U			0



Ge	neral Information
Site:	Albina Yard, Portland, OR
Coordinates	45.54531 -122.67559
Drainage Area	0.45 acres

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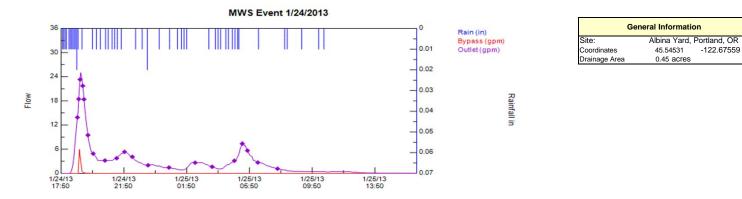
	Precipitation Inf	formation		
	Goal	Result	QA	Notes
Precipitation Total (in)	≥0.15	0.25		
Precipitation Duration (hr)	≥1	4.7		
Max Precip. Intensity (in/5 min)	NA	0.01		
Mean Precip. Intensity (in/hr)	0.03	0.05		
Antecedent Dry Period (hr)	≥6	214.1		

	Sampling Information									
	Goal	Result	QA	notes						
Number of Aliquots	≥10	32								
% Storm Sampled	≥75	99								
Sampling Duration (hr)	≤36	6								
		Flow Inf	ormatio	n						
	Goal	Treated	QA	Bypass	QA	notes				
Max Discharge (gpm)	NA	10.2		10.2						
Duration (hr)	NA	8.8		5.6						
Volume (gal)	NA	1124.5		10.7						

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.10		0.08				19
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	40.0		41.2				-3.0
Total Suspend Solids	mg/L	42.0		26.7				36
Total Kjedahl Nitrogen	mg/L	1.22		0.40	U			67
Nitrate + Nitrite	mg/L	0.33		0.29				14.2
рН	std units	8.06		7.72				4
Copper Total	ug/L	9.30		7.10				24
Copper Dissolved	ug/L	4.10		3.50				15
Lead Total	ug/L	7.32		5.50				25
Lead Dissolved	ug/L	0.04		0.04				0
Zinc Total	ug/L	53.90		30.60				43
Zinc Dissolved	ug/L	15.60		7.60				51
Sediment < 1 µm	%	10.08		14.36				
Sediment 1 - 3.9 µm	%	10.27		12.01				
Sediment 3.9 - 62.5 µm	%	25.28		3.36				
Sediment 62.5 - 125 µm	%	0.00	U	0.00	U			
Sediment 125 -250 µm	%	0.00	U	0.00	U			
Sediment 250 -500 µm	%	0.19		0.00	U			
Sediment > 500 µm	%	0.29		0.00	U			
Total Sediment	mg/L	36.5		28.8				21
		Sampl	e Resul	lts - Gral	b			
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	7.8		2				74
E. Coli	MPN/100 ml	7.8		2				74
Total Petroleum Hydrocarbons -Diesel	mg/L	0.25	U	0.24	U			4.0
Total Petroleum Hydrocarbons -Oil	mg/L	0.71	0	0.47	U			34
Oil and Grease	ma/L	4.7	U	4.7	U			0

 [Oil and Grease
 mg/L
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 notes: j = conditional use (storm/sampling criteria); J = conditional use (chemical analysis criteria); r = rejected (storm/sampling criteria)
 R = rejected (chemical analysis criteria); U = at o below detection limit; G = value greater than max. detection limit; NA = not applicable



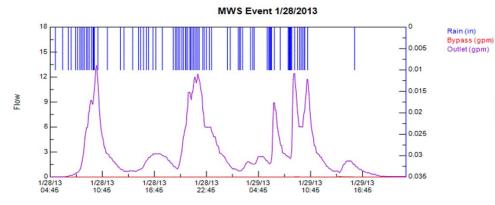
	Precipitation Inf	ormation			
	Goal	Result	QA	Notes	
Precipitation Total (in)	≥0.15	0.50			
Precipitation Duration (hr)	≥1	16.8			
Max Precip. Intensity (in/5 min)	NA	0.02			
Mean Precip. Intensity (in/hr)	0.03	0.03			
Antecedent Dry Period (hr)	≥6	25.7			

