## Appendix 8-A

## **EXAMPLE BMP DESIGN CHECKLISTS**

## **Table of Contents**

## APPENDIX SECTION HEADINGS

8-A.1.0	INTRODUCTION	8-A-2
8-A.2.0	ROOFTOP DISCONNECTION: DESIGN CHECKLIST	8-A-3
8-A.3.0	SHEET FLOW TO VEGETATED FILTER AREAS AND CONSERVED OPEN SPACE: DESIGN CHECKLIST	8-A-7
8-A.4.0	GRASS CHANNELS: DESIGN CHECKLIST	8-A-12
8-A.5.0	SOIL COMPOST AMENDMENTS: DESIGN CHECKLIST	8-A-17
8-A.6.0	VEGETATED ROOF: DESIGN CHECKLIST	8-A-20
8-A.7.0	RAINWATER HARVESTING: DESIGN CHECKLIST	8-A-24
8-A.8.0	PERMEABLE PAVEMENT: DESIGN CHECKLIST	8-A-29
8-A.9.0	INFILTRATION PRACTICES: DESIGN CHECKLIST	8-A-35
8-A.10.0	BIORETENTION PRACTICES: DESIGN CHECKLIST	8-A-41
8-A.11.0	DRY SWALES: DESIGN CHECKLIST	8-A-51
8-A.12.0	WET SWALES: DESIGN CHECKLIST	8-A-58
8-A.13.0	FILTERING PRACTICES: DESIGN CHECKLIST	8-A-65
8-A.14.0	CONSTRUCTED WETLANDS: DESIGN CHECKLIST	8-A-72
8-A.15.0	WET PONDS: DESIGN CHECKLIST	8-A-93
8-A.16.0	EXTENDED DETENTION PONDS: DESIGN CHECKLIST	8-A-113
8-A.17.0	REFERENCES	8-A-133

## 8-A.1.0. INTRODUCTION

Design and plan review checklists provide general guidance, for both the designer and plan reviewer, regarding the proper design of BMPs. Some items listed on the checklists may not apply to every design, so it is up to the designer to indicate items as "*not applicable*" (or "*NA*") where appropriate. Similarly, the reviewer must be able to distinguish which items are required, based on the local conditions or requirements, and verify the status of those items.

These checklists can be used as tools to provide designers with the necessary information needed to develop an approvable plan, as well as to provide the plan review authority with a consistent review procedure. The various "basin" checklists (Constructed Wetlands, Wet Pond, and Extended Detention Basin) have items included that reflect design criteria in Appendices A through E of the document entitled *Introduction to the New Virginia Stormwater Design Specifications*, found on the Virginia Stormwater BMP Clearinghouse web site at the following URL:

#### http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html

These appendices address a number of design issues common to basin-type practices, such as the sediment forebay, earthen embankment, principal spillway, emergency spillway, and pond landscaping.

## 8-A.2.0. ROOFTOP DISCONNECTION: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

#### **Plan Status**

Approved	Legend:	Complete
Not Approved	-	Inc Incomplete/Incorrect
		<u>N/A</u> - Not Applicable

Compensatory device type (include if the pervious area flow path is less than the required minimum length): (NOTE: See the separate plan review checklist for the compensatory device)

- Dry Well (Micro-Infiltration, Stormwater Design Specification No. 8)
- French Drain (Micro-Infiltration, Stormwater Design Specification No. 8)
- Amended Soils (Stormwater Design Specification No. 4)
- □ Rain Garden (Micro-Bioretention, Stormwater Design Specification No. 9)
- Stormwater Planter (Micro-Bioretention, Stormwater Design Specification No. 9, Appendix A))
- Other:

#### I. SUPPORTING INFORMATION

Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design (infiltration basin, infiltration trench, etc.).

- Provide a site map showing the location of this BMP and showing:
  - \_\_\_\_\_ Facility area and any compensatory devices
  - Contributing drainage area (CDA) boundaries and acreage
  - Areas of the site compensated for in water quality calculations
- \_\_\_\_\_ Provide topography of the site
- Provide a soil map for the site
  - Provide soil boring logs with Unified Soils Classifications, showing:
    - \_\_\_\_\_ Depth to seasonal high groundwater table (minimum 2 ft. 4 ft. below the design bottom of the facility)
      - Depth to bedrock (minimum 2 ft. 4 ft. below the design bottom of the facility)
    - Soil suitability for infiltration (HSG A or B soils or use soil amendments)
  - If located in Karst environment, any provide additional geophysical investigation and recommendations

#### **II. COMPUTATIONS**

#### A. Hydrology

- Provide runoff curve number determinations (re- and post-developed conditions) with worksheets.
- Provide time of concentration (pre- and post-developed conditions), with worksheets.
- Provide hydrograph generation (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### **B.** Hydraulics

- \_\_\_\_\_ Specify assumptions and coefficients used.
- Hydraulic head required = 1-3 ft. for Micro-Infiltration and Micro-Bioretention
- Provide a stage-storage table and curve
- Show that compensatory devices are able to drain within 48 hours following a storm.

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - When soil amendments are used in the downspout discharge flow path, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information

Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
 Show the layout and dimensions of the BMP(s)

### 1. Simple Rooftop Disconnection

- \_\_\_\_\_ Maximum rooftop area treated = 1,000 sq. ft.
- \_\_\_\_\_ Longest flow path (roof/gutter) = 75 ft.
- Disconnection length = longest flow path, but no less than 40 ft.
- Distance downspouts are extended from buildings or foundations = 5 ft. for simple foundations if grade is < 1% (15 ft. in karst areas)

### 2. Rooftop Disconnection to Micro-Infiltration (Dry Well or French Drain)

- Maximum rooftop area treated = 250 to 2,500 sq. ft.
- Runoff reduction sizing based on Stormwater Design Specification #8
- Observation well NOT required
- Soil test/boring required = 1 per practice
- Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient

#### 3. Rooftop Disconnection to Micro-Bioretention (Rain Garden, Stormwater Planter, etc.)

- Maximum rooftop area treated = 1,000 sq. ft.
- Type of inflow to secondary practice = sheet flow or roof leader
- Runoff reduction sizing based on a bioretention surface area = 5% of roof area (Level 1) or 6% of roof area (Level 2); for Stormwater Planters, an infiltration planter is sized to store a minimum of 1/2-inch of runoff from the contributing roof area
- \_\_\_\_\_ Observation well NOT required
- Underdrain and gravel layer = Required for Level 1; Optional for Level 2, depending on soils (refer to Stormwater Design Specification No. 9, Table 2)
- \_\_\_\_\_ Soil test/boring required = 1 per practice, but only when an underdrain is NOT used
- \_\_\_\_\_ Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient
- \_\_\_\_\_ Stormwater filter planters can be placed right next to the building; infiltration planters must be placed a minimum of 10 ft. from the building

#### B. BMP Section Views & Related Details

#### 1. Simple Rooftop Disconnection

- Disconnection slope = < 2% (or < 5% with specified turf reinforcement)
- \_\_\_\_\_ Distance downspouts are extended from buildings or foundations = 5 ft. for simple foundations if grade is < 1% (15 ft. in karst areas)
- Pre-treatment = external (leaf screens, etc.)

#### 2. Rooftop Disconnection to Micro-Infiltration (Dry Well or French Drain)

- Recommended maximum depth = 3 ft.
- Minimum soil infiltration rate = 0.5 in./hr.
- Observation well NOT required
- \_\_\_\_\_ Pre-treatment = external (leaf screens, grass filter strip, etc.)
- \_\_\_\_\_ Soil test/boring required = 1 per practice
- \_\_\_\_\_ Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient

#### 3. Rooftop Disconncection to Micro-Bioretention (Rain Garden, Stormwater Planter, etc.)

- \_\_\_\_\_ Type of inflow to secondary practice = sheet flow or roof leader
- Minimum soil infiltration rate = 0.5 in./hr. (or use underdrain)
- \_\_\_\_\_ Observation well NOT required
- \_\_\_\_\_ Pre-treatment = external (leaf screens, etc.)
- Underdrain and gravel layer = Required for Level 1; Optional for Level 2, depending on soils (refer to Stormwater Design Specification No. 9, Table 2)
- \_\_\_\_\_ Stormwater filter planters must have an overflow pipe installed to prevent water from spilling over the side when excess rainfall occurs
- Minimum filter media depth = 18 in. for Level 1; 24 inches for Level 2; for a stormwater planter, 30 in. for an infiltration planter, and a min. 18 in. for a filter planter
- Media source = mixed on site consistent with Stormwater Design Specification No. 9; planting media should have an infiltration rate of at least 2 in./hr., and the sand/gravel on the planter bottom should have a rate of at least 5 in./hr.
- \_\_\_\_\_ Soil test/boring required = 1 per practice, but only when an underdrain is NOT used
- Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient
- \_\_\_\_\_ Stormwater filter planters can be placed right next to the building; infiltration planters must be placed a minimum of 10 ft. from the building

#### C. Landscape Plan (perimeter)

- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
- \_\_\_\_\_ Specify preservation measures for existing vegetation
  - Ensure that topsoil / planting soil is included in the final grading
- \_\_\_\_\_ The construction contract should include a *Care and Replacement Warranty* to ensure that new vegetation is properly established and survives during the first growing season following construction.

#### **D.** Construction Notes

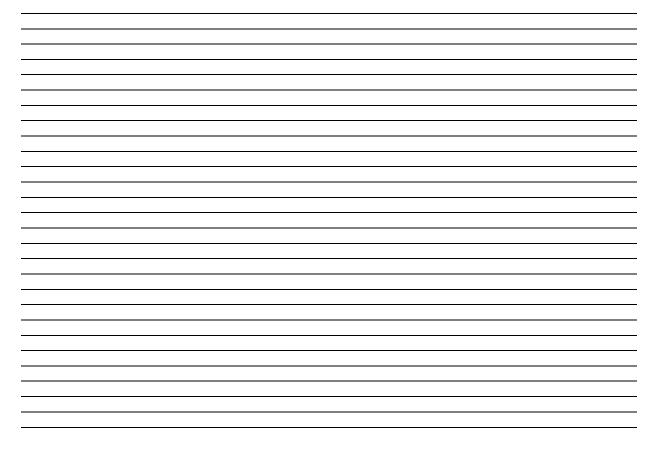
Construction sequence for BMP(s) and E&S controls:

- \_\_\_\_\_ Install applicable temporary E&S control measures.
- \_\_\_\_\_ Convey base flow around secondary practice while it is being constructed.
- Prepare the bottom surface of the stone reservoir,
- \_\_\_\_\_ Lay down filter fabric, if applicable.
- \_\_\_\_\_ Install french drain tile, if applicable.
- \_\_\_\_\_ Place aggregate for dry well or french drain.

- Install overflow and underdrain, if applicable.
- \_\_\_\_\_ Place bioretention media, if applicable.
- For other compensatory BMP(s), see the plan review checklists for those practices
- Install temporary and permanent stabilization measures
- E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
    - \_\_\_\_\_ Include a Maintenance Narrative which describes the long-term maintenance requirements.

Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure property owner awareness, access for inspections and maintenance, and that downspouts remain disconnected.

#### IV. COMMENTS



By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.3.0. SHEET FLOW TO VEGETATED FILTER AREAS AND CONSERVED OPEN SPACE: DESIGN CHECKLIST

Plan Submission Date		
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
BMP Designer		Phone Number
General Contractor		Phone Number
Signature and stamp of lice certification	ensed professi	onal design consultant and owner
Plan Status		
Approved	Legend:	📃 - Complete
Not Approved		<u>Inc.</u> - Incomplete/Incorrect <u>N/A</u> - Not Applicable
Control device type:	Rece	iving filter area:
Engineered Level Spreader (ELS)		Vegetated filter area (amended soils
Level Spreader with vegetated lip		with dense turf cover or herbaceous
Gravel Diaphragm (GD)		cover, shrubs and trees
		Forested/vegetated buffer/open space
. ,		(undisturbed soils and native veg.)
□ Other:		Other:
Facility Type: Level 1	L	evel 2
I. SUPPORTING INFORMATION		
		ater management strategy, describing how
	in, and stating all	assumptions made in the design (infiltration
basin, infiltration trench, etc.).		
Provide a site map showing locatio		
Facility area, control device		
Contributing drainage area Topography	(CDA) boundaries	s and acreage
Areas of the site compensation	ated for in water a	uality calculations
Show the location of boundary spre		
		Spreader at the top of a conserved open
space filter area		
	Engineered Leve	I Spreader at the top of a vegetated filter
strip AND a Permeable Be		

- Provide a soil map for site and area of facility
- Provide soil boring logs with Unified Soils Classifications

#### **II. COMPUTATIONS**

#### A. Hydrology

- Provide runoff curve number determinations (pre- and post-developed conditions), with worksheets.
- Provide time of concentration (pre- and post-developed conditions), with worksheets.
- Provide a hydrograph generation (pre- and post-developed condition) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### B. Hydraulics

- \_\_\_\_\_ Specify assumptions and coefficients used.
- Provide a stage-storage table and curve
- \_\_\_\_\_ Show that compensatory devices are able to drain within 48 hours following a storm.

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
- When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information (see example graphics in Design Specification No. 2)

- \_\_\_\_\_ Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- \_\_\_\_\_ Show the layout and dimensions of the BMP(s)
- \_\_\_\_\_ Maximum flow length = 150 ft. from adjacent *pervious* area OR 75 ft. from adjacent *impervious* area
  - Show location of perimeter protection of Conserved Open Space(s) and note that no grading or heavy equipment access is allowed except for temporary disturbances associated with incidental utility construction, restoration operations, or management of nuisance vegetation

#### 1. If Soils Are Amended

\_\_\_\_\_ Show the full length and width of any area of amended soils

#### 2. Engineered Level Spreader

\_\_\_\_\_ Avoiding concentrated flows:

- Length of ELS lip = 13 lin. ft. per each 1 cfs of inflow (min. 13 lin. ft.; max 130 lin. ft.) for vegetated filter strips or for undisturbed conserved open space with at least 90% veg. cover (per Section 6.2 of the Design Specification)
- Length of ELS lip = 40 lin. ft. per 1 cfs for forested or reforested filter areas
  Overflow/bypass to a reinforced swale designed to convey all peak flows greater than the water quality design storm (1-inch rainfall)

#### 3. Gravel Diaphragm

\_\_\_\_\_ Show the location, if applicable, at top of veg. filter area or conserv. open space slope

#### 4. Permeable Berm

- \_\_\_\_\_ Show the location, if applicable, at the toe of the vegetated filter area slope
- Show the location of the outlet pipe (or gravel lens with perforated pipe) through berm

#### B. BMP Section Views & Related Details (see example graphics in Design Specification No. 2)

Topographic conditions meet minimum slope and width requirements

- \_\_\_\_\_ The first 10 ft. of filter must be 1-2% slope in all cases
- \_\_\_\_\_ 0.5% 3% slope for conserved open space or 1% 4% slope for veg. filter strip = minimum 35 ft. filter width
- \_\_\_\_\_ 3% -6% slope for conserved open space or 4% 6% slope for veg. filter strip = minimum 50 ft. filter width
- \_\_\_\_\_ 6% 8% slope for veg. filter strip = minimum 65 ft. width

#### 1. If Soils Are Amended

\_\_\_\_ Note the depth to which soil compost amendments must be incorporated

#### 2. Engineered Level Spreader

- Avoiding concentrated flows:
  - Length of ELS lip = 13 lin. ft. per each 1 cfs of inflow (min. 13 lin. ft.; max 130 lin. ft.) for veg. filter strips or for undisturbed conserved open space with at least 90% veg. cover (per Section 6.2 of the Design Specification)
  - Length of ELS lip = 40 lin. ft. per 1 cfs for forested or reforested filter areas Overflow to reinforced swale if ELS designed for 1-in./hr. storm
- Section through the ELS system, including the forebay or ELS channel/trench located above the ELS, consistent with the Design Specification (No. 2)
- \_\_\_\_\_ Detail showing any temporary or permanent biodegradable fabric or matting (EC-2, or EC-3) employed to stabilize steeper slopes
- Ends of ELS tied back into the natural slope to prevent scouring around the ends

#### 3. Gravel Diaphragm

- Show a section through the gravel diaphragm, if used, at top of veg. filter area or conserv. open space slope, consistent with the Design Specification (No. 2)
- Filter fabric, stone and other materials should be consistent with the Design Spec

#### 4. Permeable Berm

- \_\_\_\_\_ Show a section through the permeable berm at toe of veg. filter area slope, consistent with the Design Specification (No. 2)
- \_\_\_\_\_ Note the filter media composition and other materials, which should be consistent with the Design Specification

#### C. Landscape Plan

- \_\_\_\_\_ There should be NO grading or clearing of native vegetation within conserved open space area; invasive species may be removed, if the locality approves
- Provide specifications for any compost amendments used and depth of incorporation (see Stormwater Design Specification No. 4) soil amendments should NOT be incorporated until after the gravel diaphragm or level spreader are installed
- Ensure that planting specifications for the conserved open space or vegetated filter areas are consistent with the Stormwater Design Specification No. 2.
- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native vegetation
- \_\_\_\_\_ Specify preservation measures for existing vegetation
- Ensure that topsoil / planting soil is included in the final grading
- The construction contract should include a *Care and Replacement Warranty* to ensure that new vegetation is properly established and survives during the first growing season following construction.

#### D. Construction Notes

- Construction sequence for BMP(s) and E&S controls:
- The filter area should be clearly marked off before construction begins to prevent construction traffic from compacting the area
- Install applicable temporary E&S control measures.
- Convey base flow around secondary practice while it is being constructed.
- Install temporary and permanent stabilization measures.

