

FIRST DEFENSE[®] TESTING USING MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION PROTOCOL UTILIZING OK-110 FEED SAND

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1. INTRODUCTION

Hydro International (Hydro) has a full-scale testing facility at its headquarters in Portland, Maine. This facility is comprehensive and allows testing of the First Defense[®] and other Dynamic Separators to be done under controlled conditions to comply with different laboratory testing protocols.

Hydro has conducted testing of a 4-ft diameter First Defense[®] at its facility using the Maine DEP protocol for laboratory testing. This report presents the results of this testing which involved the use of U.S. Silica grade OK-110 foundry sand as the feed material. The results obtained confirm the ability of the 4-ft First Defense[®] to remove greater than or equal to 80% of the feed material at 320 gpm.

The above performance conforms to the Maine DEP's 60% Total Suspended Solids (TSS) removal rating criteria and this report is submitted to Maine DEP in advance of a request for witness testing and verification prior to formal approval of the 60% rating.

2. LAB TEST FACILITY DESCRIPTION

The Hydro test facility consists of a 23,300-gallon clean water storage reservoir equipped with a Flygt submersible pump to provide feed water. The test unit is a 4-ft diameter First Defense[®] with a 12-inch inlet. The First Defense[®] is connected to the pump delivery with 12-inch diameter PVC pipe-work that incorporates clear standpipes, as well as a valved bypass, which directs excess flows back to the reservoir. The delivery line is fitted with a Hershey VP-820 gearbox butterfly valve along with a variable frequency drive (VFD) for accurate flow control. The overflow from the First Defense[®] is sent back to the reservoir for re-circulation via a 12-inch PVC pipe.

Water and sand are mixed in a 60-gallon barrel to create a sand-slurry, which is fed into the test unit via the inlet piping. The sand-slurry is injected into the 8-inch inlet pipe upstream of the First Defense[®] by a Watson-Marlow peristaltic pump.

A grab sample valve is incorporated in the inlet piping of the First Defense[®], and this consists of a simple 6-inch diameter gate valve with a T-handle. An automatic sampler is located upstream from the feed standpipe to sample background Total Suspended Solids concentrations in the feed from the clean water storage reservoir. The automatic sampler is a Sigma 900 portable sampler that takes about 700 ml per sample.

An ISCO UniMag Magnetic Flowmeter is located in the 8-inch diameter inlet piping upstream from the inlet to the First Defense[®] test unit. The underflow from the First Defense[®] test unit is valved to an underflow

collection tank with a weir wall and two baffles for sediment collection after a test. A clean-out port at the base of the First Defense[®] allows for sediment collection and rinsing.

Materials and equipment used in the TSS analysis included:

- Distilled water, spray bottles, and containers
- Calibrated scales
- 47mm diameter glass fiber ProWeigh Filters with a 1.5 µm pore size
- Welch-Thomas vacuum pump
- Millipore Frit Glass base and stopper for 47mm filters
- VWR Scientific Products 1370 forced air oven
- A W.S. Tyler RX-29 ROTAP sieve shaker for the sieve analysis of sand

An arrangement drawing of the test facility is included in Appendix A and photographs showing aspects of the test set-up and equipment are included in Appendix B.

3. LABORATORY TESTING PROTOCOL

3.1 Flow Calibration

The First Defense[®] was tested at the designed treatment flow rate. This flow rate was 320 gpm.

Flow was measured using the ISCO UniMag Magnetic Flowmeter System which has an accuracy of plus/minus 0.5% of flow rate for mean velocities of 1 ft/s and greater. This equates to a minimum flow rate of 156 gpm for an 8-inch pipe.

The flow rate was also verified by an alternative measurement technique using volumetric, time-to-fill calculations.

The test sand slurry inflow was regulated through a peristaltic pump and was introduced into the inlet pipe via a tube into the feed standpipe. The slurry concentration was continuously stirred in the 60 gallon feed barrel with a rotating stir rod and propeller on a drill motor. The TSS concentrations from the influent samples were in a range of 136 to 299 mg/l and averaged 225 mg/l overall.

3.2 System Equilibrium

The 4-ft diameter First Defense[®] test unit has an effective treatment volume equal to:

 $V=\pi \cdot r^2 \cdot h$; r = 2 ft, h = 4.4 ft V = 55.29 ft

- where r = radius of treatment unit,

h = distance between the invert of the inlet and elevation of maximum storage capacity of the First Defense[®].

The theoretical residence time is equal to the amount of time it takes one (1) unit volume to pass through the system at a given flow rate assuming plug flow conditions (no underflow). The residence times for our experiments were based on the volume between the sampling points. The residence time was calculated by dividing this volume by the flow rate through the system. To ensure that equilibrium conditions had been established, four (4) residence times passed before sampling commenced.