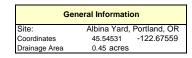
		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	20				
% Storm Sampled	≥75	89				
Sampling Duration (hr)	≤36	13				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	25.0		25.0		
Duration (hr)	NA	22.2		2.8		
Volume (gal)	NA	3095.8		50.7		

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	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.10		0.04				60
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	38.0		34.8				8.4
Total Suspend Solids	mg/L	41.2		14.3				65
Total Kjedahl Nitrogen	mg/L	1.20		1.00				17
Nitrate + Nitrite	mg/L	0.27		0.21				21.1
рН	std units	7.71		7.81				-1
Copper Total	ug/L	13.60		8.97				34
Copper Dissolved	ug/L	11.70		5.34				54
Lead Total	ug/L	5.58		2.05				63
Lead Dissolved	ug/L	0.31		0.02				93
Zinc Total	ug/L	44.00		15.00				66
Zinc Dissolved	ug/L	19.80		6.92				65
Sediment < 1 µm	%	6.50		8.54				
Sediment 1 - 3.9 µm	%	6.64		4.38				
Sediment 3.9 - 62.5 µm	%	23.15		0.00	U			
Sediment 62.5 - 125 µm	%	0.00	U	0.00	U			
Sediment 125 -250 µm	%	0.00	U	0.00	U			
Sediment 250 -500 µm	%	0.00	U	0.00	U			
Sediment > 500 µm	%	0.00	U	0.00	U			
Total Sediment	mg/L	38.5		11.2				71
				ts - Grab				
	Units	IN	QA	OUT	QA	MDL	notes	-
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

Rainfall in





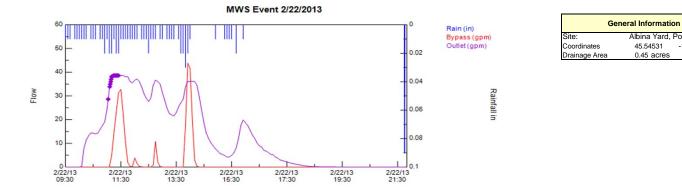
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	Precipitation Information								
	Goal	Result	QA	Notes					
Precipitation Total (in)	≥0.15	0.86							
Precipitation Duration (hr)	≥1	35.1							
Max Precip. Intensity (in/5 min)	NA	0.01							
Mean Precip. Intensity (in/hr)	0.03	0.03							
Antecedent Dry Period (hr)	≥6	13.6							

		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	0				
% Storm Sampled	≥75	0				
Sampling Duration (hr)	≤36	0				
		Flow Infe	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	13.4		0.0		
Duration (hr)	NA	41.1		4.0		
Volume (gal)	NA	7159.1		5.2		

	Sa	mple Res	ults - Fl	ow Com	nposite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L							NA
Ortho-Phosphorus	mg/L							NA
Hardness	mg/L							NA
Total Suspend Solids	mg/L							NA
Total Kjedahl Nitrogen	mg/L							NA
Nitrate + Nitrite	mg/L							NA
pH	std units							NA
Copper Total	ug/L							NA
Copper Dissolved	ug/L							NA
Lead Total	ug/L							NA
Lead Dissolved	ug/L							NA
Zinc Total	ug/L							NA
Zinc Dissolved	ug/L							NA
Particle Size Distribution 1-2 µm	%							
Particle Size Distribution 2-5 µm	%							
Particle Size Distribution 5-15 µm	%							
Particle Size Distribution 15-25 µm	%							
Particle Size Distribution 25-50 µm	%							
Particle Size Distribution 50-100 µm	%							
Particle Size Distribution >100 µm	%							
Suspended Sediment Coarse	mg/L							NA
Suspended Sediment Fine	mg/L							NA
			le Resul					
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	79		79				0
E. Coli	MPN/100 ml	114		47				59
Total Petroleum Hydrocarbons -Diesel	mg/L	0.37	н	0.25	U			32.4
Total Petroleum Hydrocarbons -Oil	mg/L	1.80	0	0.60	0			67
Oil and Grease	mg/L	4.8	U	4.8	U			0

notes: j = conditional use (storm/sampling criteria); U = at or below detection limit; G = value greater than max. detection limit; NA = not applicable