In addition:

#### 1. Conserved Open Space

- Perimeter of Conserved Open Space should be protected by acceptable signage, super silt fence, snow fence, chain link fence, orange safety fence or other comparable methods
- Note that no clearing, grading or heavy equipment access is allowed except for temporary disturbances associated with incidental utility construction, restoration operations or management of nuisance vegetation
- Note (if applicable) that (1) construction of the gravel diaphragm or engineered level spreader shall not commence until the contributing drainage area has been stabilized and perimeter E&S controls have been removed and cleaned out; and (2) stormwater should not be diverted into the filter area until the gravel diaphragm and/or level spreader are installed and stabilized.
- \_\_\_\_\_ Note that any light grading necessary at the filter area boundary must be done with tracked vehicles to prevent compaction

#### 2. Vegetated Filter Strips

- Note that only vehicular traffic necessary for the filter strip construction should be allowed within 10 feet of the filter strip boundary
- \_\_\_\_\_ Note that if existing topsoil is stripped during grading, it shall be stockpiled and stabilized for later use
- \_\_\_\_\_ Note that construction runoff shall be directed away from the proposed filter strip area, using perimeter silt fence or, preferably, a diversion dike.
- Note (if applicable) that (1) construction of the gravel diaphragm or engineered level spreader shall not commence until the contributing drainage area has been stabilized and perimeter E&S controls have been removed and cleaned out; and (2) stormwater should not be diverted into the filter area until the gravel diaphragm and/or level spreader are installed and stabilized and until the turf cover is dense and well-established.
- Note that amended soils should be hand-raked to the most level slope without using heavy equipment, but that any light grading necessary to achieve desired elevations and slopes must be done with tracked vehicles to prevent compaction.
- Note that compost amendments and/or topsoil shall be incorporated evenly across the filter strip area, stabilized with seed, and, if slopes exceed 3%, protected by biodegradable E&S control matting or blankets (EC-2).
- E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
    - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including installation/maintenance of signage; removal and disposal of trash, debris and sediment accumulations; and mowing.
  - Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure property owner awareness, access for inspections and maintenance, and that the filter area is remains intact and fully functional.
    - Provide sufficient facility access from the public ROW or roadway to both the filter area and accessory practices.

## **IV. COMMENTS**

By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.4.0. GRASS CHANNELS: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

#### **Plan Status**

Approved	Legend:		- Complete
Not Approved	-	Inc.	- Incomplete/Incorrect
		N/A	<ul> <li>Not Applicable</li> </ul>

Type of pretreatment facility:

- Check Dams (channel flow)
- Tree Check Dams (channel flow)
- Grass Filter Strip (sheet flow)
- Gravel or Stone Diaphragm (sheet flow)
- Gravel or Stone Flow Spreaders (concentrated flow)
- Other: \_\_\_\_\_
- None

#### I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design (infiltration basin, infiltration trench, etc.).
- Provide a site map of the location of this BMP showing:
  - Grass channel area and per-treatment practice
    - \_\_\_\_\_ Contributing drainage area (CDA) boundaries and acreage, not to exceed 5 acres for any individual grass channel
  - \_\_\_\_\_ Topography
    - Areas of the site compensated for in water quality calculations
- \_\_\_\_\_ Provide a soil map for site and area of the grass channel
- Provide soil boring logs with Unified Soils Classifications
- \_\_\_\_\_ Pre-treatment is recommended for grass channels to dissipate energy, trap sediments and slow down runoff velocity.
- \_\_\_\_\_ Minimum depth to bedrock in karst areas is 18 inches.
- \_\_\_\_\_ Minimum depth to groundwater in coastal areas is 12 inches.
- In areas of steep terrain, terracing a series of grass channel cells may work on slopes of from 5% to 10% grade, where the drop in elevation between check dams should be no more than 18 inches and the check dams should be armored on the down-slope side with suitably sized stone to prevent erosion.

#### **II. COMPUTATIONS**

- A. Hydrology
- Provide runoff curve number determinations (pre- and post-developed conditions), with worksheets.
  - Provide time of concentration (pre- and post-developed conditions), with worksheets.

Provide hydrograph generation (pre- and post-developed condition) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

- **B.** Hydraulics
  - Show that compensatory devices are able to drain within 48 hours following a storm.
  - Grass channels are designed based on peak flow rate the maximum flow velocity of the channel must be less than 1 foot per second during a 1-inch water quality storm event
- The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity requirements)
  - Verify hydraulic capacity using Manning's Equation or an accepted equivalent method, such as erodibility factors and vegetal retardance
    - \_\_\_\_\_ The flow depth for the peak treatment volume (1-inch rainfall) should be maintained at 3 inches or less
    - Manning's "n" value for grass channels should be 0.2 for flow depths up to 4 inches, decreasing to 0.03 at a depth of 12 inches (which applies to the 2-year and 10-year storms if an on-line application
    - Peak flow rates for the 2-year and 10-year frequency storms must be non-erosive or subject to site-specific analysis of the channel lining material and vegetation
    - \_\_\_\_\_ The 10-year peak flow rate must be contained within the channel banks, with a minimum of 6 inches of freeboard
  - \_\_\_\_\_ Specify assumptions and coefficients used.
- Provide a stage-storage table and curve
- Calculations for peak flow depth and velocity should reflect any increase in flow along the length of the channel, as appropriate. If a single flow is used, the flow at the outlet should be used.
- The hydraulic residence time should be a minimum of 9 minutes for the treatment volume (1inch rainfall) design storm. If flow enters the channel at multiple locations, a 9-minute minimum hydraulic residence time should be demonstrated for each entry point, using equations in Stormwater Design Specification No. 3.
  - The minimum length may be achieved with multiple swale segments connected by culverts with energy dissipators

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
- When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)
  - \_\_\_\_\_ Specific sizing/dimensions determined from criteria in Stormwater Design Specification No. 3.
- Grass channels should NOT be used as stand-alone water quality treatment systems in Coastal Plain settings, due to poor nutrient and bacteria removal rates (Dry Swales or Wet Swales are a better choice).

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information (see example graphics in Design Specification No. 2)

- Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
  - Layout and dimensions of the grass channel and pre-treatment device(s)
- The bottom width of the channel should be from 4 to 8 feet. If a channel must be wider, incorporate benches, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion along the channel bottom.
- Grass channels should generally be aligned adjacent to and the same length (minimum) as the contributing drainage area identified for treatment.

In karst areas, the channel may have off-line cells and must be connected to an adequate discharge point.

In coastal areas, the channel may have off-line cells and must be connected to the ditch system.

#### B. BMP Section Views & Related Details (see example graphics in Design Specification No. 2)

- \_\_\_\_\_ Topographic conditions must meet minimum slope and width requirements.
- Grass channels should be designed with a trapezoidal or parabolic cross-section. A parabolic shape is preferred for aesthetic, maintenance and hydraulic reasons.
- The channel side slopes should be 3H:1V or flatter. For ease of mowing and routine maintenance, side slopes should be no steeper than 4H:1V. Flatter slopes are encouraged to aid in pre-treatment of sheet flows entering the channel.
- The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; Longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity requirements). A minimum slope of 0.5% must be maintained in karst or coastal areas to ensure positive drainage.
- **C.** Check Dams (generally discouraged in karst areas, where flow spreaders flush with the ground surface and spaced along the channel length may be useful in spreading flows more evenly across the channel width)
  - Check dams should be should configured with elevated driveway culverts or be composed of wood, concrete, rip-rap, or other non-erodible material, underlain with filter fabric conforming to the following standards:
    - \_\_\_\_\_ Needled, non-woven, polypropylene geotextile.
    - Grab Tensile Strength (ASTM D4632): ∃ 120 lbs.
    - \_\_\_\_\_ Mullen Burst Strength (ASTM D3786): ∃ 225 lbs./sq. in.
    - \_\_\_\_\_ Flow Rate (ASTM D4491): ∃ 125 gpm/sq. ft.
      - \_\_ Apparent Opening Size (ASTM D4751): ∃ US #70 or #80 sieve
- Wood used for check dams should consist of pressure-treated logs or timbers, or water-resistant tree species such as cedar, hemlock, swamp oak or locust.
- It is necessary to compute check dam materials, based on the surface area and depth used in the design computations.
- Check dams should be spaced (based on the channel slope) as needed to increase residence time and provide adequate storage for the treatment volume (1-inch rainfall) or any additional volume attenuation requirements. The ponded water at a downhill check dam should not touch the toe of the upstream check dam.
- The maximum desired check dam height is 12 inches (for maintenance purposes). However, for challenging sites, a maximum of 18 inches can be allowed, with additional design elements to ensure the stability of the check dam and the adjacent and underlying soils The average ponding depth throughout the channel should be 12 inches.
- Soil plugs serve to help minimize the potential for blow-out of the soil media underneath the check dams due to hydrostatic pressure from the upstream ponding. Soil plugs are appropriate for Grass Channels (1) on slopes of 4% or greater, or (2) with check dams equal to or greater than 12-inches in height.
- Armoring may be needed at the downstream toe of the check dam to prevent erosion.
- Check dams must be firmly anchored into the side-slopes to prevent outflanking; check dams must also be anchored into the channel bottom so as to prevent hydrostatic head from pushing out the underlying soils.
- \_\_\_\_\_ Check dams must be designed with a center weir sized to pass the channel design storm peak flow (10-year storm event for man-made channels).
- \_\_\_\_\_ Check dams should be designed and constructed so as to facilitate easy mowing of the channel.
  - Each check dam should have a weep hole or similar drainage feature so it can dewater after storms.
- Individual channel segments formed by check dams or driveways should generally be at least 25 to 40 feet in length.

#### D. Diaphragms

Pea gravel used to construct pre-treatment diaphragms should consist of washed, open-graded, course aggregate between 3 and 10 mm in diameter and must conform to local design standards.

#### E. Soil Compost Amendments

- The compost-amended strip should extend over the length and width of the channel bottom, and the compost should be incorporated to a depth as outlined in Stormwater Design Specification No. 4.
- \_\_\_\_\_ The amended area will need to be rapidly stabilized with perennial, salt tolerant grass species.
- For grass channels on steep slopes, it may be necessary to install a protective biodegradable geotextile fabric to protect the compost-amended soils. Care must be taken to consider the erosive characteristics of the amended soils when selecting an appropriate geotextile.
- For redevelopment or retrofit applications, the final elevation of the grass channel (following compost amendment) must be verified as meeting the original design hydraulic capacity.

#### F. Landscape Plan

- Choose grass species that can withstand both wet and dry periods as well as relatively highvelocity flows. Taller and denser grasses are preferable, though the species is less important than the ability to provide effective stabilization. (Consult Standard and Specification 3.32 of the Virginia E&S Control Handbook for a list of acceptable grass species.)
- For channels adjacent to roads and parking lots, salt-tolerant species should be chosen.
- Use grass seed, NOT sod.
- \_\_\_\_\_ Seed at a density that achieves a 90% turf cover by the end of the second growing season.
- Provide specifications for any compost amendments used, including the depth of incorporation (see Stormwater Design Specification No. 4)
- Provide immediate stabilization of the channel bed and banks using a biodegradable erosion control fabric (netting or mats) durable enough to last at least two growing seasons (conforming to Standard and Specification 3.36 of the Virginia E&S Control Handbook).
- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
   Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
- Specify preservation measures for existing vegetation
- Ensure that topsoil / planting soil is included in the final grading
- The construction contract should include a *Care and Replacement Warranty* to ensure that new vegetation is properly established and survives during the first growing season following construction.

#### G. Construction Notes

- \_\_\_\_\_ Ideally, grass channels should be constructed during months that are best for establishing turf cover without irrigation (February 15 April 15; September 15 November 15).
- Applicable temporary E&S control measures
- Ideally, grass channels should remain outside the limit of disturbance during construction to prevent soil compaction by heavy equipment. If this is not feasible, temporary E&S controls such as dikes, silt fences and similar measures should be integrated into the channel design. Specifically, barriers should be installed at key check dam locations, and E&S control fabric should be used to protect the channel bottom.
- Grass channel construction should begin only after the entire contributing drainage area has been stabilized with vegetation. Sediment accumulation must be removed during final grading to achieve the design cross-section.
- \_\_\_\_\_ Stormwater flows should be bypassed and not allowed into the grass channel until the bottom and side slopes are stabilized.
  - Construction sequence for BMP(s) and E&S controls:
    - \_\_\_\_\_ Grade the channel to the final dimensions shown on the plan.

- Install check dams, driveway culverts and internal pre-treatment features as shown on the plan
- Fill material used to construct the check dams should be placed in 8- to 12-inch lifts and compacted to prevent settlement. The top of each check dam should be constructed level at the design elevation.
- (Optional) Till the bottom of the channel to a depth of 1 foot and incorporate compost amendments according to Stormwater Design Specification No. 4.
- Add soil amendments as needed, hydro-seed the bottom and banks of the channel, and peg in erosion control fabric or blanket where needed. After initial planting, a biodegradable E&S control fabric should be used, conforming to Standard and Specification 3.36 of the VESCH.
- Prepare planting holes for any trees and shrubs, then plant materials as shown in the landscaping plan and water them weekly in the first two months.

## H. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements for the grass channels and all their components, including removal and disposal of trash, debris and sediment accumulations; and mowing.
- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure property owner awareness, access for inspections and maintenance, and that the grass channels remain intact and fully functional.
- Provide sufficient facility access from the public ROW or roadway to the grass channels for inspection and maintenance.

#### IV. COMMENTS

By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.5.0. SOIL COMPOST AMENDMENTS: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

#### Plan Status

Approved	Legend:	Complete
Not Approved	-	Inc Incomplete/Incorrect
		<u>N/A</u> - Not Applicable

#### I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design (infiltration basin, infiltration trench, etc.).
- Provide a site map showing location of area(s) where soil compost amendments are to be applied
- \_\_\_\_\_ Show the contributing drainage area (CDA) boundaries and acreage, not to exceed 5 acres for any individual Grass Channel
- Provide topography of the site
- Provide a soil map for site and area of soil amendments
  - Provide two soil tests (pre-construction to determine soil properties to a depth 1 foot below the proposed amendment area, and 1 week after amendments have been incorporated):
    - First test done every 5,000 sq. ft. to determine bulk density, porosity, pH, salts, and soil nutrients (to determine potential drainage problems and what amendments are needed)
       Second test done to determine any further nutritional requirements, pH, adjustment, or organic matter adjustments are need for plant growth (done in conjunction with the final construction inspection to ensure tilling or subsoiling has achieved design depths).
    - Provide soil boring logs with Unified Soils Classifications
- Show the areas of the site compensated for in water quality calculations
  - The following are site conditions where soil compost amendments should NOT be used:
    - Existing soils have high infiltration rates (HSG A and B), although amendments may be needed were B-soils are mass-graded, in order to maintain the runoff reduction rate.
      - The water table or bedrock is within 1.5 feet of the soil surface
      - The slope exceeds 10%; terracing may be needed on slopes between 5% and 10%
    - \_\_\_\_\_ Existing soils are saturated or seasonally wet
    - Incorporation of compost would harm tree roots (keep amendments outside the tree drip line)
      - \_\_\_\_\_ The downhill slope runs toward an existing or proposed building foundation.
      - \_\_\_\_\_ The contributing impervious surface area exceeds the surface are of the amended soils.
    - The area under consideration will be used for snow storage
    - \_ The following site conditions involve special considerations:
      - In karst areas, ensure the soil pH is adjusted as needed to conform to the pre-existing soil conditions found in limestone-dominated areas.
      - \_\_\_\_\_ In coastal areas, depth to groundwater should be a minimum of 2 feet to ensure the entire depth of soil amendment will not become saturated

#### **II. COMPUTATIONS**

#### A. Hydrology

Provide runoff curve number determinations (pre- and post-developed conditions), with worksheets.

Provide time of concentration (pre- and post-developed conditions), with worksheets.

Provide hydrograph generation (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### B. Hydraulics

\_\_\_\_ Specify assumptions and coefficients used.

Provide a stage-storage table and curve

#### C. Water Quality

Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)

When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information (see example graphics in Design Specification No. 2)

- \_\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- Show the layout and dimensions of the soil amendment area
- \_\_\_\_\_ Topographic conditions must meet minimum slope requirements

#### B. Landscape Plan

- \_\_\_\_\_ Use grass seed, NOT sod.
- Seed at a density that achieves a 90% turf cover by the end of the second growing season.
- Provide material specifications for any compost amendments used, including the depth of incorporation (see Stormwater Design Specification No. 4)
- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
- \_\_\_\_\_ Specify preservation measures for existing vegetation
- Ensure that topsoil / planting soil is included in the final grading
- The construction contract should include a *Care and Replacement Warranty* to ensure that new vegetation is properly established and survives during the first growing season following construction.

#### C. Construction Notes

- \_\_\_\_ For rooftop disconnection, vegetative filter strip or grass channel applications, see the checklists for those practices. For larger, more expansive areas, the following criteria apply:
  - \_\_\_\_\_ Ideally, the soil amendment area should remain outside the limit of disturbance during construction to prevent soil compaction by heavy equipment.
  - Prior to construction, the proposed soil amendment area should be deep-tilled to a depth of 2 to 3 feet using a tractor and subsoiler with two deep shanks (curved metal bars) to create rips perpendicular to the direction of flow.
  - \_\_\_\_\_ A second deep tilling to a depth of 12-18 inches is needed after final building lots have been graded.
  - It is important to have dry conditions at the site prior to incorporating compost.
  - Incorporate the acceptable compost mix into the soil using a rototiller or similar equipment at the volumetric rate of 1 part compost to 2 parts soil.

- \_\_\_\_\_ The site should be leveled and seed or sod used to establish a vigorous grass cover.
- \_\_\_\_\_ Lime and/or irrigation may be needed initially to help the grass grow quickly.
- Areas of compost amendments exceeding 2500 sq. ft. should employ simple E&S control measures, such as silt fence, to reduce the potential for erosion and to trap sediment.
- D. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - If the soil amendment area exceeds 10,000 sq. ft., provide a standard BMP Maintenance Agreement, indicating person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Record a deed restriction or other enforceable mechanism, including GPS coordinates of the area, to ensure the infiltrating areas are not disturbed or converted to other uses.
- \_\_\_\_\_ To educate the property owner, provide a maintenance narrative which describes the short-term and long-term maintenance requirements.
- Provide sufficient facility access from the public ROW or roadway to the grass channels for inspection and maintenance.

#### **IV. COMMENTS**

Ву:	Date:
Dy.	Dale.