3.3 Sampling

Six (6) sets of samples were collected at 1-minute intervals from the inlet and outlet via grab sampling. Sample volumes were a minimum of 630 ml and averaged 715 ml. Automatic samples for determining background concentrations were also taken corresponding to the 6 inlet samples thus giving a total of 18 samples per test.

For example, for a test at a flow rate of 320 gpm, 4 unit volumes were allowed to pass before sampling to ensure equilibrium conditions. This meant that the first influent was sampled at 5:13 min/sec and the first effluent at 6:31 min/sec, after the start of the test. This reflects the 78.28 seconds residence time for that flow rate. The second samples were taken 1 minute after the first at 6:13 and so on.

To ensure there was no buildup at the gate valve and to ensure representative sampling, the valve was purged seconds before a sample was taken so that a more accurate and representative reflection of the influent stream was sampled.

4. LABORATORY TESTING PROCEDURE

The following is an outline description of the testing procedure.

4.1 Test

- 1. Start with a clean First Defense[®] and clean water in the reservoir.
- 2. Accurately weigh out 4 lbs. of OK-110 influent feed sand. Fill the slurry feed tank with 45 gallons of clean water.
- 3. Take a sieve sample of the feed sand. The sieve analysis shows the consistency of feed sand used for each micron category to minimize variability in test results.
- 4. Make sure the bypass valve and the control valve are fully opened for unrestricted flow. Make sure the clean-out port is closed on the First Defense[®] and the underflow valve is closed. Make sure the influent grab sample valve is closed.
- 5. Start the pump and watch for the First Defense[®] to overflow into the reservoir and the flow rate to stabilize.
- 6. Adjust the flow rate using the VFD to the target rate of 320 gpm. (This flow rate was verified with at least 3 time-to-fill volumetric tests.)
- 7. Start the stirring motor in the slurry feed barrel and then introduce the sand into the barrel.
- 8. Turn on the peristaltic pump and automatic sampler.
- 9. Once sand slurry flow enters the pipe, start the automatic sampler and timer. The automatic sampler will take blank samples at 1-minute intervals corresponding with the influent sample times.
- 10. After 4 residence times have passed (i.e. 5:13 min/sec), take the first influent grab sample. Note: At 5:03 min/sec a purge or flush is performed by quickly opening and closing the valve immediately before taking the sample.
- 11. Take effluent sample 1 residence time (6:31) after influent sample (giving 5 residence times from sand introduction).
- 12. Take 6 sets of samples at 1-minute intervals. This yields a total of 18 samples.
- 13. Stop the sampling and test. Stop the pumps, stirring motor, and automatic sampler.
- 14. Drain the unit, flush it twice, clean and prepare for another test.
- 15. Analyze samples using an equivalent standard to the TSS Test Method 2 Filtration in ASTM, 1999, D 3977-97. Specifically, the Standard Methods 19th Ed 1995 for the Examination of Water and Wastewater prepared and published by the American Public Health Association (APHA), American Water Works Association (AWWA), and Water Environment Federation (WEF) chapter 2-2540 D Total Suspended Solids Dried at 103-105 deg C was used.

4.2 Calculation of Removal Efficiency

The average removal efficiency was calculated using:

(Mean inflow TSS concentration – Mean outflow TSS concentration) / Mean inflow TSS concentration

5. RESULTS AND DISCUSSION

After performing 3 tests at 320 gpm flow rate, the efficiency from the TSS analysis showed removal efficiencies equal to or greater than 80%. The observed removal efficiency range was 89.4 – 96.9 % with an average influent concentration of 225mg/l and an average effluent concentration of 14 mg/l.

The results show that the 4-ft First Defense[®] achieves greater than 80% TSS removal efficiencies with OK-110 sand at a flow rate of 320 gpm using the recommended protocol. The effects of blanks on influent and effluent concentrations are negligible and are not reported.