	Precipitation In	ormation		
	Goal	Result	QA	Notes
Precipitation Total (in)	≥0.15	0.67		
Precipitation Duration (hr)	≥1	6.4		
Max Precip. Intensity (in/5 min)	NA	0.03		
Mean Precip. Intensity (in/hr)	0.03	0.10		
Antecedent Dry Period (hr)	≥6	41.6		

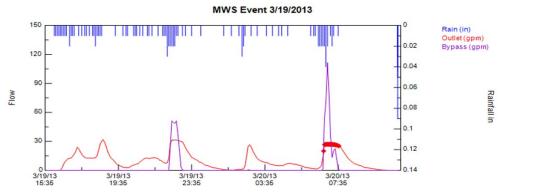
		Sampling I	nformat	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	20				
% Storm Sampled	≥75	9				
Sampling Duration (hr)	≤36	0				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	38.6		38.6		
Duration (hr)	NA	11.8		5.3		
Volume (gal)	NA	9208.0		1441.6		

Albina Yard, Portland, OR 45.54531 -122.67559 0.45 acres

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	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.56		0.26				53
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	62.8		50.8				19.1
Total Suspend Solids	mg/L	271.0		116.0				57
Total Kjedahl Nitrogen	mg/L	1.81		1.15				36
Nitrate + Nitrite	mg/L	0.26		0.19				27.3
pH	std units	8.84		8.14				8
Copper Total	ug/L	29.50		15.10				49
Copper Dissolved	ug/L	2.50		2.40				4
Lead Total	ug/L	56.00		26.50				53
Lead Dissolved	ug/L	0.08		0.02	U			75
Zinc Total	ug/L	247.00		103.00				58
Zinc Dissolved	ug/L	2.20		6.00				-173
Sediment < 1 µm	%	93.07		44.80				
Sediment 1 - 3.9 µm	%	77.38		40.60				
Sediment 3.9 - 62.5 µm	%	183.30		49.94				
Sediment 62.5 - 125 µm	%	2.82		0.00	U			
Sediment 125 -250 µm	%	0.00	U	0.00	U			
Sediment 250 -500 µm	%	6.48		0.29				
Sediment > 500 µm	%	3.33		0.00	U			
Total Sediment	mg/L	271.0		116.0				57
				lts - Grat				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml	140		70				50
E. Coli	MPN/100 ml	71.2		107				-50
Total Petroleum Hydrocarbons -Diesel	mg/L	0.94	Н	0.59	Н			37.2
Total Petroleum Hydrocarbons -Oil	mg/L	3.80	0	2.30	0			39
Oil and Grease	mg/L	18.8		12.8				32

 $\frac{1}{1} \frac{1}{1} \frac{1}$



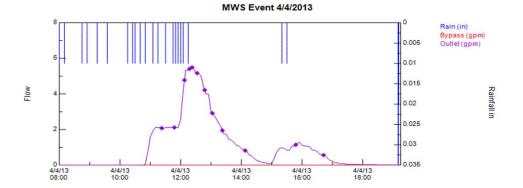
Ge	eneral Information
Site:	Albina Yard, Portland, OR
Coordinates	45.54531 -122.67559
Drainage Area	0.45 acres

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	Precipitation In	formation		
	Goal	Result	QA	Notes
Precipitation Total (in)	≥0.15	1.03		
Precipitation Duration (hr)	≥1	16.0		
Max Precip. Intensity (in/5 min)	NA	0.04		
Mean Precip. Intensity (in/hr)	0.03	0.06		
Antecedent Dry Period (hr)	≥6	71.7		