## 8-A.6.0. VEGETATED ROOF: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

#### **Plan Status**

Approved Not Approved	Legend:       Image: Complete         Inc.       -       Incomplete/Incorregion         N/A       -       Not Applicable	ect
Facility Type: Level 1	Level 2	

Type of Vegetated Roof:

- Extensive (shallower planting media, herbaceous vegetation)
- □ Intensive (planting media typically twice as deep, can have shrubs and trees among vegetative cover typically qualify as Level 2 roofs)

#### I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design (infiltration basin, infiltration trench, etc.).
- \_\_\_\_\_ Show the location of the BMP roof on the site map.
- A structural engineer, architect or other qualified professional should be involved with the design to ensure that the building has enough structural capacity to support the additional weight of the water held in the planting media (typical fully saturated *extensive* vegetated roof loads range from 15-25 lbs./sq. ft.).
- Adequate access to the roof must be provided to deliver and stockpile construction materials and perform routine maintenance. The roof hatch or trap door should be not less than 16 sq. ft. in area with a minimum dimension of 24 inches.
- Vegetated roofs can be applied to most roof surfaces, although concrete roof decks are preferred. Certain roof materials, such as exposed treated wood and uncoated galvanized metal, are not appropriate decks for vegetated roofs.
- \_\_\_\_\_ Vegetated roof surfaces should not be located near rooftop electrical or HVAC systems.
- \_\_\_\_\_ Vegetated roof designs should comply with the Virginia Uniform Statewide Building Code with respect to roof drains and emergency overflow devices.
- \_\_\_\_\_ Vegetated roofs can be used as retrofits, based on the roof area, age, structural capacity and accessibility, as well as the owner's ability to provide necessary maintenance.
  - Special design adaptations:
    - In karst areas, direct the roof downspout discharges at least 15 feet away from the building to minimize the risk of sinkhole formation
    - \_\_\_\_\_ In coastal areas, designers should choose plant materials that tolerate drought and salt spray.
    - In cold climates, it is important to match the plant materials to the plant hardiness zone, design the roof so the growing media is not subject to freeze-thaw cycles, and provide greater structural capacity to account for winter snow loads.
    - Where acid rain falls, growing media can neutralize the pH of the rainfall; however, it is not clear whether the acid rain will impair plant growth or leach minerals from the growing media.

#### I. COMPUTATIONS

#### A. Hydrology

- Determine the runoff curve number (pre-development and post-development conditions), providing the worksheets; post-development recommendations for 4 design storm events are provided in Table 5.1 of Stormwater Design Specification No. 5.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method), providing the results.

#### B. Hydraulics

- The drainage layer below the growing media should be designed to convey the 10-year storm without backing up water into the growing media, conveying the flow to an outlet or overflow system such as a traditional rooftop drainage system with inlets set slightly above the elevation of the vegetated roof surface.
- \_\_\_\_\_ Specify assumptions and coefficients used.
- Provide a stage-storage table and curve.

#### C. Water Quality

Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information (see example graphics in Design Specification No. 2)

Layout and dimensions of the vegetated roof.

- A 2-foot wide vegetation-free zone is recommended along the perimeter of the roof (may be a 1-foot setback for very small vegetated roof applications), with a 1-foot vegetation-free zone around all roof penetrations, to act as a firebreak.
- The roof design should include strategically located non-vegetated walkways (e.g., permeable paver blocks) to allow for easy access to the roof for weeding and making spot repairs.
- Size (surface area) to address the required treatment volume per equation in Stormwater Design Specification #5 or per manufacturer recommendations.
  - Show the layout of the outlet or overflow system and locations of roof drains

#### B. BMP Section Views & Related Details (see example graphics in Design Specification No. 2)

- Vegetated roofs are composed of up to 8 different systems or layers, which may consist of a wide variety of materials and differ in cost, performance and structural load. Proprietary designs are available. The entire system must be assessed to meet the design requirements (see Stormwater Design Specification No. 5).
- \_\_\_\_\_ Roof drains immediately adjacent to the growing media should be boxed and protected by flashing extending at least 3 inches above the growing media, to prevent clogging.

#### C. Planting Plan

- \_\_\_\_\_ The planting plan must be prepared by a landscape architect, botanist or other professional experienced with vegetated roofs.
- Plant materials are selected based on local climate (plant hardiness zone) and design objectives, as well as toleration of the difficult growing conditions on building rooftops. Selected plants should be fire-resistant and able to withstand heat, cold and high winds; the primary groundcover for most vegetated roof installations is a hardy, low-growing succulent such as *Sedum, Delosperma, Talinum, Semperivum,* or *Hieracium*. Plant choices can be much more diverse for deeper *intensive* vegetated roof systems.

- The species selection and planting plan layout should reflect the building location in terms of its height, exposure to wind, snow loading, heat stress, sun orientation, and shading by trees or surrounding buildings. Note: Most effective vegetated roof plant species will *NOT* be native to Virginia or the Chesapeake Bay watershed.
- \_\_\_\_\_ Species should also be selected to match the expected rooting depth of the growing media.
- Accent plants may be included to provide seasonal diversity and color.
- Due to limited vegetated roof plant nurseries in the region, designers should order plant materials 6-12 months prior to the expected planting date and to have the plants contract-grown.
- \_\_\_\_\_ The planting period extends from spring to early fall, but it is important to allow plants enough time to root thoroughly prior to the first killing frost.
- Typically, most vegetated roofs will not require supplemental irrigation, except for temporary irrigation during dry months as the roof vegetation becomes established.
- Plants can be established using cuttings, plugs, mats and, more rarely, seedlings or containers; some vendors also provide mats, rolls, or proprietary roof planting modules.
- Initial fertilization may be needed to support growth, using a slow-release fertilizer with minerals.
- Hand weeding must be performed regularly during the first 2 years.
- The construction contract should include a *Care and Replacement Warranty* that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.

#### **D.** Construction Notes

- \_ An experienced installer should be retained to construct the vegetated roof system.
- \_\_\_\_\_ The roof system should be constructed in sections to facilitate easier inspection and maintenance.
- Construction sequence:
  - Construct the roof deck with the appropriate slope and material.
    - Install the waterproofing method according to the manufacturer's specifications.
    - Conduct a flood test to ensure the system is water-tight, by placing 2 inches of water over the membrane for 48 hours.
    - \_\_\_\_\_ Add the additional system components, taking care not to damage the waterproofing.
    - \_\_\_\_\_ Drain collars and protective flashing should be installed to ensure free flow of excess stormwater.
    - \_\_\_\_\_ The growing media should be mixed prior to delivery to the site.
    - The media should be spread evenly over the filter fabric surface and covered until planting, to prevent weeds from growing.
    - Sheets of exterior-grade plywood can be laid over the growing media to accommodate foot or wheelbarrow traffic (however, limit this traffic to reduce compaction).
    - \_\_\_\_\_ Moisten the growing media prior to planting.
    - Plant the vegetation in accordance with the planting plan of ASTM E2400.
    - Water the plants immediately after planting and routinely during the establishment period and, especially, during the first summer (generally 12-18 months for full establishment).

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components.
- Record a deed restriction or other enforceable mechanism, including GPS coordinates of the area, to ensure the the vegetated roof is not converted to a conventional roof surface (in order to maintain this component of the site's stormwater management plan).
- Avoid the use of herbicides, insecticides and fungicides, because their presence can result in deterioration of the waterproof membrane and contaminate runoff discharged from the roof.
- Avoid power-washing so that the cleaning agents do not harm the rooftop plant communities.

## **IV. COMMENTS**


By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.7.0. RAINWATER HARVESTING: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

# Signature and stamp of licensed professional design consultant and owner certification

Plan Status Approved Not Approved	Legend:	-	Image: CompleteInc Incomplete/IncorrectN/A- Not Applicable
Secondary BMPs used with Rainwater Harvestin	g:		
Rooftop Disconnection (No. 1)			Storage and release in Foundation
Sheet Flow to Veg Filter/Open Space			Planter (No. 9, Appendix A)

- Sheet Flow to Veg Filter/Open Space (No. 2)
- Grass Channel (No. 3)
- □ Infiltration (No. 8)
- □ Micro-Bioretention (rain garden) (No. 9)

#### I. SUPPORTING INFORMATION

Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design and the purpose for which the harvested rainwater will be used, including any of the following:

Dry Swale (No. 10)

Other: \_\_\_\_\_

Underground infiltration soak-away pit

- Outdoor non-potable uses, including irrigation, car washing, etc.
- Indoor, non-potable uses, such as toilet flushing, fire suppression, etc., assuming building code and health department regulations allow such uses and appropriate regulatory approvals are obtained.
- Indoor, potable uses, including food preparation, drinking water, showers, etc., assuming building code and health department regulations allow such uses and appropriate regulatory approvals are obtained.
- Use of rainwater as a resource to meet on-site demand (above) or design in conjunction with infiltration to promote groundwater recharge
  - Pollutant reduction (realized only due to reduced volume of runoff leaving the site)
  - Reduction in peak flows (realized due to reduced volume of runoff leaving the site)
- \_\_\_\_\_ Show the location of BMP on the site map; adequate space is needed to house the tank and overflow (this is rarely a problem if considered during initial design and site layout).
- \_\_\_\_\_ Underground utilities or other obstructions should be identified prior to determining the final tank location.
  - \_\_\_\_ The plan should identify and provide sufficient details to construct the six primary components of the rainwater harvesting system:
    - \_\_\_\_\_ Roof surface
      - \_\_\_\_\_ The rooftop should be made of smooth, non-porous material with efficient drainage (sloped roof or efficient roof drain system)
      - \_\_\_\_\_ If the harvested rainwater will have potable uses or uses with significant human exposure, ensure that the roofing materials do not leach toxic chemicals.
      - In general, avoid harvesting rainwater from roofs with asphalt sealcoats, tar and gravel, painted roofs, galvanized metal roofs, sheet metal or any material that may contain asbestos or may leach trace metals and other toxic compounds.

Some industrial roof surfaces may be designated as "hot spots," limiting the use and benefits of harvesting the rainwater.

- Collection and conveyance system (e.g., gutters, downspouts and pipes to the stroage tank)
  - \_\_\_\_\_ Runoff should be routed from rooftops to cisterns in closed roof drain systems or storm drain pipes, avoiding surface drainage which could increase contamination of the water
  - \_\_\_\_\_ Aluminum, round-bottom gutters and round downspouts are generally recommended.
  - \_\_\_\_\_ Gutter slopes should be 0.5% for 2/3 of the length and 1% for the remaining 1/3.
  - Gutters should be sized to contain the 1-inch rainfall event (treatment volume) at a rate of 1 inch/hour.
  - If volume control credit is desired for channel protection and flood protection purposes, gutters should be sized to convey 1-year and 10-year design storms.

Pipes connecting the downspouts to the storage tank should have a minimum slope of 1.5% and be sized to convey the intended design storm.

Pre-screening and first flush diverter (filters out sediment, leaves, contaminants and debris).

- Pre-filtration devices that filter out large debris should be low-maintenance or maintenance free (e.g., leaf screens, gutter guards, etc.)
- For larger tank systems, the initial first flush (0.02 0.06 inches of rooftop runoff) must be diverted from the tank and directed to an acceptable nonerodible pervious flow path or secondary BMP for infiltration (preferably the same practice that receives tank overflows).
- A 95% filter efficiency (including the first flush diversion) must be achieved for the 1-inch rainfall event. For the 1-year and 10-year design storms, the filtering must have a minimum efficiency of 90%.
- If **leaf screens** are used, note in the maintenance agreement that they must be cleaned regularly to be effective and maintain flow from the gutters into the storage tank.
- \_\_\_\_\_ If a **roof washer** tank is used just ahead of the storage tank, note in the maintenance agreement that they must be cleaned regularly to be effective.
- A first flush diverter, which filters out small contaminants such as dust, pollen and animal feces, require the ability to actively drain the first flush water volume to a pervious area (filter path) following each rainstorm (this is the preferred pretreatment method if the harvested water is intended for indoor uses).

A **vortex filter** can be used to filter rooftop rainwater for larger rooftop areas.

\_\_\_\_ Storage tank

- \_\_\_\_ The tank volume must be calculated to meet the water demand and the stormwater treatment volume credit objectives.
- Dead storage below the outlet to the distribution system and an air gap at the top of the tank should be added to the total volume. For gravity-fed systems, a minimum of 6 inches of dead storage should be provided. For systems using a pump, the dead storage depth is be based on the pump specifications.
- \_\_\_\_\_ The system should be sealed using a water-safe, non-toxic substance.
- Storage tanks should be opaque or otherwise protected from direct sunlight to inhibit algae growth and should be screened to inhibit mosquito breeding and reproduction.
- The relationship of tank location to site topography should be considered as they relate to all inlet and outlet invert elevations in the system and to the amount of pumping that may be needed. The total elevation drop will be realized beginning from the downspout leaders to the final mechanism receiving gravity-fed discharge and/or overflow from the cistern.
- \_\_\_\_\_ Storage tanks should be placed on native soils or on fill in accordance with the manufacturer's guidelines.

- \_\_\_\_\_ The soil pH must be considered in relation to the material of which the tank/cistern is made.
- \_\_\_\_\_ Storage tanks should be designed to be watertight to prevent water damage when placed near building foundations.
- Rainfall pH must also be considered (Virginia rain tends to be acidic, from 4.5-5.0), due to the risk of leaching metals form the roof surface, tank lining or water laterals to interior connections. Limestone or other neutralizing substances may be added in the tank to buffer acidity.
- Underground storage tanks are most appropriate in areas where the tank can be buried *above* the water table and in a manner that it will not be subject to flooding. If buried *below* the water table, special design features must be employed to prevent the tank from "floating," etc.
- Underground systems should be placed in areas without vehicle traffic and designed to support the overlying sediment and other anticipated loads, or otherwise be designed to support live loads from heavy trucks (this may increase construction costs).
- \_\_\_\_\_ Underground systems should have a standard size manhole or equivalent opening to allow access for cleaning, inspection, and maintenance purposes. The opening must be able to be locked or otherwise secured to prevent unwanted access.
- Distribution system
  - The system should be equipped with an appropriately sized pump that produces sufficient pressure for all end-uses.
- \_\_\_\_\_ The typical pump and pressure tank arrangement consists of a multi-stage centrifugal pump that draws water from the storage tank and sends it to a pressure tank, where it is stored for distribution.
- \_\_\_\_\_ The municipal code may require the separate plumbing to be labeled as non-potable.
- Any hookup to a municipal backup water supply must have a backflow prevention device, subject to local codes, to keep municipal water separate from stored rainwater. This may include incorporating an air gap to separate the two supplies.
- \_\_\_\_\_ Distribution lines must be buried beneath the frost line. If above-ground outdoor pipes are installed, they must be insulated or heat-wrapped to prevent freezing and ensure uninterrupted operation during the winter.
- \_\_\_\_\_ Distribution lines to the building must have shut-off valves that are accessible when snow cover is present.
  - A drain plug or cleanout sump, draining to a pervious area, must be installed to allow the system to be completely emptied.
- \_ Overflow, filter path or secondary runoff reduction practice(s)
  - An overflow mechanism must be included in the system design to handle and individual storm event or multiple events in succession that exceed the capacity of the storage tank.
  - Overflow pipes must have a capacity equal to or grater than the inflow pipe(s) and have a diameter and slope sufficient to drain the storage tank while maintaining an adequate freeboard height.
  - Overflow pipes must be screened to prevent access to the tank by rodents and birds.
  - The filter path should be a pervious or grass corridor that extends from the overflow to the next runoff reduction practice, the street, an adequate existing or proposed channel, or the storm drain system.
  - \_\_\_\_\_ The filter path must be graded with a slope that results in sheet flow conditions.
  - If compacted or impermeable soils are present along the filter path, compost amendments may be necessary (see Stormwater Design Specification #4).

#### **II. COMPUTATIONS**

#### A. Hydrology

- The contributing drainage area is the impervious area draining to the tank, generally only the rooftop surface. Paved surfaces can be included in rare circumstances with appropriate treatment.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
  - Generate hydrographs (re- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### **B.** Hydraulics

- \_\_\_\_\_ The required hydraulic head depends upon the ultimate use/destination of the harvested water.
- \_\_\_\_\_ Specify the assumptions and coefficients used.
- \_\_\_\_\_ Provide a stage-storage table and curve.
- \_\_\_\_\_ Show that compensatory devices are able to drain within 48 hours following a storm.

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA
- The Cistern Design Spreadsheet (explanation and instructions provided in Stormwater Design Specification No. 6) must be used to determine cistern sizing, including the treatment volume requirements, and by extension, pollutant load removal (provide a copy of the spreadsheet calculations)
- IMPORTANT NOTE: In order to adequately address the required design treatment volume, the design specification assumes the practice will achieve a dedicated year-round drawdown. While seasonal uses (such as warm weather irrigation, etc.) may be incorporated into the site design, they are not considered to contribute to the treatment volume credit (for stormwater management purposes) unless a drawdown at an equal or greater rate is also realized during non-seasonal periods (e.g., infiltration during non-irrigation months, etc.). Designing for constant drawdown of the stored water is also important in assuring that the tank will have sufficient storage capacity for future rainstorms.

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information (see example graphics in Design Specification No. 2)

\_ Show the layout and dimensions of the rainwater harvesting system.

- In general, underground tanks should be set at least 10 feet from any building foundation.
- \_\_\_\_\_ Cistern overflow devices should be designed to avoid causing ponding or soil saturation within 10 feet of building foundations.
- \_\_\_\_\_ The roof design should include strategically located non-vegetated walkways (e.g., permeable paver blocks) to allow for easy access to the roof for weeding and making spot repairs.
- Ensure sizing (surface area) sufficient to address the required treatment volume consistent with the equation in Stormwater Design Specification No. 5 or manufacturer recommendations.
  - \_\_\_\_\_ Show the layout of the outlet or overflow system and locations of roof drains

#### B. BMP Section Views & Related Details (see example graphics in Design Specification No. 2)

Show sections through the system and, as appropriate, through system components

#### C. Planting Plan

Provide a planting schedule and specifications (transport / storage / installation / maintenance) Ensure plant selection appropriate for the site's vegetation climatic zone (4-8 in Virginia) The construction contract should include a Care and Replacement Warranty to ensure that new vegetation is properly established and survives during the first growing season following construction.