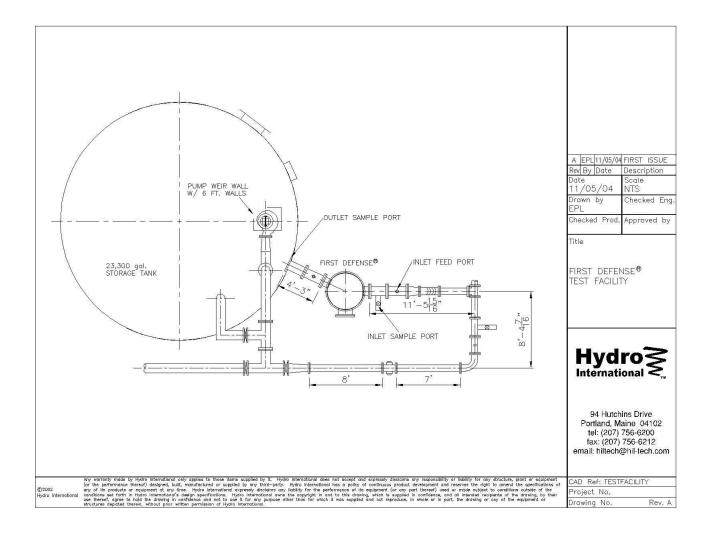
A simple Dixon Q Test was performed for every 6 sample-set to determine whether the data included any outliers within a 95% confidence interval. A statistical Dixon Q test was chosen to determine whether there is a determinate (systematic) or indeterminate (random) error in the data. This check showed that the influent and effluent data had no samples as outliers for a 95% confidence interval. The average influent sample was 224.688 mg/l and the average effluent sample was 14.346 mg/l, which shows an average removal efficiency of 93.66% within a 95% confidence interval.

See Appendix C for test data.

6. ACKNOWLEDGEMENT

Hydro International would like to acknowledge and thank the Maine Technology Institute (MTI) for providing some funding to assist in the development of the First Defense[®]. We also acknowledge the Maine DEP for providing us the opportunity to participate in the laboratory testing protocol and appreciate the ME DEP for establishing the protocols to provide a uniform basis for the evaluation of the performance of all proprietary stormwater treatment systems.

Appendix A Lab Arrangement Diagram



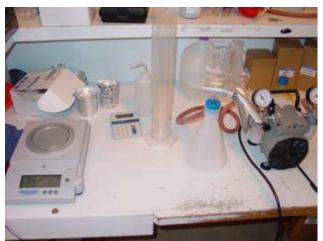
Appendix B Lab Photographs



First Defense



FD Outlet Into Test Tank



TSS Lab, Scale, Vacuum Pump



Slurry feed set-up



Volumetric Time-To-Fill Tank





Forced Air Dryer and Scale



UNIMAG Flow meter



Watson-Marlow Peristaltic Pump



Sigma Automatic Sampler



Control Valve



Flygt Submersible Pump

Appendix B (pg 2)



Influent Sample Valve (Gate)



FD Internal Components



FD Cleanout Port

Appendix B (pg 3)

Appendix C Test Data

OK 110 Sand Testing

	Tar	get Flow Rate =	20	l/s	26-Oct-04		
	Peristaltic	Pump Speed =	80	rpm	Test 60		
	И	/eight of Sand =	4	lb			
	Vo	lume of Water =	45	gallons			
				Combined	Combined Dried Mass (a)		
	Sample	Volume (mL)	Volume (L)	empty Mass (g)	Combined Dried Mass (g)	Δ Mass (mg)	mg/L
	<u>0</u> 1	690	0.690	2.65	2.744	<u>94</u>	136.2319
F	2	725	0.725	2.658	2.782	124	171.0345
é	3	630	0.630	2.621	2.75	129	204.7619
INFL UENT	4	745	0.745	2.605	2.786	181	242.9530
Ž	5	665	0.665	2.603	2.745	142	213.5338
	6	665	0.665	2.602	2.784	182	273.6842
	AVG	686.6667	0.6867			142.00	205.7331
				Combined			
	0				Combined Dried Mass (g)		
	Sample	Volume (mL)	Volume (L)	(g)		Δ Mass (mg)	mg/L
L	1	830	0.830	2.598	2.619	21	25.3012
N.	2	855	0.855	2.586	2.591	5	5.8480
Ë	3	875	0.875	2.596	2.617	21	24.0000
EFFLUENT	4	860	0.860	2.645	2.661	16	18.6047
Ш	5	770	0.770	2.597	2.61	13	16.8831
	6	850	0.850	2.585	2.615	30	35.2941
	AVG	840.0000	0.8400			17.67	21.8096

Total Efficiency =	89.399%
Efficiency Sample 1 =	81.428%
Efficiency Sample 2 =	96.581 %
Efficiency Sample 3 =	88.279%
Efficiency Sample 4 =	92.342%
Efficiency Sample 5 =	92.093%
Efficiency Sample 6 =	87.104%