		Sampling I	nformat	ion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	55				
% Storm Sampled	≥75	12				
Sampling Duration (hr)	≤36	1				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	31.8		31.8		
Duration (hr)	NA	20.2		4.6		
Volume (gal)	NA	11259.5		3555.5		

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	0.40		0.13				67
Ortho-Phosphorus	mg/L	0.05	U	0.05	U			0
Hardness	mg/L	36.8		39.2				-6.5
Total Suspend Solids	mg/L	209.0		47.0				78
Total Kjedahl Nitrogen	mg/L	1.43		0.80				44
Nitrate + Nitrite	mg/L	0.10		0.10				3.9
pH	std units	7.86		7.77				1
Copper Total	ug/L	17.80		6.50				63
Copper Dissolved	ug/L	2.60		2.20				15
Lead Total	ug/L	22.00		8.22				63
Lead Dissolved	ug/L	0.06		0.06				0
Zinc Total	ug/L	161.00		55.40				66
Zinc Dissolved	ug/L	10.40		12.20				-17
Sediment < 1 µm	%	33.83		11.62				
Sediment 1 - 3.9 µm	%	35.19		9.22				
Sediment 3.9 - 62.5 µm	%	197.31		32.53				
Sediment 62.5 - 125 µm	%	4.28		0.00	U			
Sediment 125 -250 µm	%	0.00	U	0.00	U			
Sediment 250 -500 µm	%	6.29		7.03				
Sediment > 500 µm	%	7.72		4.03				
Total Sediment	mg/L	180.0		46.7				74
				ts - Grab				
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA



Ge	neral Informat	ion
Site:	Albina Yard,	Portland, OR
Coordinates	45.54531	-122.67559
Drainage Area	0.45 acres	

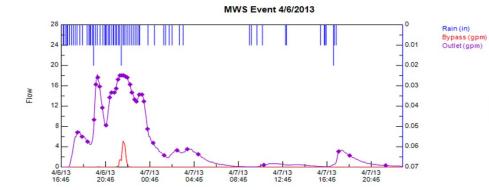
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	Precipitation In	formation		
	Goal	Result	QA	Notes
Precipitation Total (in)	≥0.15	0.22		
Precipitation Duration (hr)	≥1	7.5		
Max Precip. Intensity (in/5 min)	NA	0.01		
Mean Precip. Intensity (in/hr)	0.03	0.03		
Antecedent Dry Period (hr)	≥6	305.2		

	Sampling Information							
	Goal	Result	QA	notes				
Number of Aliquots	≥10	12						
% Storm Sampled	≥75	89						
Sampling Duration (hr)	≤36	5						
		Flow Inf	ormatio	n				
	Goal	Treated	QA	Bypass	QA	notes		
Max Discharge (gpm)	NA	5.5		5.5				
Duration (hr)	NA	8.4		0.0				
Volume (gal)	NA	650.7		0.0				

	Sa	mple Res	ults - Fl	ow Com	posite			
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction
Total Phosphorus	mg/L	2.15		0.40				81
Ortho-Phosphorus	mg/L	0.96		0.20				79
Hardness	mg/L	76.0		58.8				22.6
Total Suspend Solids	mg/L	145.0		19.0				87
Total Kjedahl Nitrogen	mg/L	9.32		1.20				87
Nitrate + Nitrite	mg/L	0.26		0.26				-3.5
рН	std units	7.09		7.69				-8
Copper Total	ug/L	85.60		33.20				61
Copper Dissolved	ug/L	34.00		27.50				19
Lead Total	ug/L	24.30		6.61				73
Lead Dissolved	ug/L	6.76		4.08				40
Zinc Total	ug/L	505.00		208.00				59
Zinc Dissolved	ug/L	352.00		194.00				45
Sediment < 1 µm	%	171.01		0.72				
Sediment 1 - 3.9 µm	%	0.00	U	0.10				
Sediment 3.9 - 62.5 µm	%	0.00	U	3.30				
Sediment 62.5 - 125 µm	%	0.00	U	12.57				
Sediment 125 -250 µm	%	0.00	U	3.66				
Sediment 250 -500 µm	%	9.15		10.68				
Sediment > 500 µm	%	32.70		6.43				
Total Sediment	mg/L	301.0		21.6				93
		Sample	e Resu	lts - Grab)			
	Units	IN	QA	OUT	QA	MDL	notes	
Fecal Coliform	MPN/100 ml							NA
E. Coli	MPN/100 ml							NA
Total Petroleum Hydrocarbons -Diesel	mg/L							NA
Total Petroleum Hydrocarbons -Oil	mg/L							NA
Oil and Grease	mg/L							NA