#### D. Construction Notes

- It is advisable that a single contractor, with a plumbing license and familiar with rainwater harvesting system sizing, installation and placement, install the rainwater harvesting system, outdoor irrigation system, and secondary runoff reduction practices.
- The tank location must be identified on the site and the tank installed.
- All downspouts or roof drains must be routed to pre-screening devices and first flush diverters.
- \_\_\_\_\_ The pre-treatment system must be installed.
- \_\_\_\_\_ Mosquito screens must be installed on all openings.
- \_\_\_\_ The overflow device must be installed and directed, as shown on the plans.
- \_\_\_\_ The catchment area and overflow area must be stabilized.
- The secondary runoff reduction practice(s) must be installed.

#### E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a maintenance narrative describing the purpose of the facility and the property owner's primary responsibilities for long-term maintenance requirements of all its components, require the owner to pay to have the system inspected according to a specified schedule, and authorize the gualifying local program staff to access the property for inspection or corrective action in the event this is not done.
- Record a drainage easement to allow for inspection and maintenance. The easement should include the tank, the filter path, and any secondary runoff reduction practice(s).
- Provide sufficient facility access from public ROW or roadway to facilitate inspection and maintenance.
  - \_\_\_\_\_ If the system is located on a private residential lot, its existence and purpose must be noted on the deed of record.

#### **IV. COMMENTS**

By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.8.0. PERMEABLE PAVEMENT: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number Practice No./Location on Site	
Owner BMP Designer	
General Contractor	
Signature and stamp of licensed profess certification	sional design consultant and owner
Plan Status	
Approved Legend	Complete
Not Approved	Inc Incomplete/Incorrect
	N/A - Not Applicable
	<u></u>
Facility Type: Level 1	Level 2
Type of Pre-Treatment Facility:	
□ Stone diaphragm	
Grass filter strip	
□ Other:	
I. SUPPORTING INFORMATION	
this practice fits into the overall plan, and stating basin, infiltration trench, etc.). Showing the location of the permeable pavemer Facility area Contributing drainage area (CDA) bound Proposed topographic contours Delineation of FEMA 100-year floodplain Areas of the site compensated for in wa	daries and acreage
descriptions (at least one boring must be taker depth where infiltration is designed to occu table/bedrock or karst is identified)	boring logs with Unified Soils Classifications and to confirm the underlying soil properties <i>at the</i> <i>tr</i> , to ensure that depth to the groundwater g to confirm a subsoil infiltration rate of at least one infiltration test per 1,000 sq. ft. of planned er table and bedrock (minimum 2 ft. below the investigation is recommended to ensure the arst impacts (e.g., sinkholes, etc.) and an brane liner covered by 8 to 12 oz./sq. yd. non-
woven geotextile) must be place beneath the ONLY to meet the Level 1 design criteria	permeable pavement, which must be designed

#### **II. COMPUTATIONS**

#### A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### B. Hydraulics

- Verify that 2 to 4 feet of hydraulic head is available to drive flows through the facility
- Verify that the pavement will drain within 48 hours following a storm (minimum 36 hours).
- Specify the assumptions and coefficients used.
- Provide a stage-storage table and curve
- The designer may use the PICP Permeable Design Pro Software to design the pavement, including hydraulics (software available from the Interlocking Concrete Pavement Institute, at <u>www.icpi.org</u>)

#### C. Water Quality

Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information

- \_\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- \_\_\_\_\_ Show the layout and dimensions of permeable pavement facility
- Ensure the proper orientation and slope of the facility, including pre-treatment, to avoid shortcircuiting
  - \_\_\_\_\_ Show the location of the observation well(s)

#### B. BMP Section Views & Related Details

#### 1. Porous Asphalt

- \_\_\_\_\_ Subgrade preparation
- \_\_\_\_\_ Aggregate
  - Bedding layer: 2-inch layer of VDOT No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter)
    - \_\_\_\_\_ Reservoir layer (required to support structural load): VDOT No. 2 open graded course aggregate or equivalent
  - Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter particles)
  - Porous asphalt surface layer
    - Void content: 15% to 20%
    - Thickness: Typically 3 to 7 inches, depending on the traffic load
    - \_\_\_\_\_ Open void fill media: None
  - Underdrains

Observation well (perforated vertical 4 to 6 inch diameter Schedule 40 PVC pipe – AASHTO M 252 – with 3/8-inch diameter perforations at 6 inches on center and a lockable cap, installed flush with the surface) and underdrain pipes, which are of the same material – or equivalent corrugated HDPE may be used for smaller load-bearing applications – installed at a minimum 0.5% slope for the full length of the permeable pavement cell and located no more than 20 feet

from the next pipe. Non-perforated pipe may be used to connect with the storm drain system, and Ts and Ys may be installed, as needed, based on the underdrain configuration. Cleanout pipes should be extended to the surface with vented caps at the Ts and Ys.) Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.

\_\_\_\_ Filter fabric: (Optional) Non-woven, polypropylene geotextile with:

- Grab tensile strength:  $\exists$  120 lbs. (ASTM D4632)
- \_\_\_\_\_ Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
- \_\_\_\_\_ Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
- Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.

#### 2. Pervious Concrete

- \_\_\_\_ Subgrade preparation
- \_\_\_\_\_ Aggregate
  - \_\_\_\_\_ Bedding layer: None
    - Reservoir layer (may not be needed to support structural load, but may be included to increase runoff storage or infiltration): VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Filter layer: 2 to 4 inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter particles)
  - Permeable concrete surface layer
    - Void content: 15% to 25%
    - \_\_\_\_\_ Thickness: Typically 4 to 8 inches
    - \_\_\_\_\_ Compressive strength: 2.8 to 28 Mpa.
    - \_\_\_\_\_ Open void fill media: aggregate
- Underdrains
- Observation well
- Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
  - Grab tensile strength:  $\exists$  120 lbs. (ASTM D4632)
  - Mullen burst strength:  $\exists$  225 lbs./sq. in. (ASTM D3786)
  - \_\_\_\_\_ Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
  - Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.

#### 3. Permeable Interlocking Concrete Pavers (PICP)

- \_\_\_\_\_ Subgrade preparation
- Aggregate
  - Bedding layer: 2-inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Reservoir layer (required to support structural load): VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter particles)
  - \_\_\_ Concrete paver surface layer (must conform to ASTM C936 specifications)
    - \_\_\_\_\_ Surface open area: 5% to 15%
    - Thickness: 3.125 inches for vehicles
    - Compressive strength: 55 Mpa.
    - \_\_\_\_\_ Open void fill media: aggregate

#### Underdrains

Observation well

Filter fabric: (Optional) Non-woven, polypropylene geotextile with:

- \_\_\_\_\_ Grab tensile strength:  $\exists$  120 lbs. (ASTM D4632)
- \_\_\_\_\_ Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
- \_\_\_\_\_ Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
- Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.

#### 4. Concrete Grid Pavers

- \_\_\_\_ Subgrade preparation
- \_\_\_\_ Aggregate
  - Bedding layer: 2-inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Reservoir layer (required to support structural load): VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter particles)
  - \_\_\_ Concrete paver surface layer (must conform to ASTM C1319 specifications)
    - \_\_\_\_\_ Open void area: 20% to 50%
    - Thickness: 3. 5 inches
    - Compressive strength: 35 Mpa.
    - Open void fill media: aggregate, coarse sand, topsoil and grass
- Underdrains
- \_\_\_\_\_ Observation well
  - Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
    - Grab tensile strength:  $\exists$  120 lbs. (ASTM D4632)
    - Mullen burst strength:  $\exists$  225 lbs./sq. in. (ASTM D3786)
    - Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
    - Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.

#### 5. Plastic Reinforced Grid Pavers

- \_\_\_\_ Subgrade preparation
- Aggregate
  - Bedding layer: 2-inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Reservoir layer (required to support structural load): VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
  - Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter particles)
- Concrete paver surface layer
  - \_\_\_\_\_ Void content: Depends on fill material
    - Compressive strength: Varies, depending on fill material
  - Open void fill media: Aggregate, coarse sand, topsoil and grass
  - Underdrains
- Observation well
- Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
  - Grab tensile strength:  $\exists$  120 lbs. (ASTM D4632)
  - Mullen burst strength:  $\exists$  225 lbs./sq. in. (ASTM D3786)

- Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
- Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.

#### C. Landscape Plan (perimeter)

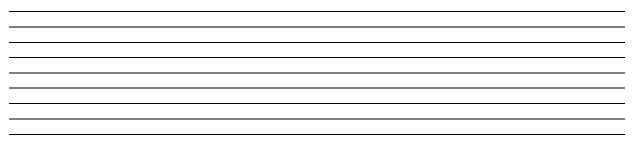
- Where grass is used in grid pavers, include specifications appropriate for the site's vegetation climatic zone (4-8 in Virginia)
- \_\_\_\_\_ Specify preservation measures for existing vegetation surrounding permeable pavement area

#### **D.** Construction Notes

- Permeable pavement areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment. Permeable pavement areas should *not* be used during construction as sites for temporary sediment traps or basins.
- \_\_\_\_\_ Traffic control to avoid tracking mud and fine sediment
- Store materials in a protected area to keep them free from mud, dirt, and other foreign materials.
  - Ensure that pre-treatment structures are properly installed and working effectively.
- \_\_\_\_\_ Construction sequence:
  - Construction inspections should occur before, during and after installation to ensure the permeable pavement installation is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
  - Construction of the permeable pavement facility should begin only *after* site work is completed and the entire contributing drainage area has been stabilized with dense and healthy vegetation.
  - Temporary E&S control measures (typically silt fence) to prevent sediment from moving into the stone base material or onto the pavement surface during construction), to avoid clogging
    - Excavators or backhoes (with arms with adequate extension) should work from the sides to excavate the reservoir layer to its appropriate design depth and dimensions.
      - \_\_\_\_\_ For micro-scale and small-scale installations, excavators should avoid setting up inside the facility footprint to avoid compaction.
      - Where feasible, use the cell construction approach, splitting the proposed permeable pavement area into 500 to 1,000 sq. ft. temporary cells with a 10 to 15 foot earth bridge in between, so the cells can be excavated from the side.
         Excavated material should be place away from the open excavation to avoid
        - jeopardizing the stability of the side walls.
  - Scarify or till the native soils along the bottom and sides of the permeable pavement system to a depth of 3 to 4 inches prior to placing the filter layer or filter fabric.
    - For large scale paving applications with weak soils, the soil subgrade may need to be compacted to 95% of the Standard Proctor Density to achieve the desired load-bearing capacity (effectively eliminating any infiltration function, so this must be addressed during the hydrologic design stage).
  - If used, filter fabric should be installed next along the bottom and sides of the reservoir layer.
    - Filter fabric strips should overlap down-slope by a minimum of 2 feet and should be secured a minimum of 4 feet beyond the edge of the excavation.
    - Where the filter layer extends beyond the edge of the pavement (to convey runoff to the reservoir layer), install an additional layer of filter fabric 1 foot below the surface to prevent sediments from entering the reservoir layer. Do not trim excess filter fabric until the site is fully stabilized.
    - Install the observation well(s) and, if used, install the underdrains.
      - Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth

- \_\_\_\_\_ Check elevations (underdrain inverts, inflow and outflow point inverts, depth of aggregate installations, etc.) and the surface slope.
- Provide a minimum of 2 inches of aggregate above and below the underdrains.
  - \_\_\_\_\_ Underdrains should slope down towards the outlet at a grade of 0.5% or steeper.
- \_\_\_\_\_ Up-gradient ends of underdrains in the reservoir layer should be capped, but *not* the downstream ends.
- \_\_\_\_\_ Where an underdrain pipe is connected to a structure, there must be *no* perforations within 1 foot of the structure.
- Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.
- Moisten and spread 6-inch lifts of the appropriate clean, washed stone aggregate (usually No. 2 or No. 57 stone).
  - Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth.
    - Place at least 4 inches of additional aggregate above the underdrain(s), and then compact it using a vibratory roller in static mode until there is no visible movement of the aggregate.
      - \_ Do not crush the aggregate with the roller.
- \_\_\_\_\_ Install the design depth of bedding layer, depending on the type of pavement to be used.
  - Install paving materials according to manufacturer or industry specifications for the type of pavement to be used (see Stormwater Design Specification No. 7 for specific guidance).
    - \_\_\_\_\_ Make sure the permeable pavement surface is even, that water spreads evenly across it, and the storage bed drains within 36 to 48 hours.
  - Implement any remaining permanent stabilization measures.
  - Log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.
- E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
    - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components.
  - Record a deed restriction or other enforceable mechanism, including GPS coordinates of the area, to ensure the the permeable pavement is not converted to conventional pavement (in order to maintain this component of the site's stormwater management plan).

#### IV. COMMENTS



By: \_\_\_\_\_ Date: \_\_\_\_\_

## 8-A.9.0. INFILTRATION PRACTICES: DESIGN CHECKLIST

Plan Submission Date Project Name	_
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

Plan Status Approved Not Approved	Legend:       Image: Complete         Inc.       - Incomplete/Incorrect         N/A       - Not Applicable	
Facility Type: Level 1	Level 2	
<ul> <li>Hydraulic Configuration:</li> <li>On-line facility</li> <li>Off-line facility (sized to receive only a portion of the Treatment Volume)</li> </ul>	Type of Pre-Treatment Facility:   Sediment forebay (above ground)  Sedimentation chamber  Plunge pool  Stone diaphragm	
Type of Infiltration Facility: ☐ Surface facility (basin) ☐ Subsurface facility	<ul> <li>Grass filter strip</li> <li>Grass channel</li> <li>Other:</li> </ul>	_

#### I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design. Show the location of this BMP on the site map, including:
  - \_ Show the location of this BMP on the \_\_\_\_\_ Facility area
  - Contributing drainage area (CDA) boundaries and acreage (not to exceed 2 acres and as close to 100% impervious as possible)
  - Proposed topographic contours
  - If a basin, the embankment area: centerline principal spillway, emergency spillway, abutments
  - \_\_\_\_\_ Delineation of FEMA 100-year floodplain
  - Areas of the site compensated for in water quality calculations
  - Provide topography for the site area, showing that the slope of the CDA does not exceed 15%.
  - Provide a soil map for site and area of the facility, showing the CDA and facility boundaries (HSG A and B soils are prime locations for infiltration facilities)
  - Provide soil boring locations and soil boring logs with Unified Soils Classifications and descriptions (at least one boring must be taken to confirm the underlying soil properties at the depth where infiltration is designed to occur, to ensure that depth to the groundwater table/bedrock or karst is identified). NOTE: To be suitable, native soils must have a silt/clay content of less than 40% and a clay content of less than 20%. Furthermore, infiltration facilities should not be located above fill soils, and "urban" soils that have been previously disturbed or graded are not good sites for infiltration. Nor should they be located where they will receive regular dry weather flows from sources such as sump pumps or irrigation systems, or any flows from hot spot areas, etc.

- Provide results of soil infiltration rate testing to confirm a subsoil infiltration rate of 0.5 to 1 inch/hour for Level 1 design or 1 to 4 inches/hour for a Level 2 design (the number of infiltration tests should be based on the scale of the planned infiltration facility area see Table 8.3 and Appendix 8-A in Stormwater Design Specification No. 8).
- \_\_\_\_\_ Depth to seasonal high groundwater table and bedrock (minimum 2 ft. below the design bottom of the facility)
- \_\_\_\_\_ NOTE: An EPA UIC permit may be required for a facility exceeding 20,000 sq. ft. if the surface width is less than the maximum depth.
- Avoid installing geotextile filter fabric along the *bottom* of infiltration facilities (causes clogging). A layer of coarse washed choker stone is more effective.
- If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) must be place beneath the infiltration facility. Where karst is present, there must be at least 4 feet of vertical separation between the bottom of the infiltration facility and the karst layer. Furthermore, only micro-scale or small-scale infiltration facilities may be used, and they must be designed *ONLY* to meet the Level 1 design criteria (incorporating an underdrain). NOTE: Bioretention should be preferred to infiltration in karst locations.

#### II. COMPUTATIONS

#### A. Hydrology

- Confirm a soil infiltration rate of 0.5 inch/hour minimum. NOTE: The *design* infiltration should be calculated to be 50% of the measured infiltration rate, to provide a factor of safety.
- A porosity value of 0.40 must be used in the design of stone reservoirs, although a larger value may be used if perforated corrugated metal pipe, plastic pipe, concrete arch pipe, or comparable materials are installed within the reservoir to detain runoff.
- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

#### **B.** Hydraulics

- \_\_\_\_\_ Verify that there is sufficient hydraulic head to drive flows through the facility:
  - 1 to 3 feet for micro-scale infiltration
  - \_\_\_\_\_1 to 5 feet for small-scale infiltration
    - 2 to 6 feet for conventional large-scale infiltration
  - \_\_\_\_\_ The Treatment Volume should be infiltrated or drained from the facility within 36 to 48 hours.
- \_\_\_\_\_ Specify the assumptions and coefficients used.
- \_\_\_\_\_ Provide a stage-storage table and curve.
- Provide storm drainage and hydraulic grade line calculations.

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - Specific sizing/dimensions must be determined from criteria in Stormwater Design Specification No. 8.

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information

- \_\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- Show the layout and dimensions of the infiltration facility
  - Micro-scale infiltration from 250 to 2,500 sq. ft. (dry well, french drain, paving blocks)
  - Small-scale infiltration from 2,500 to 20,000 sq. ft. (infiltration trench)
  - Large-scale conventional infiltration from 20,000 to 100,000 sq. ft. (infiltration trench or basin)
- Show the location and confirm the proper orientation (to prevent short-circuiting) of all conveyance system outfalls into the basin with pre-treatment and outlet protection designed in accordance with the VE&SCH
  - Ensure proper setbacks from building foundations, down-gradient slopes, etc.:
    - 5 feet down-gradient from dry or wet utility lines
    - 5 feet down-gradient and 25 feet up-gradient from building foundations for micro-scale infiltration facilities
    - 10 feet down-gradient and 50 feet up-gradient from building foundations for small-scale infiltration facilities
    - \_\_\_\_\_ 25 feet down-gradient and 100 feet up-gradient from building foundations for large-scale infiltration facilities
    - \_\_\_\_\_ In cold climate areas, 25 feet from roadways to prevent potential frost heaving of the pavement
      - \_\_\_\_\_ 50 feet from septic systems
    - 100 feet from any water supply well
    - 200 feet from down-gradient slopes with greater than 20% grade
  - \_\_\_ Infiltration basin features:
    - \_\_\_\_\_ Top of bank and basin bottom elevations
    - Elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
    - Side slope (H:V) of basin storage area and embankment (upstream and downstream slopes)
    - \_\_\_\_\_ Sediment forebay
      - Maintenance access to the sediment forebay and riser structure
  - \_\_\_\_ Safety fence during construction, but not after completion of construction.
- Location of observation well for facilities larger than micro-scale (perforated vertical 6 inch diameter Schedule 40 PVC pipe AASHTO M 252 with 3/8-inch diameter perforations at 6 inches on center and a lockable cap, installed flush with the ground surface, with one for every 50 feet of length of the infiltration practice) and any underdrain pipes, which are of the same material or equivalent corrugated HDPE may be used for smaller load-bearing applications installed at a minimum 1.0% slope for the full length of the infiltration cell and located no more than 20 feet from the next pipe. Non-perforated pipe may be used to connect with the storm drain system, and Ts and Ys may be installed, as needed, based on the underdrain configuration. Cleanout pipes should be extended to the surface with vented caps at the Ts and Ys.) Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface. NOTE: An underdrain is required only for large-scale conventional infiltration facilities and for micro-scale infiltration facilities on marginal soils (where the underdrain must be elevated. Install non-perforated pipe with one or more caps, as needed from the structure.