OK 110 Sand Testing

	Tar	get Flow Rate =	20	l/s	1-Nov-04	ŀ	
	Peristaltic	Pump Speed =	80	rpm	Test 65	5	
		/eight of Sand =		lb			
	Vo	lume of Water =	45	gallons			
				Combined			
					Combined Dried Mass (g)		
	Sample	Volume (mL)	Volume (L)	(g)	(3)	Δ Mass (mg)	mg/L
	1	725	0.725	2.752	2.946	194	267.5862
F N	2	790	0.790	2.747	2.927	180	227.8481
INFL UENT	3	700	0.700	2.754	2.936	182	260.0000
FL	4	645	0.645	2.741	2.872	131	203.1008
Ś	5	785	0.785	2.829	2.95	121	154.1401
	6	705	0.705	2.849	2.977	128	181.5603
	AVG	725.0000	0.7250	1		156.00	228.0191
				Combined			
	Commu				Combined Dried Mass (g)		
	Sample	Volume (mL)	Volume (L)	(g)	2.2.12	Δ Mass (mg)	mg/L
F	1	820	0.820	2.838	2.846	8	9.7561
N	2	685	0.685	2.724	2.726	2	2.9197
S	3	775	0.775	2.709	2.715	6	7.7419
EFFLUENT	4	775	0.775	2.724	2.731	7	9.0323
Ш	5	815	0.815	2.758	2.77	12	14.7239
	6	690	0.690	2.846	2.85	4	5.7971
	AVG	760.0000	0.7600			6.50	7.0494

Total Efficiency =	96.908 %
Efficiency Sample 1 =	96.354 %
Efficiency Sample 2 =	98.719%
Efficiency Sample 3 =	97.022 %
Efficiency Sample 4 =	95.553 %
Efficiency Sample 5 =	90.448 %
Efficiency Sample 6 =	96.807 %

OK 110 Sand Testing

Target Flow Rate =	20 l/s
Peristaltic Pump Speed =	80 rpm
Weight of Sand =	4lb
Volume of Water =	45 gallons

Sample

1

1-Nov-	04
Test	66

Combined Empty Mass Combined Dried Mass (g) Volume (mL) Volume (L) (g) Δ Mass (mg) 710 0.710 2.756 2.968 212 730 0.730 2.751 2.945 194 ~ ~~

5	2	730	0.730	2.751	2.945	194	265.7534
Ш	3	785	0.785	2.755	2.99	235	299.3631
F	4	760	0.760	2.74	2.924	184	242.1053
N	5	655	0.655	2.825	2.933	108	164.8855
	6	725	0.725	2.847	3.019	172	237.2414
	AVG	727.5000	0.7275			184.17	268.6109

Combined

Empty Mass Combined Dried Mass (g)

					Complified Dried Mass (g	1)	
	Sample	Volume (mL)	Volume (L)	(g)		Δ Mass (mg)	mg/L
	1	750	0.750	2.838	2.851	13	17.3333
ž	2	710	0.710	2.718	2.727	9	12.6761
UEN	3	885	0.885	2.71	2.72	10	11.2994
Ц	4	855	0.855	2.723	2.732	9	10.5263
ΕĽ	5	850	0.850	2.759	2.772	13	15.2941
	6	790	0.790	2.844	2.856	12	15.1899
	AVG	806.6667	0.8067			11.00	13.4050

Total Efficiency =	95.010%
Efficiency Sample 1 =	94.195 %
Efficiency Sample 2 =	95.230 %
Efficiency Sample 3 =	96.226 %
Efficiency Sample 4 =	95.652 %
Efficiency Sample 5 =	90.724%
Efficiency Sample 6 =	93.597 %

mg/L

298.5915

DIXON Q TEST	f	or 95% conf	idence Q6=0	0.621			
TEST RUN	I	NFLUENTS:	6 samples a	arranged lowe	est to highest		
	1	136.232	171.035	204.762	213.534	242.953	273.684
Q calculated:		0.2532011	0.2453729	0.0638186	0.2778497	0.2140311	0.2235762 all < Q6 = no outliers
	2	154.140	181.56	203.101	227.848	260	267.586
Q calculated:		0.2417009	0.1898789	0.1898789	0.218139	0.0668688	0.0668688 all < Q6 = no outliers
	3	164.886	237.241	242.105	265.753	298.592	299.363
Q calculated:		0.5380474	0.0361698	0.0361698	0.1758516	0.0057333	0.0057333 all < Q6 = no outliers
Average Influents:		224.688					
DIXON Q TEST	f	or 95% conf	idence Q6=0	0.621			
TEST RUN	E	EFFLUENTS	: 6 samples	arranged low	est to highes	t	
	1	5.848	16.883	18.605	24	25.301	35.294
Q calculated:		0.3747538	0.3747538	0.0584799	0.0441826	0.0441826	0.339367 all < Q6 = no outliers
	2	2.92	5.797	7.742	9.032	9.756	14.724
Q calculated:		0.2437309	0.1647747	0.1647747	0.0613351	0.0613351	0.4208743 all < Q6 = no outliers
	3	10.526	11.299	12.676	15.19	15.294	17.333
Q calculated:		0.1135596	0.1135596	0.2022918	0.0152784	0.0152784	0.2995446 all < Q6 = no outliers
Average Effluents:		14.346					