Rainfall in



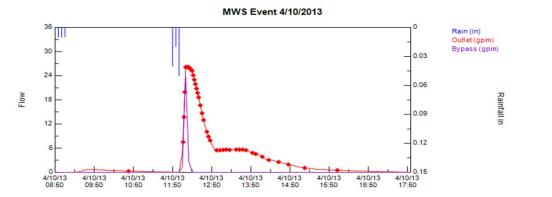
Ge	neral Information
Site:	Albina Yard, Portland, OR
Coordinates	45.54531 -122.67559
Drainage Area	0.45 acres

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Precipitation Information											
	Goal	Result	QA	Notes							
Precipitation Total (in)	≥0.15	0.71									
Precipitation Duration (hr)	≥1	30.8									
Max Precip. Intensity (in/5 min)	NA	0.02									
Mean Precip. Intensity (in/hr)	0.03	0.02									
Antecedent Dry Period (hr)	≥6	10.5									

Sampling Information										
	Goal	Result	QA	notes						
Number of Aliquots	≥10	36								
% Storm Sampled	≥75	97								
Sampling Duration (hr)	≤36	28								
		Flow Inf	ormatio	n						
	Goal	Treated	QA	Bypass	QA notes					
Max Discharge (gpm)	NA	18.2		18.2						
Duration (hr)	NA	30.9		2.5						
Volume (gal)	NA	6523.9		130.8						

Sample Results - Flow Composite											
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction			
Total Phosphorus	mg/L	0.17		0.04				75			
Ortho-Phosphorus	mg/L	0.12		0.05	U			59			
Hardness	mg/L	36.0		38.4				-6.7			
Total Suspend Solids	mg/L	12.0		2.1				83			
Total Kjedahl Nitrogen	mg/L	0.96		0.67				30			
Nitrate + Nitrite	mg/L	0.07		0.05	U			30.6			
pH	std units	7.67		6.96				9			
Copper Total	ug/L	18.60		8.60				54			
Copper Dissolved	ug/L	14.40		7.60				47			
Lead Total	ug/L	2.23		0.54				76			
Lead Dissolved	ug/L	0.72		0.32				56			
Zinc Total	ug/L	42.10		16.40				61			
Zinc Dissolved	ug/L	33.80		15.60				54			
Sediment < 1 µm	%	0.38		0.68							
Sediment 1 - 3.9 µm	%	0.08		0.12							
Sediment 3.9 - 62.5 µm	%	1.83		0.00	U						
Sediment 62.5 - 125 µm	%	8.92		0.00	U						
Sediment 125 -250 µm	%	1.33		0.00	U						
Sediment 250 -500 µm	%	8.47		7.67							
Sediment > 500 µm	%	6.35		6.89							
Total Sediment	mg/L	18.0		1.7				91			
Sample Results - Grab											
	Units	IN	QA	OUT	QA	MDL	notes				
Fecal Coliform	MPN/100 ml							NA			
E. Coli	MPN/100 ml							NA			
Total Petroleum Hydrocarbons -Diesel	mg/L							NA			
Total Petroleum Hydrocarbons -Oil	mg/L							NA			
Oil and Grease	mg/L							NA			