#### B. BMP Section Views & Related Details

#### 1. Pre-Treatment Practices

- \_\_\_\_\_ Minimum 2 pre-treatment practices required for micro-scale infiltration facilities, but no minimum pre-treatment volume required.
- \_\_\_\_\_ Minimum 3 pre-treatment practices required for small-scale infiltration facilities, and pretreatment volume is required to be 15% of the Treatment Volume.

Minimum 3 pre-treatment practices required for large-scale conventional infiltration facilities, and pre-treatment volume is required to be 25% of the Treatment Volume. If the facility footprint exceeds 20.000 sq. ft., a surface pre-treatment cell must be provided (e.g., sand filter or dry sediment basin). Pre-treatment facilities designed so exit velocities are non-erosive for the 2-year design storm \_\_\_\_ and evenly distribute runoff flows across the width of the facility (using a level spreader, etc.) In cold climate areas, oversize pre-treatment measures by up to 40% to account for additional sediment load caused by road sanding. 2. Infiltration Basin (also refer to the checklists for Extended Detention Facilities – Section 8-A.16.0 – regarding Earthen Embankments, Principal Spillways, Emergency Spillways, etc.) Best if designed to be off-line, to avoid damage from the erosive velocities of larger storms. Elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms \_ Maximum depth no greater than 1 foot (a maximum of 2 feet if pre-treatment cells are used) Bottom of the basin should be flat (i.e., 0% longitudinal and lateral slopes). A maximum longitudinal slope of 1% is permissible if an underdrain is used. Top of dam elevations: constructed height and settled height (allowing for 10% settlement). Adequate freeboard Top width labeled Elevation of crest of emergency spillway Principal/emergency spillway, with side slopes labeled. Existing ground and proposed improvements profile along center line of embankment \_\_\_\_ Existing ground and proposed improvements profile along center line of principal spillway \_\_\_\_ Typical grading section through the basin \_\_\_\_\_ Typical grading section through the forebay Existing ground and proposed improvements along center line of emergency spillway Dimensions of zones for zoned embankment Foundation Cut Off Trench or Key Trench Materials labeled \_\_\_\_\_ Bottom width (4' minimum, or greater, as specified in the geotechnical report). Side slopes labeled (4H:1V maximum steepness). Depth (4' minimum or as specified in the geotechnical report) 3. Infiltration Trench Dimensions provided Maximum depth: \_\_\_\_\_ 3 feet for micro-scale infiltration facilities \_\_\_\_\_ 5 feet for small-scale infiltration trenches

- 6 feet for large-scale conventional infiltration trenches
  - In cold climate areas, the bottom of the trench should extend below the frost line.
- Bottom of the trench should be flat (i.e., 0% longitudinal and lateral slopes). A maximum longitudinal slope of 1% is permissible if an underdrain is used.
- Aggregate specifications:
  - Reservoir stone must be clean washed VDOT No. 1 Open-Graded Coarse Aggregate (diameter of 3.5 to 1.5 inches) or equivalent.
    - Stone jacket for the underdrain must be clean double-washed VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent, free of all soil fines, installed 3 inches above the underdrain and 12 inches below it.
- Filter fabric installed on the sides of the infiltration facility (to prevent piping) must be non-woven polyprene geotextile with a flow rate of > 110 gpm/sq. ft. (Geotex 351 or equivalent).
- The trench surface can be covered by a 3-inch layer of river stone or pea gravel. Turf is acceptable when there is sub-surface inflow (e.g., a roof leader).

# C. Landscape Plan

- Where grass is used on the infiltration facility surface, include specifications appropriate for the site's vegetation climatic zone (4-8 in Virginia)
- \_\_\_\_\_ Specify preservation measures for existing vegetation surrounding the infiltration area
- Keep adjacent vegetation from forming an overhead canopy above the infiltration facility, in order to keep leaf litter, fruits and other vegetative litter from clogging the stone.

## **D.** Construction Notes

- Infiltration areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment. Infiltration areas should *not* be used during construction as sites for temporary sediment traps or basins, which can clog the base soils with fine sediments.
- Provide traffic control to avoid tracking mud and fine sediment and compacting the soil.
- Store materials in a protected area to keep them free from mud, dirt, and other foreign materials.
- Ensure that pre-treatment structures are properly installed and working effectively. Keep the infiltration facility "off-line" until construction is complete.
- \_\_\_\_\_ Keep the inilitration facility off-line until (
- \_\_\_\_\_ Construction sequence:
  - Construction inspections should occur before, during and after installation to ensure the infiltration facility is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
  - Construction of the infiltration facility should begin only *after* site work is completed and the entire contributing drainage area has been stabilized with dense and healthy vegetation.
  - Temporary E&S control measures (typically super silt fence, diversion berms, etc.) to prevent sediment from moving into the stone base material or onto the pavement surface during construction), to avoid clogging. The plan should indicate the conditions that must be met before runoff may be directed to a conventional infiltration basin.
  - Excavators or backhoes (with arms with adequate extension) should work from the sides to excavate the reservoir layer to its appropriate design depth and dimensions.
    - The floor of the facility should be completely level, but equipment should be kept off the floor to prevent soil compaction.
    - Correctly install filter fabric on the trench sides.
      - Trim large tree roots flush with the sides of the trench to prevent puncturing or tearing of the filter fabric.
    - When laying out the geotextile, the width should include sufficient material to compensate for perimeter irregularities in the trench and for a 6-inch minimum overlap at the top of the trench.
    - \_\_\_\_\_ Tuck filter fabric under the sand layer on the bottom of the trench.
    - Place stones or other anchoring objects on the fabric at the trench sides to keep the trench open during windy periods.
    - Place natural soils in any voids that occur between the fabric and the excavated sides of the trench, to ensure the fabric conforms smoothly to the sides of the excavation.
  - \_\_\_\_\_ Scarify or till the native soils along the bottom and sides of the permeable pavement system to a depth of 3 to 4 inches prior.
  - Spread 6 inches of sand on the bottom as a filter layer.
  - Install and anchor the observation well(s) and, if used, install the underdrains.
    - \_\_\_\_\_ Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth
    - \_\_\_\_\_ Check elevations (underdrain inverts, inflow and outflow point inverts, depth of aggregate installations, etc.) and the surface slope.
    - Provide a minimum of 2 inches of aggregate above and below the underdrains.
    - \_\_\_\_\_ Underdrains should slope down towards the outlet at a grade of 0.5% or steeper.

- Up-gradient ends of underdrains in the reservoir layer should be capped, but not the downstream ends.
- \_\_\_\_ Where an underdrain pipe is connected to a structure, there must be no perforations within 1 foot of the structure.
- \_\_\_\_\_ Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.
- Moisten and spread 1-foot lifts of the appropriate clean, washed stone aggregate (usually No. 2 or No. 57 stone).
  - \_\_\_\_\_ Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth.
  - Place at least 4 inches of additional aggregate above the underdrain(s), and then compact it using a vibratory roller in static mode until there is no visible movement of the aggregate.
    - Do not crush the aggregate with the roller.
  - Use sod to establish a dense turf cover for at least 10 feet on each side of the infiltration facility, to reduce erosion and sloughing. If the vegetation is seeded instead, use native grasses primarily due to their adaptability to the local climate and soil conditions.
  - Implement any remaining permanent stabilization measures.
- Log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, and regular mowing.
- Record a deed restriction or other enforceable mechanism, including GPS coordinates of the area, to ensure that infiltration areas are not converted to other uses.
- Provide sufficient facility access from public ROW or roadway to facilitate inspection and maintenance.

# **IV. COMMENTS**

By: \_\_\_\_\_ Date: \_\_\_\_\_

# 8-A.10.0. BIORETENTION PRACTICES: DESIGN CHECKLIST

Plan Submission Date	
Project Name	—
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

Plan Status Approved Not Approved	Legend:	<ul> <li>Complete</li> <li>Inc Incomplete/Incorrect</li> <li>N/A - Not Applicable</li> </ul>	
Facility Type: Level 1		Level 2	
Hydraulic Configuration: On-line facility Off-line facility		Type of Pre-Treatment Facility: <ul> <li>Sedimentation chamber</li> <li>Plunge pool</li> <li>Stone diaphragm</li> <li>Grass filter strip</li> <li>Grass channel</li> <li>Other:</li> </ul>	

#### I. SUPPORTING INFORMATION

Provide a concise narrative describing the stormwater management strategy, describing how
this practice fits into the overall plan, and stating all assumptions made in the design.
Observations of the DMD on the site many including the following

Show the location of this BMP on the site map, including the following:

- Facility area
  - \_\_\_\_\_ Contributing drainage area (CDA) boundaries and acreage.
  - Embankment area
  - Delineation of FEMA 100-year floodplain (bioretention should be constructed *outside* the limits of the floodplain).
    - Areas of site compensated for in water quality calculations
- If the Bioretention facility will receive runoff from a hotspot land use, then an underdrain must be used.
- Bioretention facilities must not be located where they will receive regular dry weather flows or flow from sources such as sump pumps, irrigation water, chlorinated wash-water or swimming pool discharge, or other flows that are not stormwater runoff.
- Provide topography for the site area, showing that the slope of the CDA is between 1% and 5%. Provide a soil map for site and area of facility, showing CDA and facility boundaries
  - Show the soil boring locations and provide the soil boring logs with Unified Soils Classifications and descriptions (at least one boring must be taken to confirm the underlying soil properties *at the depth where biofiltration or bioinfiltration is designed to occur,* to ensure that depth to the groundwater table/bedrock or karst is identified). HSG-B, C or D soils typically require an underdrain, whereas HSG-A soils generally do not.

Provide the results of soil infiltration rate testing to confirm a minimum subsoil infiltration rate of > 0.5 inch/hour (> 1 inch/hour in order to avoid the use of an underdrain). The number of infiltration tests is based on the scale of the planned infiltration facility area – see Tables 9.2 and 9.3 in Stormwater Design Specification No. 9 and Appendix 8-A in Stormwater Design Specification No. 8).

- Confirm the depth to seasonal high groundwater table (minimum 2 ft. below the design bottom of the facility, or 1 ft. if in a coastal area and a large-diameter underdrain is used that only partially dewaters the bed)
  - Confirm the depth to bedrock (minimum 2 ft. below the design bottom of the facility)
  - If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (recommend a min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) must be place beneath the bioretention facility. Where karst is present, there must be at least 3 feet of vertical separation between the bottom of the bioretention facility and the karst layer. Furthermore, only micro-scale or small-scale bioretention facilities not exceeding 20,000 sq. ft. may be used, and they must be designed *ONLY* to meet the Level 1 design criteria (incorporating an underdrain).
- \_\_\_\_\_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.)
- \_\_\_\_\_ Avoid installing geotextile filter fabric along the *bottom* of bioretention facilities (causes clogging).

# **II. COMPUTATIONS**

# A. Hydrology

\_\_\_\_\_ Determine the runoff curve numbers (pre- and post-developed conditions), providing the worksheets.

\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.

\_\_\_\_\_ Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

Urban Bioretention facilities, in particular, should be designed to fully drain within 24 hours following each storm.

# **B.** Hydraulics

- Ensure that 4 to 5 feet of hydraulic head (3 to 5 feet for Urban Bioretention) are available above the bottom elevation needed to tie the underdrain into the storm drain system, in order to drive runoff through the filter bed. Less head is necessary for HSG-A soils.
- \_\_\_\_\_ Specify assumptions and coefficients used.
- Provide a stage-storage table and curve
- Provide for large storm overflow or bypass
- Provide storm drainage and hydraulic grade line calculations.

# C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - Provide specific sizing/dimensions determined from criteria in Stormwater Design Specification No. 9.

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information

- Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of the bioretention facilities / planters. NOTE: The maximum contributing drainage area for a micro-bioretention facility (e.g., rain garden) is 0.5 acre (3% of the CDA or 5% of the roof area for Level 1 or 4% of the CDA or 6% of the roof area for Level 2); for an urban bioretention facility is 2,500 sq. ft., and for a conventional bioretention facility is 2.5 acres. Observe proper setbacks from building foundations, down-gradient slopes, etc.: 5 feet down-gradient from wet utility lines. NOTE: Dry utility lines (e.g., gas, electric, cable and telephone, etc.) may cross under bioretention areas if they are double-cased. \_\_\_\_\_10 feet down-gradient from building foundations for urban bioretention. NOTE: If the facility is lined and an underdrain is used, there is no minimum setback requirement. 5 feet down-gradient and 25 feet up-gradient from building foundations for micro-scale (rain garden) facilities \_\_\_\_\_10 feet down-gradient and 50 feet up-gradient from building foundations for standard bioretention facilities with a 0.5 acre or smaller CDA \_\_\_\_\_ 25 feet down-gradient and 100 feet up-gradient from building foundations for standard bioretention facilities with a CDA of between 0.5 to 2.5 acres. If an in-ground basement or other special conditions exist, the design should be reviewed by a licensed engineer. NOTE: A special footing or drainage design may be used to justify a reduction of the setbacks noted above. In cold climate areas, 25 feet from roadways to prevent potential frost heaving of the pavement 100 feet from any water supply well (50 feet if the biofilter is lined) Design Urban Bioretention, in particular, to minimize interference with pedestrian traffic and allow for frequent landscape and facility maintenance Geometry: \_\_\_\_\_ Level 1: Length of the shortest flow path/overall length = 0.3 OR other design methods are used to prevent short-circuiting; a one-cell design (not including the pre-treatment cell. Level 2: Length of the shortest flow path/overall length = 0.8 OR other design methods are used to prevent short-circuiting; a two-cell design (not including the pre-treatment cell. Show the location of all conveyance system outfalls (inlets) into the facility with pre-treatment and outlet protection designed in accordance with the VE&SCH \_\_\_\_ Ensure the proper geometry and orientation of the facility and inlets to the facility to avoid shortcircuiting Show the top-of-bank and basin bottom elevations \_\_\_\_ Show the treatment volume and maximum water surface elevations for all appropriate design storms and safety storms Show the location of the underdrain, if applicable Ensure and show adequate maintenance access to the facility
- Show the location of the observation well

# B. BMP Section Views & Related Details

#### 1. Micro-Bioretention Facility (Rain Garden)

- Pre-treatment:
  - Level 1: External (leaf screens, grass filter strip, energy dissipators, etc.)
    - Level 2: External plus a grass filter strip
- Inflow: From sheet flow or a roof leader

Facility may be a single-cell design (can be divided into smaller cells at downspout locations) Maximum ponding depth: 6 inches.

# Virginia Stormwater Management Handbook, Chapter 8

Show the elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms \_ Show the facility rim elevations: constructed height and settled height (allowing for 10% settlement). \_\_\_ Ensure adequate freeboard Provide a typical grading section through the facility Filter media: Depth: minimum 18 inches for Level 1; minimum 24 inches for Level 2; recommended maximum depth is 36 inches for both. Media mixed on site or supplied by vendor for Level 1, but *must* be supplied by vendor for Level 2 P-index: Between 20 and 30 for a media mix, OR between 7 and 21 mg/kg of P in the soil media (see Section 6.6 of Stormwater Design Specification No. 9) \_\_\_\_ Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for pollutant removal. Infiltration Rate: Between 1 to 2 inches per hour Media mix: Equivalent to loamy sand, with the following composition: \_\_\_\_\_ 85% to 88% sand \_\_\_\_\_ 8% to 12% soil fines 3% to 5% organic matter Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch Underdrain: Level 1: Corrugated HDPE or equivalent Level 2: Corrugated HDPE or equivalent, with a minimum 6-inch stone sump below the invert: OR none. if soil infiltration requirements are met A minimum of 3 inches of VDOT #57 clean washed stone (less than 1% passing a #200 sieve) must be laid and packed above and below the pipe. Cleanouts are *not* needed In cold climates (winter or otherwise) it is advisable to extend the filter bed and underdrain pipe below the frost line and/or oversize the underdrain by on pipe size to reduce the potential for freezing. Vegetation: Level 1: Turf or herbaceous cover (alternative to mulch), or shrubs (minimum 1 of these 3 choices) Level 2: Turf or herbaceous cover (alternative to mulch), shrubs, or trees (minimum 2 of these 4 choices) 2. Standard Bioretention Filter or Bioretention Basin Pre-treatment: Level 1: A pre-treatment cell, grass filter strip, gravel diaphragm, gravel flow spreader, or another approved (manufactured) pre-treatment device. Level 2: A pre-treatment cell plus one of the following: a grass filter strip, gravel diaphragm, gravel flow spreader, or another approved (manufactured) pre-treatment device. Inflow: From sheet flow, curb cuts, trench drains, concentrated flow, or the equivalent Maximum ponding depth: 6 inches (preferred) to 12 inches. NOTE: Ponding depths greater than 6 inches will require a specific planting plan to ensure appropriate plant selection. \_ Show the elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms \_\_\_\_ Show the facility rim elevations: constructed height and settled height (allowing for 10% settlement). Ensure adequate freeboard Provide a typical grading section through the facility Filter media: \_\_\_\_\_ Depth: minimum 24 inches for Level 1; minimum 36 inches for Level 2; recommended maximum depth is 6 feet for both.