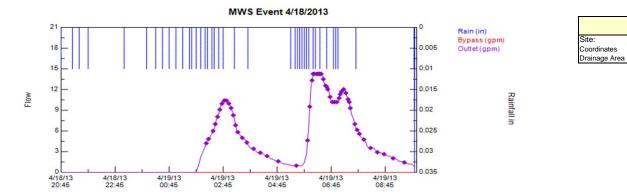
Ge	eneral Information
Site:	Albina Yard, Portland, OR
Coordinates	45.54531 -122.67559
Drainage Area	0.45 acres

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Precipitation Information											
	Goal	Result	QA	Notes							
Precipitation Total (in)	≥0.15	0.15									
Precipitation Duration (hr)	≥1	3.2									
Max Precip. Intensity (in/5 min)	NA	0.05									
Mean Precip. Intensity (in/hr)	0.03	0.05									
Antecedent Dry Period (hr)	≥6	63.5									

	ion					
	Goal	Result	QA	notes		
Number of Aliquots	≥10	41				
% Storm Sampled	≥75	96				
Sampling Duration (hr)	≤36	5				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	26.1		26.1		
Duration (hr)	NA	8.7		0.4		
Volume (gal)	NA	1468.0		156.6		

	Sa	ample Res	ults - Fl	ow Com	posite					
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction		
Total Phosphorus	mg/L							NA		
Ortho-Phosphorus	mg/L	0.43		0.05	U			88		
Hardness	mg/L	43.2		41.6				3.7		
Total Suspend Solids	mg/L	153.0		17.1				89		
Total Kjedahl Nitrogen	mg/L	1.66		1.17				30		
Nitrate + Nitrite	mg/L	0.09		0.05	U			45.7		
pH	std units	7.83		8.13				-4		
Copper Total	ug/L	28.70		11.90				59		
Copper Dissolved	ug/L	20.50		9.00				56		
Lead Total	ug/L	14.00		2.62				81		
Lead Dissolved	ug/L	2.36		1.11				53		
Zinc Total	ug/L	201.00		72.60				64		
Zinc Dissolved	ug/L	152.00		65.20				57		
Sediment < 1 µm	%	9.63		0.51						
Sediment 1 - 3.9 µm	%	1.55		0.12						
Sediment 3.9 - 62.5 µm	%	24.96		2.21						
Sediment 62.5 - 125 µm	%	86.22		10.13						
Sediment 125 -250 µm	%	12.58		0.83						
Sediment 250 -500 µm	%	5.45		4.62						
Sediment > 500 µm	%	4.11		4.13						
Total Sediment	mg/L	215.0		15.3				93		
Sample Results - Grab										
	Units	IN	QA	OUT	QA	MDL	notes			
Fecal Coliform	MPN/100 ml							NA		
E. Coli	MPN/100 ml							NA		
Total Petroleum Hydrocarbons -Diesel	mg/L							NA		
Total Petroleum Hydrocarbons -Oil	mg/L							NA		
Oil and Grease	mg/L							NA		



Precipitation Information												
	Goal	Result	QA	Notes								
Precipitation Total (in)	≥0.15	0.39										
Precipitation Duration (hr)	≥1	10.9										
Max Precip. Intensity (in/5 min)	NA	0.01										
Mean Precip. Intensity (in/hr)	0.03	0.04										
Antecedent Dry Period (hr)	≥6	69.9										

	Goal	Result	QA	notes		
Number of Aliquots	≥10	56				
% Storm Sampled	≥75	97				
Sampling Duration (hr)	≤36	7				
		Flow Inf	ormatio	n		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	14.3		14.3		
Duration (hr)	NA	8.2		0.0		
Volume (gal)	NA	2562.1		0.0		

General Information

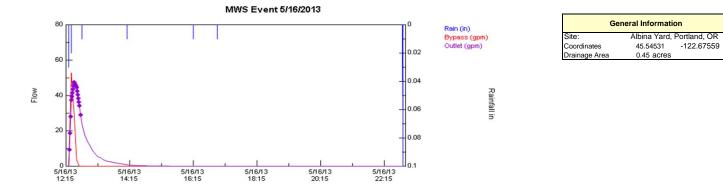
0.45 acres

Albina Yard, Portland, OR

45.54531 -122.67559

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Sample Results - Flow Composite											
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction			
Total Phosphorus	mg/L							NA			
Ortho-Phosphorus	mg/L	0.06		0.05	U			17			
Hardness	mg/L	48.0		47.2				1.7			
Total Suspend Solids	mg/L	20.6		4.7				77			
Total Kjedahl Nitrogen	mg/L	1.02		0.86				16			
Nitrate + Nitrite	mg/L	0.07		0.06				18.1			
pH	std units	7.66		7.69				0			
Copper Total	ug/L	32.20		11.10				66			
Copper Dissolved	ug/L	22.50		9.00				60			
Lead Total	ug/L	4.34		0.92				79			
Lead Dissolved	ug/L	0.53		0.22				58			
Zinc Total	ug/L	362.00		35.80				90			
Zinc Dissolved	ug/L	299.00		31.20				90			
Sediment < 1 µm	%	1.00		0.00	U						
Sediment 1 - 3.9 µm	%	0.23		0.00	U						
Sediment 3.9 - 62.5 µm	%	4.04		0.00	U						
Sediment 62.5 - 125 µm	%	10.39		0.00	U						
Sediment 125 -250 µm	%	6.28		0.00	U						
Sediment 250 -500 µm	%	6.23		6.39							
Sediment > 500 µm	%	6.63		6.49							
Total Sediment	mg/L	27.9		2.6				91			
Sample Results - Grab											
	Units	IN	QA	OUT	QA	MDL	notes				
Fecal Coliform	MPN/100 ml	7.8		17				-118			
E. Coli	MPN/100 ml	6.2		3				50			
Total Petroleum Hydrocarbons -Diesel	mg/L	1.30	U	0.25	U			80.8			
Total Petroleum Hydrocarbons -Oil	mg/L	2.60		0.80	0			69			
Oil and Grease	mg/L	5.0	U	5.0	U			0			

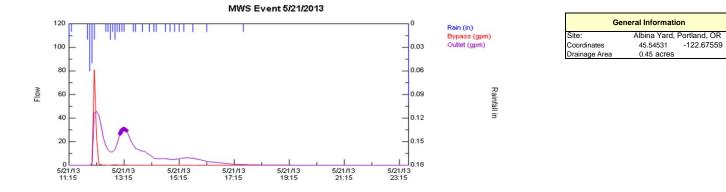


Precipitation Information									
	Goal	Result	QA	Notes					
Precipitation Total (in)	≥0.15	0.17							
Precipitation Duration (hr)	≥1	4.8							
Max Precip. Intensity (in/5 min)	NA	0.08							
Mean Precip. Intensity (in/hr)	0.03	0.04							
Antecedent Dry Period (hr)	≥6	416.8							

		Sampling	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	20				
% Storm Sampled	≥75	59		peak flow sa	ample	
Sampling Duration (hr)	≤36	0				
		Flow Inf	ormatio	on		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	47.6		47.6		
Duration (hr)	NA	10.6		9.2		
Volume (gal)	NA	1422.0		439.8		