- \_\_\_\_\_ Media mixed on site or supplied by vendor for Level 1, but *must* be supplied by vendor for Level 2
- P-index: Between 20 and 30 for a media mix, *OR* between 7 and 21 mg/kg of P in the soil media (see Section 6.6 of Stormwater Design Specification No. 9)
- \_\_\_\_\_ Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for pollutant removal.
- Infiltration Rate: Between 1 to 2 inches per hour
- Media mix: Equivalent to loamy sand, with the following composition:
  - \_\_\_\_\_ 85% to 88% sand
    - \_\_\_\_\_ 8% to 12% soil fines
      - \_\_\_\_\_ 3% to 5% organic matter

\_\_\_\_\_ Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch Underdrain:

- Level 1: Schedule 40 PVC with clean-outs
- Level 2: Schedule 40 PVC with clean-outs *and* with a minimum 12-inch stone sump below the invert; *OR* none, if soil infiltration requirements are met
- A minimum of 3 inches of VDOT #57 clean washed stone (less than 1% passing a #200 sieve) must be laid and packed above and below the pipe.
- In cold climates (winter or otherwise) it is advisable to extend the filter bed and underdrain pipe below the frost line and/or oversize the underdrain by on pipe size to reduce the potential for freezing.
  - Conveyance and Overflow:
    - For on-line bioretention: Incorporate an overflow structure to safely convey larger storms through the bioretention area. The following criteria apply to overflow structures:
      - The overflow associated with the 2-year and 10-year design storms should be controlled so that velocities are non-erosive at the outlet point (to prevent downstream erosion)
      - Common overflow systems within bioretention practices consist of an inlet structure, where the top of the structure is placed at the maximum water surface elevation of the bioretention area, which is typically 6 to 12 inches above the surface of the filter bed (6 inches is preferred).
      - The overflow capture device (typically a yard inlet) should be scaled to the application; this may be a landscape grate inlet or a commercial-type structure.
      - \_\_\_\_\_ The filter bed surface should generally be flat so the bioretention area fills up like a bathtub.
    - For off-line bioretention (preferred): Create an alternate flow path at the inflow point into the structure so that when the maximum ponding depth is reached, the incoming flow is diverted past the facility (so that the excess flows do not pass over the filter bed and through the facility, but additional flow is able to enter as the ponding water filters through the soil media).

Vegetation:

- Level 1: A planting template to include turf or herbaceous cover (alternative to mulch), shrubs, and/or trees to achieve surface area coverage of at least 75% within 2 years.
- Level 2: A planting template to include turf or herbaceous cover (alternative to mulch), shrubs, and/or trees to achieve surface area coverage of at least 90% within 2 years. If using turf, it must be combined with other vegetation.

#### 3. Urban Bioretention (planters, etc.)

Pre-treatment (keep in mind the aesthetic qualities of the visible materials):

- A pre-treatment cell, grass filter strip, gravel diaphragm, gravel flow spreader, or another approved (manufactured) pre-treatment device.
- \_\_\_\_\_ A trash rack between the pre-treatment cell and the main filter bed, allowing trash to be collected from a single location.
- \_\_\_\_\_ Trash racks across curb cuts, keeping trash in the gutter, accessible to street-sweeping equipment.

# Virginia Stormwater Management Handbook, Chapter 8

A pre-treatment area above the ground or a manhole or removable grate directly over
the pre-treatment area.
 Inflow: From sheet flow, curb cuts, trench drains, roof drains, concentrated flow, or the
equivalent
 Inlets should be stabilized with VDOT #3 stone, a splash block, river stone, or another
acceptable energy dissipation measure.
 Surface slope: 1% toward the outlet, unless a stormwater planter is used.
 Maximum ponding depth: 6 inches (preferred) to 12 inches. NOTE: Ponding depths greater than
6 inches will require a specific planting plan to ensure appropriate plant selection.
 Filter media:
Depth: minimum 30 inches; recommended maximum depth is 4 feet. NOTE: If large
trees and shrubs are planted, the <i>minimum</i> depth should be 4 feet.
Media mixed on site or supplied by vendor for Level 1, but <i>must</i> be supplied by vendor
for Level 2
P-index: Between 20 and 30 for a media mix, OR between 7 and 21 mg/kg of P in the
soil media (see Section 6.6 of Stormwater Design Specification No. 9)
Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for
pollutant removal.
Infiltration Rate: Between 1 to 2 inches per hour
Media mix: Equivalent to loamy sand, with the following composition:
85% to 88% sand
8% to 12% soil fines
3% to 5% organic matter
Filter media in a box should be extended from one wall to within 6 inches of the opposite
wall, and it may be centered in the box or offset to one side.
Filter media must be separated from the soil by non-woven geotextile fabric or a 2 to 3
inch layer of either washed VDOT #8 stone or 1/8 to 3/8-inch pea gravel.
Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch.
 Waterproof stormwater planters near building foundations by using a watertight concrete shell or
an impermeable liner, to prevent seepage.
 Expanded tree pits:
The bottom of the soil/media layer must be a minimum of 4 inches below the root ball of
trees and shrubs being planted.
Where portions of extended tree pits are covered with permeable pavers or cantilevered
sidewalks, ensure the filter media is connected beneath these surfaces so roots can
share the space.
Installing a removable tree pit grate (capable of supporting H-20 axel loads) over the
filter bed media can prevent pedestrian traffic and trash accumulation.
Low, wrought iron fences can help restrict pedestrian traffic across the tree pit bed and
protect pedestrians where there is a drop-off from the sidewalk to the bioretention cell.
Each tree needs a minimum of 400 cubic feet of shared root space. Stormwater Curb Extensions: It may be necessary to provide a barrier to keep water from
 saturating the adjacent road or street's sub-base and ensure it continues to be capable of
supporting H-20 axel loads.
Underdrain:
 Slotted Schedule 40 PVC pipe greater than 4 inches in diameter, with clean-outs.
A minimum of 2 inches of VDOT #57 clean washed stone (less than 1% passing a #200
sieve) must be laid and packed above and below the pipe.
Minimum underdrain pipe slope is 0.5%.
Overflows can either be diverted from entering the bioretention cell or dealt with via an overflow
 inlet. Optional methods include:
Curb openings sized to capture only the treatment volume and bypass higher flows
through the existing gutter.
Landscaping-type inlets or standpipes with trash guards.
A pre-treatment chamber with a weir design that limits flow to the filter bed area.

Any grates used above Urban Bioretention areas must be removable to allow maintenance access.

- Stencil or otherwise permanently mark each Urban Bioretention unit as a "stormwater management facility," indicating that (1) it has a water quality protection purpose, (2) it may pond briefly after a storm, and (3) it is not to be disturbed except for required maintenance. Vegetation:
  - Urban Bioretention cells can vary from formal gardens or naturalized landscapes, depending on the degree of landscape maintenance that can be provided
  - Where less frequent maintenance may be available and trash accumulation is a concern, use a "turf and trees" landscape model, perhaps including some herbaceous flowering plants.
  - Choose native trees and shrubs known to be hearty in the polluted air and compacted soils of urban settings, although some ornamental species can be used.
    - Selected vegetation must be tolerant of road salts, drought, and inundation.

# C. Landscape Plan

- Consider the importance of aesthetics and visual characteristics (foliage form, texture, color, etc.)
- Consider visibility, traffic considerations and other safety issues
- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Plant selection should be appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
- \_\_\_\_\_ Check whether future tree canopy heights associated with Urban Bioretention practices will interfere with existing overhead utility lines.
- \_\_\_\_\_ Specify preservation measures for existing vegetation
- The construction contract should include a *Care and Replacement Warranty* that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.

# D. Ecological Considerations

- Consider sun and wind exposure
- Consider the effects upon bioretention area from adjacent plant communities
  - \_\_\_\_\_ Wildlife benefits appropriate for the location may be included in plant material layout
- Consider any insect and disease infestation at or near the facility site

# E. Construction Notes

- Planned bioretention areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment.
  - Bioretention areas *may* be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the following:
    - The maximum excavation depth at the construction stage must be at least 1 foot above the post-construction installation.
    - \_\_\_\_\_ The facility must contain an underdrain.
    - Showing the proper procedures for converting the temporary sediment controls to a permanent bioretention facility, including dewatering, cleanout and stabilization.
    - Provide traffic control to avoid tracking mud and fine sediment into the facility and compacting the soil.

\_\_\_\_ Store materials in a protected area to keep them free from mud, dirt and other foreign materials.

- Obtain filter media from an approved vendor and store it on an adjacent impervious area or on plastic sheeting.
- Where any Urban Bioretention facilities are constructed in the road or right-of-way, the construction sequence may need to be adjusted to account for traffic control, pedestrian access and utility notification.

Construction sequence:

- Construction inspections should occur before, during and after installation to ensure the bioretention facility is constructed according to specifications.
  - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
- \_\_\_\_\_ Check the proposed site for existing utilities prior to any excavation.
- The designer and the installer/contractor should have a pre-construction meeting, checking the boundaries of the CDA and the actual inlet elevations to ensure they conform to the original design.
  - The designer should clearly communicate, in writing, any project changes determined during the pre-construction meeting to the installer and the plan review/inspection authority.
- Construction of the bioretention facility should begin only *after* site work is completed and the entire contributing drainage area has been stabilized with dense and healthy vegetation.
- \_\_\_\_\_ It may be necessary to block certain curb or other inlets while the bioretention area is being constructed.
- Temporary E&S control measures (typically silt fence, diversion berms, EC fabric, etc.) to prevent sediment from moving into the filter media or stone base material during construction), to avoid clogging (particularly if the practice relies on infiltration), and to protect the facility's vulnerable side slopes from erosion during construction.
- Ensure that pre-treatment structures are properly installed and working effectively.
- Excavators or backhoes (with arms with adequate extension) should work from the sides to excavate the reservoir layer to its appropriate design depth and dimensions.
  - Contractors should use a cell construction approach in larger bioretention basins, with the basin split into 500 to 1,000 sq. ft. temporary cells with a 10 to 15 foot earth bridge in between each cell, so that cells can be excavated from the side.
  - \_\_\_\_\_ The floor of the facility should be completely level, but equipment should be kept off the floor to prevent soil compaction.
  - \_\_\_\_\_ It may be necessary to rip the bottom soils to a depth of 6 to 12 inches to promote greater infiltration.
  - Correctly install geotextile fabric on the excavation sides.
    - Trim large tree roots flush with the sides of the excavation to prevent puncturing or tearing of the filter fabric.
    - When laying out the geotextile, the width should include sufficient material to compensate for perimeter irregularities in the trench and for a 6-inch minimum overlap at the top of the excavation.
  - \_\_\_\_\_ Place stones or other anchoring objects on the fabric at the trench sides to keep the trench open during windy periods.
  - Place natural soils in any voids that occur between the fabric and the excavated sides of the trench, to ensure the fabric conforms smoothly to the sides of the excavation.
  - \_\_\_\_ Install and anchor the observation well(s) and, if used, install the underdrains.
    - \_\_\_\_\_ Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth
    - \_\_\_\_\_ Check elevations (underdrain inverts, inflow and outflow point inverts, depth of aggregate installations, etc.) and the surface slope.
    - Provide the correct depth and type of aggregate above and below the underdrains.
    - \_\_\_\_\_ Underdrains should slope down towards the outlet at a grade of 0.5% or steeper.
    - \_\_\_\_\_ Up-gradient ends of underdrains in the reservoir layer should be capped, but *not* the downstream ends.

- Where an underdrain pipe is connected to a structure, there must be *no* perforations within 1 foot of the structure.
- Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.
- Place approximately 3 inches of choker stone/pea gravel on the stone above the underdrain(s) as a filter between the underdrain stone layer and the soil filter media.
- Place the filter media by hand (to avoid compaction and maintain porosity) in 12-inch lifts, with no machinery allowed directly on the media surface during or after construction, until the design top elevation is achieved.
  - \_\_\_\_\_ Overfill the media above the proposed finished surface elevation to allow for natural settling. Lifts may be lightly watered to encourage settling.
  - After the final lift is placed, rake the media to level it, saturate it, and allow it to settle for at least one week prior to installing plant materials. Check for settlement and add additional media, if needed, to achieve the design elevation.
- Prepare planting holes for any trees and shrubs, install the vegetation, and water accordingly.
- Install any temporary irrigation equipment.
- Place the surface cover in the bioretention cells (mulch, river stone or turf), depending on the design.
  - \_\_\_\_\_ If coir or jute matting will be used instead of mulch, the matting will need to be installed prior to planting, and holes or slits will have to be cut in the matting to install the plants.
- \_\_\_\_\_ Install the plant materials as shown in the landscaping plan, and water them during weeks of no rain for the first two months following installation.
  - The construction contract should include a *Care and Replacement Warranty* to ensure that vegetation is properly established and survives during the first growing season following construction.
  - Implement any remaining permanent stabilization measures.
- Log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.
- E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
    - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, periodic replacement of soil media, care of the vegetation, and mowing.
- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the bioretention areas are not disturbed or converted to other uses.
  - Provide sufficient facility access from the public ROW or roadway to both the bioretention facility and any pre-treatment practices.

#### IV. COMMENTS

-		
-		
-		
	-	5.4
	Ву:	Date:

# 8-A.11.0. DRY SWALES: DESIGN CHECKLIST

(NOTE: Think of this practice as linear bioretention)

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

Plan Status Approved Not Approved	Legend:       Image: Complete         Inc.       - Incomplete/Incorrect         N/A       - Not Applicable		
Facility Type: Level 1	Level 2		
Type of Dry Swale:	Type of Pre-Treatment Facility:		
Dry Conveyance Swale	□ Sediment Forebay		
Dry Treatment Swale	Check Dam		
	Tree Check Dam		
Hydraulic Configuration:	Grass Filter Strip		
<ul> <li>On-line (typical)</li> </ul>	Gravel Diaphragm		
Off-line (more rare, for Level 2	Pea Gravel Flow Spreader		
designs only)	□ Other:		

# I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design. Show the location of the BMP on the site map, including:

  - \_\_\_\_\_ Swale area
  - \_\_\_\_\_ Contributing drainage area (CDA) boundaries and acreage
  - \_\_\_\_\_ Delineation of FEMA 100-year floodplain
    - Areas of site compensated for in water quality calculations
  - Provide topography for the site area, showing that the slope of the CDA is between 1% and 4%, but preferably not exceeding 2%.
    - Check dams can be used to reduce the effective slopes of the swale and lengthen the contact time to enhance filtering and/or infiltration.
    - In areas of steep terrain, Dry Swales can be implemented on slopes of up to 20% gradient, as long as a terraced multiple-cell design is used to dissipate energy prior to filterina.
      - \_\_\_\_\_ Limit the drop in elevation between cells to 1 foot.
      - \_\_\_\_\_ Armor the swale with river stone or a suitable equivalent.
      - Drop structures and energy dissipators must be carefully designed and constructed.
- Provide a soil map for the site and area of the Dry Swale(s), including the CDA
  - Provide soil boring locations and soil boring logs with Unified Soils Classifications and descriptions (at least one boring must be taken to confirm the underlying soil properties at the depth where biofiltration or bioinfiltration is designed to occur, to ensure that depth to the

groundwater table/bedrock or karst is identified). HSG-C or D soils typically require an underdrain, whereas HSG-A and B soils generally do not.

- Provide the results of soil infiltration rate testing to confirm a minimum subsoil infiltration rate of > 0.5 inch/hour to avoid the use of an underdrain. Use the infiltration test procedures provided in Appendix 8-A in Stormwater Design Specification No. 8 (Infiltration).
- Confirm the depth to the seasonal high groundwater table (minimum 2 ft. below the design bottom of the facility, or 1 ft. if in a coastal area and an underdrain is used that has a minimum slope of 0.5% and is connected to the drainage system). NOTE: Wet Swales are preferred in coastal plain settings.
  - Confirm the depth to bedrock (minimum 2 ft. below the design bottom of the facility)
- If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (recommend a min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) and underdrain must be place beneath the Dry Swale (Level 1 design only).
- Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).
  - Consult local utility design criteria for the horizontal and vertical clearance between utilities and swales.
  - \_\_\_\_\_ Utilities can cross linear swales if they are specially protected (e.g., double casing).
  - \_\_\_\_\_ Water and sewer lines generally need to be placed under road pavements to enable the use of adjacent Dry Swales.
    - The bottom elevation of a swale should be a minimum 1 foot below the invert elevation of any adjacent road bed.

\_ Dry Swales should be located so as to avoid inputs of springs, irrigation water, chlorinated wash water, or other dry weather flows.

#### **II. COMPUTATIONS**

#### A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrograph (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
- Confirm that there is adequate drainage area and/or base flow

#### **B. Hydraulics**

- \_\_\_\_\_ The treatment volume must be completely filtered within a maximum of 6 hours following a storm.
- \_\_\_\_\_ Typically require 3 to 5 feet of hydraulic head (between the inflow point and the downstream storm drain invert).
  - \_\_\_\_ The swale must be designed with enough capacity to:
    - Convey runoff from the 2-year and 10-year design storms at non-erosive velocities with at least 3 inches of freeboard.
      - \_\_\_\_\_ Contain the 10-year flow within the banks of the swale (tends to drive the surface dimensions).
- The bottom width and slope must be designed so that the velocity from a 1-inch rainfall will not exceed 3 ft./sec. (check dams can be incorporated to reduce flow volume and velocity)
- \_\_\_\_\_ Specify assumptions and coefficients used.
- \_\_\_\_\_ Provide a stage-storage table and curve
- Provide storm drainage and hydraulic grade line calculations (evaluate the flow profile through the channel at normal depth, as well as flow depth over the top of check dams).
- \_\_\_\_\_ Account for any check dams placed within the swale

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - \_ Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 10.