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Sample Results - Flow Composite									
	Units	IN	QA	OUT	QA	MDL	notes	%	6 Reduction
Total Phosphorus	mg/L								NA
Ortho-Phosphorus	mg/L	0.11		0.05	U	0.050			56
Hardness	mg/L	47.2		53.2		2.0			-12.7
Total Suspend Solids	mg/L	251.0		20.8		8.0			92
Total Kjedahl Nitrogen	mg/L	2.95		1.12		0.40			62
Nitrate + Nitrite	mg/L	1.12		0.62		0.05			45.1
pH	std units	7.32		7.41					-1
Copper Total	ug/L	29.90		15.50		0.100			48
Copper Dissolved	ug/L	12.00		10.30		0.100			14
Lead Total	ug/L	35.80		3.71		0.0200			90
Lead Dissolved	ug/L	0.14		0.27		0.0200			-93
Zinc Total	ug/L	310.00		42.50		0.500			86
Zinc Dissolved	ug/L	71.50		22.40		0.500			69
Sediment < 1 µm	%	5.60		2.80					50
Sediment 1 - 3.9 µm	%	3.20		0.70					78
Sediment 3.9 - 62.5 µm	%	28.30		15.20					46
Sediment 62.5 - 125 µm	%	47.10		37.40					21
Sediment 125 -250 µm	%	5.10		0.10					98
Sediment 250 -500 µm	%	6.20		20.20					-226
Sediment > 500 µm	%	4.60		23.70					-415
Total Sediment	mg/L	277.0		20.3		1.2			93
Sample Results - Grab									
	Units	IN	QA	OUT	QA	MDL	notes		
Fecal Coliform	MPN/100 ml								NA
E. Coli	MPN/100 ml								NA
Total Petroleum Hydrocarbons -Diesel	mg/L								NA
Total Petroleum Hydrocarbons -Oil	mg/L								NA
Oil and Grease	mg/L								NA



	Precipitation Inf	Precipitation Information								
	Goal	Result	QA	Notes						
Precipitation Total (in)	≥0.15	0.43								
Precipitation Duration (hr)	≥1	6.3								
Max Precip. Intensity (in/5 min)	NA	0.06								
Mean Precip. Intensity (in/hr)	0.03	0.07								
Antecedent Dry Period (hr)	≥6	67.0								

		Sampling	Informa	tion		
	Goal	Result	QA	notes		
Number of Aliquots	≥10	12				
% Storm Sampled	≥75	12		peak flow sa	ample	
Sampling Duration (hr)	≤36	0				
		Flow Inf	ormatio	on		
	Goal	Treated	QA	Bypass	QA	notes
Max Discharge (gpm)	NA	45.6		45.6		
Duration (hr)	NA	12.4		7.6		
Volume (gal)	NA	3521.6		542.7		

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Sample Results - Flow Composite									
	Units	IN	QA	OUT	QA	MDL	notes	% Reduction	
Total Phosphorus	mg/L	0.21		0.10		0.01		53	
Ortho-Phosphorus	mg/L	0.06		0.05	U	0.050		19	
Hardness	mg/L	28.4		34.4		2.0		-21.1	
Total Suspend Solids	mg/L	79.0		20.5		5.0		74	
Total Kjedahl Nitrogen	mg/L	1.11		0.82		0.40		26	
Nitrate + Nitrite	mg/L	0.33		0.10		0.05		68.3	
pH	std units	7.65		7.57				1	
Copper Total	ug/L	15.00		9.50		0.100		37	
Copper Dissolved	ug/L	7.60		5.60		0.100		26	
Lead Total	ug/L	16.60		6.01		0.0200		64	
Lead Dissolved	ug/L	0.14		0.13		0.0200		7	
Zinc Total	ug/L	113.00		33.90		0.500		70	
Zinc Dissolved	ug/L	34.90		13.60		0.500		61	
Sediment < 1 µm	%	5.70		42.40				-644	
Sediment 1 - 3.9 µm	%	2.30		13.80				-500	
Sediment 3.9 - 62.5 µm	%	20.60		0.00				100	
Sediment 62.5 - 125 µm	%	48.80		0.00				100	
Sediment 125 -250 µm	%	0.20		0.00				100	
Sediment 250 -500 µm	%	13.40		22.40				-67	
Sediment > 500 µm	%	9.00		21.40				-138	
Total Sediment	mg/L	62.9		19.8		1.0		69	
Sample Results - Grab									
	Units	IN	QA	OUT	QA	MDL	notes		
Fecal Coliform	MPN/100 ml							NA	
E. Coli	MPN/100 ml							NA	
Total Petroleum Hydrocarbons -Diesel	mg/L							NA	
Total Petroleum Hydrocarbons -Oil	mg/L							NA	
Oil and Grease	mg/L							NA	