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information

- \_\_\_\_\_ Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
  - Show the locations and dimensions of pre-treatment practices:
    - \_\_\_\_\_ A grass filter strip for a Dry Conveyance Swale
    - For a Dry *Treatment* Swale, may use a variety of pre-treatment practices, depending on they type of flow entering the swale, with one at each inflow point to the swale (to trap coarse sediment to prevent clogging of the filter media).
  - Layout and dimensions of Dry Swale. NOTE: The maximum contributing drainage area for a Dry Swale is 5 acres (preferably less); a Dry Swale should be approximately 3% to 10% of the size of the CDA, depending on the amount of impervious cover..
  - \_\_\_\_ Dry Swales are not subject to normal building setbacks, given their position in the landscape.
  - \_\_\_\_\_ Runoff originating from hotspot sources should *not* be treated by Level 2 (infiltrating) Dry Swales; an impermeable liner should be used.
    - Proper geometry and orientation to avoid short-circuiting:
      - A parabolic cross-sectional shape is preferred for hydraulic, maintenance and aesthetic purposes; a trapezoidal shape may be used as long as the soil filter bed boundaries lay in the flat bottom of the swale
      - Side slopes should be no steeper than 3H:1V to facilitate ease of mowing; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale.
      - Dry Swales should have a bottom width of from 4 to 8 feet to provide adequate filtering area; if the swale will be wider than 8 feet, the designer should incorporate berms, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion of the swale bottom.
      - The longitudinal slope should be relatively flat (2% or less for a Level 1 design, and 1% or less for a Level 2 design), to allow for temporary ponding of the treatment volume within the channel. The minimum recommended slope is 0.5% (unless the swale is off-line, similar to a bioretention facility), but slopes up to 4% are acceptable if check dams are used.
- Location of all conveyance system outfalls into the swale with pre-treatment and outlet protection designed in accordance with the VE&SCH
- \_\_\_\_\_ Top of bank and basin bottom elevations
- Elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
  - Location of underdrain, if applicable
- Location of observation well(s)
  - Location of check dams, if applicable:
    - \_\_\_\_\_ Stone energy dissipators are required at the downstream toe of check dams to prevent erosion.
    - The check dam must be designed to spread runoff evenly over the Dry Swale's filter bed surface, through a depressed weir (in the center of the check dam) with a length equal to the filter bed width (sized to convey the depth of flow for the appropriate design storm).
    - \_\_\_\_\_ Check dams must be spaced correctly, consistent with criteria in Stormwater Design Specification No. 10.
    - Adequate maintenance access to the facility

#### B. BMP Section Views & Related Details

- Sections through pre-treatment practices. Elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms; the maximum ponding depth is a Dry Swale should not exceed 12 inches at the most downstream point. Adequate freeboard Swale bank elevations: constructed height and settled height (allowing for 10% settlement). \_\_\_\_\_ Typical grading section through the facility, showing basin bottom slope Underdrain, if applicable: \_\_\_\_\_ Underdrains are provided to ensure Dry Swales drain properly after storms. Underdrains must be 6-inch Schedule 40 PVC with 3/8-inch perforations and clean-outs; use non-perforated pipe to connect to the storm drain system. Install the underdrain with two layers of stone: A 12-inch deep underdrain stone layer must be composed of 1-inch clean, double-washed stone (VDOT #57 aggregate) free of all soil and fines, with the underdrain set 4 inches above the bottom of this laver of stone. NOTE: The depth of this storage layer (9 to 18 inches) will depend on the target treatment and storage volumes needed to meet water quality, channel protection, and/or flood protection criteria. In cold climates, extend the underdrain pipe below the frost line and oversize the pipe by one pipe size, to reduce the risk of freezing. Choker layer: A 2 to 4-inch layer of sand laid over a 2 inch layer of VDOT #8 or #89 choker stone (washed gravel) laid above the underdrain encasement stone layer and immediately below the filter laver. Observation well(s): Installed along the length of the swale, if the contributing drainage area exceeds 1 acre. Wells should be tied into any T's or Y's in the underdrain system. Each well should be flush with the ground surface, with a vented cap. Filter media:
  - \_\_\_\_\_ Depth: minimum 18 inches above choker stone layer.
  - \_\_\_\_\_ Media mixed on-site (for smaller applications) or supplied by an approved vendor.
  - P-index: Between 20 and 30 for a media mix, *OR* between 7 and 21 mg/kg of P in the soil media (see Section 6.6 of Stormwater Design Specification No. 9)
  - \_\_\_\_\_ Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for pollutant removal.
    - Infiltration Rate: Between 1 to 2 inches per hour
  - \_\_\_\_\_ Media mix: Equivalent to loamy sand, with the following consistent, homogenous composition:
    - 85% to 88% sand
    - 8% to 12% soil fines
    - \_\_\_\_\_ 3% to 5% organic matter
    - \_\_\_\_\_ Alternative: Use 100% sand for the first 18 inches of the filter, and add a combination of topsoil and leaf compost for the top 4 inches, where turf cover will be maintained.
      - The volume of the media mix should be 110% of the product of the surface area and the media depth, to account for settling.
  - Filter fabric (side slopes):
    - \_\_\_\_ Non-woven polyprene geotextile with a flow rate of > 110 gal./min./sq. ft. (e.g., Geotex 351 or equivalent).
    - \_\_\_\_ Apply immediately above the underdrain only.
  - Topsoil should be a 4-inch layer of loamy sand or sandy loam texture, with less than 5% clay content, a corrected pH of 6 to 7, and at least 2% organic content.
  - \_\_\_\_\_ Surface cover should be turf (as specified in the landscaping plan) or river stone.

Check dam details:

- \_\_\_\_\_ Made of non-erosive material such as pressure-treated logs or timbers, wood from water-resistant tree species such as cedar, hemlock, swamp oak or locust, gabions, riprap, or concrete.
- \_\_\_\_\_ Check dams must be firmly anchored into the side slopes to prevent outflanking and be stable during the 10-year design storm.
- The height of the check dam relative to the normal channel elevation should not exceed 12 inches. For greater than 12-inch high check dams or swale slopes greater than 4%, special features such as drop structures are required to ensure non-erosive flows.
- Each check dam should have a minimum of one weep hole or a similar drainage feature so it can dewater after storms (for slopes less than 2%, at least 3 weep holes in each check dam).
- Soil plugs, appropriate for Dry Swales of 4% or steeper slopes or with 12-inch high check dams, help minimize the potential for blow-out of the soil filter media beneath check dams, due to hydrostatic pressure from the upstream ponding.
- Erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric or mats (EC2) that are durable enough to last at least two growing seasons.

# C. Landscape Plan

- Provide a planting schedule and specifications (transport / storage / installation / maintenance) Plant selection must be appropriate for the site's vegetation climatic zone (4-8 in Virginia)
- Where Dry Swales receive runoff from road surfaces in areas of cold climate, they should be planted with salt-tolerant grass species.
  - \_\_\_\_\_ The construction contract should include a *Care and Replacement Warranty* that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.
    - \_\_\_\_ Specify preservation measures for existing vegetation

# E. Construction Notes

- Ideally, planned Dry Swale areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment. However, this is seldom practical, since swales are a key part of the natural drainage system at most sites. Therefore, temporary E&S controls such as dikes, silt fences, etc. should be integrated into the swale design throughout the construction sequence.
- Dry Swale areas *may* be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the following:
  - The maximum excavation depth at the construction stage must be at least 1 foot above the post-construction installation.
  - \_\_\_\_\_ The facility must contain an underdrain.
  - Showing the proper procedures for converting the temporary sediment controls to a permanent Dry Swale, including dewatering, cleanout and stabilization.
  - Provide traffic control to avoid tracking mud and fine sediment and compacting the soil.
  - Store materials in a protected area to keep them free from mud, dirt and other foreign materials.
    - Obtain filter media from an approved vendor and store it on an adjacent impervious area or on plastic sheeting.
  - Where Dry Swales are constructed in the road or right-of-way, the construction sequence may need to be adjusted to account for traffic control, pedestrian access and utility notification. Construction sequence:
    - Construction inspections should occur before, during and after installation to ensure the bioretention facility is constructed according to specifications.
      - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
      - Check the proposed site for existing utilities prior to any excavation.

- After the first big storm, verify whether the sheet flow, shallow concentrated flow or fully concentrated flow assumed in the plan actually occurred in the field and verify that the swale drains completely within 6 hours. Adjust the plan as necessary.
- \_\_\_\_\_ The designer and the installer/contractor should have a pre-construction meeting, checking the boundaries of the CDA and the actual inlet elevations to ensure they conform to the original design.
  - The designer should clearly communicate, in writing, any project changes determined during the pre-construction meeting to the installer and the plan review/inspection authority.
- \_\_\_\_\_ Construction of the bioretention facility should begin only *after* site work is completed and the entire contributing drainage area has been stabilized with dense and healthy vegetation.
- It will be necessary to divert flow while the Dry Swale is being constructed, until the filter bed and side slopes are fully stabilized.
- Temporary E&S control measures (typically silt fence, diversion berms, EC fabric, etc.) to prevent sediment from moving into the filter media or stone base material during construction), to avoid clogging (particularly if the practice relies on infiltration), and to protect the facility's vulnerable side slopes from erosion during construction.
- Ensure that pre-treatment structures are properly installed and working effectively.
- Excavators or backhoes (with arms with adequate extension) should work from the sides to excavate the reservoir layer to its appropriate design depth and dimensions.
  - Rip, roto-till or otherwise scarify the swale's bottom soils to promote greater infiltration.
  - Correctly install geotextile fabric on the side slopes.
    - When laying out the geotextile, the width should include sufficient material to compensate for perimeter irregularities in the trench and for a 6-inch minimum overlap at the top of the excavation.
    - Place stones or other anchoring objects on the fabric at the trench sides to keep the trench open during windy periods.
  - Install and anchor the observation well(s) and, if used, install the underdrains.
    - \_\_\_\_\_ Check elevations (underdrain inverts, inflow and outflow point inverts, depth of aggregate installations, etc.) and the surface slope.
    - \_\_\_\_\_ Check aggregate material prior to installation to confim that it is clean and washed and meets specifications.
    - \_\_\_\_\_ Provide the correct depth and type of aggregate layers above and below the underdrains.
    - \_\_\_\_\_ Up-gradient ends of underdrains in the reservoir layer should be capped, but *not* the downstream ends.
    - Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.
  - Place the filter media by hand (to avoid compaction and maintain porosity) in 12-inch lifts, with no machinery allowed directly on the media surface during or after construction, until the design top elevation is achieved.
    - Overfill the media above the proposed finished surface elevation to allow for natural settling. Lifts may be lightly watered to encourage settling.
    - After the final lift is placed, rake the media to level it, saturate it, and allow it to settle for at least a few days prior to installing plant materials. Check for settlement and add additional media, if needed, to achieve the design elevation.
- Install check dams, driveway culverts and internal pre-treatment features, as specified in the plan.
- \_\_\_\_\_ Install erosion control fabric, prepare planting holes for any trees and shrubs, install the vegetation, and water accordingly.
- \_\_\_\_\_ Install any temporary irrigation equipment.
- Install the plant materials as shown in the landscaping plan, and water them during weeks of no rain for the first two months following installation.

- The construction contract should include a *Care and Replacement Warranty* to ensure that vegetation is properly established and survives during the first growing season following construction.
- Implement any remaining permanent stabilization measures.
- Log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.

Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, periodic replacement of soil media, care of the vegetation, and mowing.

- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the dry swale areas are not disturbed or converted to other uses.
- Provide sufficient facility access from the public ROW or roadway to both the bioretention facility and any pre-treatment practices.

#### **IV. COMMENTS**

By: \_\_\_\_\_ Date: \_\_\_\_\_

# 8-A.12.0. WET SWALES: DESIGN CHECKLIST

(NOTE: Think of this practice as a linear constructed wetland)

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number

Signature and stamp of licensed professional design consultant and owner certification

Plan Status Approved Not Approved	Legend:       Image: Complete         Inc.       -       Incomplete/Incorrect         N/A       -       Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration:	Type of pretreatment facility:Check Dams (channel flow)Tree Check Dams (channel flow)Grass Filter Strip (sheet flow)Gravel or Stone Diaphragm (sheet flow)Gravel or Stone Flow Spreaders (concentrated flow)Other:None

#### I. SUPPORTING INFORMATION

- Provide a concise narrative describing the stormwater management strategy, describing how this practice fits into the overall plan, and stating all assumptions made in the design.
   Show the location of this BMP on the site map, including the following:
   Swale area
  - Contributing drainage area (CDA) boundaries and acreage (should not exceed 5 acres). Delineation of FEMA 100-year floodplain
    - Areas of site compensated for in water quality calculations
    - Provide topography for the site area, showing that the slope of the CDA is between 1% and 2%.
    - Check dams can be used to reduce the effective slopes of the swale and lengthen the contact time to enhance treatment.
  - An alternative for steep slopes is the *Regenerative Conveyance System (RCS)*, which conveys water down the slopes through a series of step pools that provide treatment (see Stormwater Design Specification No. 11).

Provide a soil map for site and area of facility, including the CDA.

Provide soil boring locations and soil boring logs with Unified Soils Classifications and descriptions (at least one boring must be taken to confirm the underlying soil properties). Wet Swales work best when constructed over the more impermeable HSG-C or D soils.

- Confirm the depth to the seasonal high groundwater table.
  - NOTE: It is permissible for wet swales to intersect the water table; this may reduce pollutant removal and increase excavation costs.

\_\_\_\_\_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).

\_\_\_\_\_ Wet Swales are not recommended for the following situations:

To treat runoff from stormwater hotspots, due to the potential interaction with the water table and the risk that hydrocarbons, trace metals and other pollutants could migrate into the groundwater.

Karst areas.

Residential areas, due to the risk of mosquito breeding.

# **II. COMPUTATIONS**

# A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
  - \_\_\_\_\_ Confirm that there is adequate drainage area and/or base flow.

# **B. Hydraulics**

- If designed as an on-line practice (Level 1 design), the swale must be designed with enough capacity to:
  - Convey runoff from the 2-year and 10-year design storms at non-erosive velocities with adequate freeboard.
  - Contain the 10-year flow within the banks of the swale with adequate freeboard. (tends to drive the surface dimensions).
- \_\_\_\_\_ If designed as an off-line practice (Level 2 design), a bypass or diversion structure must be designed to divert the large storm (e.g., when the flow rate and/or volume exceeds the treatment volume) to an adequate channel or conveyance system.
  - \_ The Wet Swale is then designed to meet the volume, velocity and residence time criteria for
- Wet Swales are designed based on peak flow rate the maximum flow velocity of the channel must be less than 1 foot per second during a 1-inch water quality storm event
  - The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity requirements)
  - Verify hydraulic capacity using Manning's Equation or an accepted equivalent method, such as erodibility factors and vegetal retardance
    - \_\_\_\_\_ The flow depth for the peak treatment volume (1-inch rainfall) should be maintained at 3 inches or less
    - Manning's "n" value for grass channels should be 0.2 for flow depths up to 4 inches, decreasing to 0.03 at a depth of 12 inches (which applies to the 2-year and 10-year storms if an on-line application
    - Peak flow rates for the 2-year and 10-year frequency storms must be non-erosive or subject to site-specific analysis of the channel lining material and vegetation
      - \_\_\_\_\_ The 10-year peak flow rate must be contained within the channel banks, with a minimum of 6 inches of freeboard
- \_\_\_\_\_ Specify assumptions and coefficients used.
- Provide a stage-discharge table and curve (provide equations).
- Route post-development hydrographs for appropriate design storms (2-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required)
- Provide storm drainage and hydraulic grade line calculations.
- Calculations for peak flow depth and velocity should reflect any increase in flow along the length of the channel, as appropriate. If a single flow is used, the flow at the outlet should be used.

The hydraulic residence time should be minimum of 9 minutes for the treatment volume (1-inch rainfall) design storm. If flow enters the channel at multiple locations, a 9-minute minimum hydraulic residence time should be demonstrated for each entry point, using equations in Stormwater Design Specification No. 3 (Grass Channels).

#### C. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
- Indicate the treatment volume for extended detention (if added) with draw-down calculation
- \_\_\_\_\_ Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 11.

#### III. PLAN REQUIREMENTS

#### A. BMP Plan View Information

- \_\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- \_\_\_\_\_ Show the locations and dimensions of pre-treatment practices and all conveyance system outfalls into the swale
- \_\_\_\_\_ Wet Swales are not subject to normal building setbacks, given their position in the landscape.
  - Show the layout and dimensions of the Wet Swale.
    - A Wet Swale should be approximately 5% to 15% of the size of the CDA, depending on the amount of impervious cover (NOTE: The maximum contributing drainage area for a Wet Swale is 5 acres).
    - \_\_\_\_\_ Surface dimensions are largely determined by the need to pass the 10-year design storm.
    - \_\_\_\_\_ The minimum length may be achieved with multiple swale cells connected by culverts with energy dissipators.
  - \_\_\_ Ensure the proper geometry and orientation, to avoid short-circuiting:
    - A parabolic cross-sectional shape is preferred for hydraulic, maintenance and aesthetic purposes; a trapezoidal shape may be used as long as the soil filter bed boundaries lay in the flat bottom of the swale
    - Side slopes should be no steeper than 4H:1V to enable wetland plant growth; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale. Under no circumstances are the side slopes to be steeper than 3H:1V.
    - Wet Swales should have a bottom width of from 4 to 8 feet to provide adequate filtering area; if the swale will be wider than 8 feet, the designer should incorporate berms, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion of the swale bottom.
  - \_\_\_\_\_ Indicate the top-of-bank and swale bottom elevations
  - Indicate the elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms.
    - The average normal pool depth (dry weather) throughout the swale should be 6 inches or less.
    - \_\_\_\_\_ The maximum temporary ponding depth in any single wet Swale cell should not exceed
    - 18 inches at the most downstream point (e.g., at a check dam or driveway culvert).
    - \_\_\_\_ Show the location of check dams, if applicable:
      - \_\_\_\_\_ Stone energy dissipators are required at the downstream toe of check dams to prevent erosion.
      - The check dam must be designed to spread runoff evenly over the Wet Swale's surface, through a depressed weir (in the center of the check dam) with a length equal to the bed width (sized to convey the depth of flow for the appropriate design storm).
    - Check dams must be spaced correctly:
      - \_\_\_\_\_ Cells formed by check dams or driveways should be at least 25 to 40 feet in length.

Check dams should also be spaced as needed to maintain the effective longitudinal slope of 2% for Level 1 Wet Swales or 1% for Level 2 Wet Swales. Show adequate maintenance access to the facility

## B. BMP Section Views & Related Details

- \_\_\_\_\_ Show cross-sections through the swale, showing:
  - Various water surface elevations (treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms) and adequate freeboard. Side slopes, top width, swale bank elevations: constructed height and settled height
  - (allowing for 10% settlement).
- Wetland planting areas.
- Ensure the proper geometry:
  - \_\_\_\_\_ Wet Swales should be designed with a trapezoidal or parabolic cross-section. A parabolic shape is preferred for aesthetic, maintenance and hydraulic reasons.
  - Side slopes should be no steeper than 4H:1V to enable wetland plant growth; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale. Under no circumstances are the side slopes to be steeper than 3H:1V.
  - The longitudinal slope should be relatively flat (2% or less for a Level 1 design, and 1% or less for a Level 2 design), to allow for temporary ponding of the treatment volume within the channel. The minimum recommended slope is 0.5% (unless the swale is off-line), but slopes up to 4% are acceptable if check dams are used.

#### C. Check Dams

- \_\_\_\_\_ Check dams should be composed of wood, concrete, stone, or other non-erodible material, or should be configured with elevated driveway culverts.
  - \_\_\_\_ Check dams should be underlain with filter fabric conforming to the following standards:
    - \_\_\_\_\_ Needled, non-woven, polypropylene geotextile.
      - Grab Tensile Strength (ASTM D4632): ∃ 120 lbs.
      - \_\_\_\_\_ Mullen Burst Strength (ASTM D3786): ∃ 225 lbs./sq. in.
      - \_\_\_\_\_ Flow Rate (ASTM D4491): ∃ 125 gpm/sq. ft.
        - Apparent Opening Size (ASTM D4751): ∃ US #70 or #80 sieve
  - \_\_\_\_ Wood used for check dams should consist of pressure-treated logs or timbers, or water-resistant tree species such as cedar, hemlock, swamp oak or locust.
- It is necessary to compute check dam materials, based on the surface area and depth used in the design computations.
- Check dams should be spaced based on the channel slope, as needed to increase residence time and provide adequate storage for the treatment volume (1-inch rainfall) or any additional volume attenuation requirements. The ponded water at a downhill check dam should not touch the toe of the upstream check dam.
- The maximum desired check dam height is 12 inches (for maintenance purposes). However, for challenging sites, a maximum of 18 inches can be allowed, with additional design elements to ensure the stability of the check dam and the adjacent and underlying soils. The average ponding depth throughout the channel should be 12 inches.
- Armoring may be needed at the downstream toe of the check dam to prevent erosion.
- Check dams must be firmly anchored into the side-slopes to prevent outflanking; check dams must also be anchored into the channel bottom so as to prevent hydrostatic head from pushing out the underlying soils.
- \_\_\_\_\_ Check dams must be designed with a center weir sized to pass the channel design storm peak flow (10-year storm event for man-made channels).
- Each check dam should have a weep hole or similar drainage feature so it can dewater after storms.

Individual channel segments formed by check dams or driveways should generally be at least 25 to 40 feet in length.

#### D. Diaphragms

Pea gravel used to construct pre-treatment diaphragms should consist of washed, open-graded, course aggregate between 3 and 10 mm in diameter and must conform to local design standards.

#### E. Landscape Plan

- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
  - Select plant materials appropriate for the site's vegetation climatic zone (6-8 in Virginia), emphasizing native plant materials.
    - Plant materials must be able to withstand both wet and dry periods as well as relatively high velocity flows within the swale.
      - Wet Swales should be planted with wet-footed species, such as sedges or wet meadow vegetation.
      - If the swale is adjacent to a roadway where winter conditions will require the use of road salts in the CDA, then salt-tolerant non-woody plant species should be specified.
  - \_\_\_\_ It may be advisable to incorporate sand or compost into the surface soils to promote a better growing environment.
  - Specify preservation measures for existing vegetation
- The construction contract should include a *Care and Replacement Warranty* that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.

#### **D.** Construction Notes

- Ideally, planned Wet Swale areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment. However, this is seldom practical, since swales are a key part of the natural drainage system at most sites. Therefore, temporary E&S controls such as dikes, silt fences, etc. should be integrated into the swale design throughout the construction sequence. Specifically, barriers should be installed at key check dam locations, and E&S control fabric should be used to protect the channel bottom.
- Wet Swale areas *may* be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the following:
  - The maximum excavation depth at the construction stage must be at least 1 foot above the post-construction installation.
    - \_\_\_\_\_ Show the proper procedures for converting the temporary sediment controls to a permanent Wet Swale, including dewatering, cleanout and stabilization.
- Wet Swale construction should begin only after the entire contributing drainage area has been stabilized with vegetation. Sediment accumulation must be removed during final grading to achieve the design cross-section.
- Ideally, Wet Swales should be constructed during months that are best for establishing vegetative cover without irrigation (February 15 April 15; September 15 November 15).
  - It will be necessary to divert flow while the Wet Swale is being constructed, until the bed and side slopes are fully vegetated.
    - Show applicable temporary E&S control measures.

\_\_\_ Construction sequence for BMP(s) and E&S controls:

- Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications.
  - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.

- \_\_\_\_ Check the proposed site for existing utilities prior to any excavation.
- Install applicable temporary E&S Controls prior to construction.
- Grade the channel to the final dimensions shown on the plan.
- Install check dams, driveway culverts and internal pre-treatment features as shown on the plan
- Fill material used to construct the check dams should be placed in 8- to 12-inch lifts and compacted to prevent settlement. The top of each check dam should be constructed level at the design elevation.
- (Optional) Till the bottom of the channel to a depth of 1 foot and incorporate compost amendments according to Stormwater Design Specification No. 4.
- Planting soil should be loam or sandy loam with a high organic content, placed by mechanical methods, and spread by hand to a depth of at least 4 inches for shallow wetlands.
  - Planting soil should be tamped as directed in the design specifications, but it should not be overly compacted.
  - \_\_\_\_\_ After the planting soil is placed, it should be saturated and allowed to settle for at least one week prior to installation of plant materials.
  - \_\_\_\_\_ No machinery should be allowed to traverse over the planting soil during or after construction.
- \_\_\_\_\_ Redirect previously diverted flows into the Wet Swale to allow it to fill up to normal pool elevation.
  - \_\_\_\_\_ Wetland planting areas should be at least partially inundated during planting to promote plant survivability.
    - Surveyed planting zones should be marked on the as-built or design plan, and the locations should be identified in the field, using stakes or flags.

Propagate the stormwater wetland between mid-April and mid-June, using three simultaneous techniques to propagate the emergent community over the wetland bed:

- Initial planting of container-grown wetland plant stock.
- Broadcast wetland seed mixes over the higher wetland elevations, to establish diverse emergent wetlands.
  - Seeding of Switchgrass or wetland seed mixes as a ground cover is recommended for all zones above 3 inches below the normal pool elevation.
    - Hand broadcasting or hydroseeding can be used to spread seed, depending on the size of the wetland cell.
- \_\_\_\_\_ After initial planting, a biodegradable E&S control fabric may be used, conforming to Standard and Specification 3.36 of the VESCH.
- Prepare planting holes for any trees and shrubs, then plant materials as shown in the landscaping plan and water them weekly in the first two months.
- \_\_\_\_\_ Install goose protection for newly planted or newly growing vegetation, especially emergents and herbacious plants.
  - \_\_\_\_\_ Place netting, webbing, or string installed in a criss-cross pattern over the surface area of the wetland above the level of the emergent plants.
  - Implement any remaining permanent stabilization measures.
- \_\_\_\_\_ Conduct a final inspection, log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, and care of the vegetation.

Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the wet swale area is converted to other uses.

Provide sufficient facility access from the public ROW or roadway to both the wet pond and any pre-treatment practices.

## **IV. COMMENTS**

	·

By: \_\_\_\_\_ Date: \_\_\_\_\_

# 8-A.13.0. FILTERING PRACTICES: DESIGN CHECKLIST

-		
Plan Submission Date	_	
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
BMP Designer		Phone Number
General Contractor		Phone Number
Signature and stamp of licens certification	ed professio	nal design consultant and owner
Plan Status		
Approved	Legend:	📃 - Complete
Not Approved		Inc Incomplete/Incorrect
		N/A - Not Applicable
Facility Type: Level 1	Lev	vel 2
Eacility Type:		
Facility Type: G Non-Structural Sand Filter	Pro-Tr	eatment:
G Surface Sand Filter		Wet or Dry Sedimentation
	G	Chamber designed as level
<ul> <li>Organic Media Filter</li> <li>Underground Sand Filter</li> </ul>		spreaders and sized to
<ul> <li>Proprietary Filter</li> </ul>		accommodate 25% of the
□ Other:		treatment volume
	G	Forebay
Hydraulic Configuration:		Compost-amended grass filter
□ On-line facility		path
□ Off-line facility		Gravel Diaphragm
		Check Dam
□ FILTER TREATS HOSPOT RUNOFF		Engineered Level Spreader
		Proprietary device
		Other:
I. SUPPORTING INFORMATION		
		er management strategy, describing how
this practice fits into the overall plan, a		
Show the location of this BMP on the s	site map, includir	ng the following:
Filter facility area		
Contributing drainage area (Cl		acreage and land cover
Delineation of FEMA 100-year		
Areas of site compensated for	in water quality	calculations
Provide topography of the site area.	fo allity in algorithm.	
Provide a soil map for site and area of		ogs with Unified Soils Classifications and
soil descriptions (at least one boring m		
		<i>i</i> point within the footprint of the proposed
		indwater/bedrock and to evaluate the soil
suitability		in uwaler/bedrock and to evaluate the SOII
•	um of 2 feet co	paration distance between the seasonally
		bottom invert of the filtering practice.
		estigation is recommended to ensure the
installation does not aggravate		

- \_\_\_\_\_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).
- \_\_\_\_\_ Special conditions:
  - Filters work well in karst areas, assuming that they are water tight and that excavation does not extend into a karst layer.
  - In coastal plain settings, the Perimeter Sand Filter and the Non-Structural Sand Filter work best, subject to the following criteria:
    - The combined depth of the underdrain and sand filter bed can be reduced to from 24 to 30 inches
    - \_\_\_\_\_ Consider maximizing the length of the filter or provide treatment in multiple connected cells.
    - The minimum depth to seasonally high groundwater may be relaxed to 1 foot, as long as the filter is equipped with a large diameter underdrain (e.g., 6 inches) that is only partially efficient at dewatering the filter bed.
      - Maintain an underdrain slope of at least 0.5% to ensure positive drainage and to tie it into the receiving ditch or conveyance system.
    - In steep terrain:
      - Slope gradient contributing runoff to sand filters can be increased to 15%, as long as a two-cell, terraced design is used to dissipate erosive energy prior to the filter.
        - The drop in elevation between cells should be limited to 1 foot and the slope should be armored with river stone or a suitable equivalent.

In cold climate of for winter performance (problem is ice forming over the filter bed):

- \_\_\_\_\_ Place a weir between the pre-treatment chamber and filter bed to reduce ice formation.
- \_\_\_\_\_ Extend the filter bed below the frost line to prevent freezing within the filter bed.
  - Oversize the underdrain to encourage more rapid drainage and to minimize freezing of the filter bed.
- Expand the sediment chamber to account for road sand. Pre-treatment chambers should be sized to accommodate up ot 40% of the treatment volume.

# **II. COMPUTATIONS**

# A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)

# **B. Hydraulics**

- \_\_\_\_\_ The hydraulic head required for filters varies from 2 to 10 feet, depending on the design variant; sufficient hydraulic head is critical to the proper function of filtering systems.
- Confirm that the design will result in the facility dewatering within 40 hours after a storm event.
- \_\_\_\_\_ Specify the assumptions and coefficients used.
- Provide a stage-storage table and curve
- \_\_\_\_\_ Provide for large storm overflow or bypass
- Provide storm drainage and hydraulic grade line calculations.

#### C. Water Quality

A maximum contributing drainage area (CDA) of 5 acres is recommended for surface sand filters, and a maximum CDA of 2 acres is recommended for perimeter or underground filters, to minimize clogging.

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA. For Level 1 designs, the contributing drainage area may contain some pervious area; for Level 2 designs, the CDA must be nearly 100% impervious (preferred condition).
- \_\_\_\_\_ Determine the pollutant load, pollutant load removal, and treatment volume requirements, generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet).
- Keep in mind that Level 2 designs are sized for a treatment volume that is 25% greater than for Level 1 practices.
- Also, keep in mind that for Level 2 designs, the runoff reduction value (normally 0) may be increased if a second cell is used for infiltration or bioinfiltration (Bioretention Level 2). The RR credit should be proportional to the fraction of the treatment volume designed to be infiltrated. Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 12.

# III. PLAN REQUIREMENTS

# A. BMP Plan View Information

- \_\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- \_\_\_\_\_ Show the layout and dimensions of the filtering facilities (one cell for Level 1 design; two cells for Level 2)
- Sand and organic surface filters typically consume approximately 2% to 3% of the CDA, while perimeter sand filters typically consume less than 1% of the CDA. Underground filters generally consume no surface area except for their manholes.
- NOTE: Surface area and storage volume of the filter media relates to the treatment volume (Equations 12.1 and 12.2 in Stormwater Design Specification No. 12)
- Ensure proper orientation to avoid short-circuiting
- Ensure adequate maintenance access to the facility
- \_\_\_\_\_ Show the observation well location

# B. BMP Section Views & Related Details

\_\_\_\_\_ Details will vary depending upon the type of filter employed:

**1.** Non-Structural Sand Filter – applied to sites less than 2 acres in size and essentially the same as a Bioretention Basin (Stormwater Design Specification No. 9), with the following exceptions:

- \_\_\_\_\_ The bottom is lined with an impermeable filter fabric and *always* has an underdrain.
- \_\_\_\_\_ The surface cover is sand, turf or pea gravel (*not* trees, shrubs, or herbaceous material).
- \_\_\_\_\_ The filter media is 100% sand.
  - The filter has two cells, with a dry or wet sedimentation chamber preceding the sand filter bed.

# 2. Surface Sand Filter (more economical)

- \_\_\_\_\_ Designed with both the filter bed and sediment chamber located at ground level
- Normally constructed of pre-cast or cast-in-place concrete
- Usually designed to be off-line facilities, so that only the treatment volume is directed to the filter.
- Can be installed in the bottom of a dry Extended Detention Basin (see Stormwater Design Specification No. 15).

# 3. Organic Media Filter

- Essentially the same as surface sand filters, except the sand is replaced with an organic filtering medium (e.g., peat/sand filter, leaf compost filter, etc.) that is better at removing metals and hydrocarbons. However, organic media can actually leach soluble nitrate and phosphorus back into the discharge water.
- 4. Underground Sand Filter (more expensive, but they consume very little surface area)
- \_\_\_\_\_ Filtering components are installed underground

## 5. Perimeter Sand Filter (more economical)

- \_\_\_\_\_ Incorporates a sediment chamber and filter bed, but flow enters through grates, usually at the edge of a parking lot.
- \_\_\_\_\_ Usually designed as an on-line practice (i.e., all flows enter the system), where larger flows bypass by entering an overflow chamber
- \_\_\_\_\_ Requires only about 2 feet of hydraulic head, so can be used on sites with little topographic relief

#### 6. Proprietary Filters

- Follow the design criteria provided by the manufacturer
- \_\_\_\_\_ Conveyance and Overflow:
  - For off-line filter systems, show the internal flow splitter or overflow device that bypasses runoff from larger storm events around the filter.
  - For on-line filter systems, show how the device will safely pass the local design storm(s) (1-year and/or 10-year storms) without re-suspending or flushing previously trapped material.
  - \_\_\_\_\_ Ensure that the facility will dewater within 40 hours after a storm event.
  - Filtering practices typically have an impermeable liner meeting the following criteria:
    - \_\_\_\_\_ Needled, non-woven polypropylene geotextile (do *not* use heat-set or heatcalendared fabrics)
      - Grab Tensile Strength (ASTM D4632) =  $\exists$  120 lbs.
      - Mullen Burst Strength (ASTM D3786) =  $\exists$  225 lbs./sq. in.
      - Flow Rate (ASTM D4491) =  $\exists$  125 gpm/sq. ft.
      - Apparent Opening Size (ASTM D4751) = US #70 or #80 sieve.

#### Underdrain:

- Pipes comply with AASHTO M252 and ASTM F405
- If the underdrain must meet ASTM F758, it must be perforated with slots that have a maximum width of 3/8-inch and provide a minimum inlet area of 1.76 sq. in. per linear foot of pipe.
- If underdrain meets ASTM F949, it must be perforated with slots that have a maximum width of 3/8-inch and provide a minimum inlet area of 1.5 sq. in. per linear foot of pipe.
- \_\_\_\_\_ Underdrain pipe with precision-machined slots is preferred to pipe with standard roundhole perforations.
  - \_\_\_\_\_ The stone jacket for the underdrain must meet VDOT #57 stone specifications or the ASTM equivalent (1-inch maximum diameter).
- Filter Media:
  - Normal filter media consists of clean, washed medium aggregate concrete sand with individual grains between 0.2 and 0.04 inches in diameter (AASHTO M-6/ASTM C-33)
- Organic media can be used, such as a peat/sand mixture or a leaf compost mixture, but this is not recommended unless metals and hydrocarbons are a particular issue in site runoff
- Surface Cover:
  - For surface sand filters, surface cover should consist of a 3-inch layer of topsoil on top of a non-woven filter fabric laid above the sand layer (pea gravel inlets in the topsoil layer where sheet flow enters, at margins around the filter bed, or at locations in the middle of the bed, to promote infiltration).
  - For underground sand filters, surface cover should have a pea gravel layer on top of a coarse non-woven filter fabric laid over the sand layer.
  - \_\_\_\_ Media depth can range from 12 to 18 inches.

Maintenance Reduction Design Features:

- Observation wells and cleanouts (facilitates inspection and maintenance)
  - \_\_\_\_\_ Surface sand filters should include an observation well, consisting of a 6-inch diameter non-perforated PVC pipe fitted with a lockable cap.
  - \_\_\_\_\_ Install the observation well flush with the ground surface.
  - Typically, a cleanout pipe will be tied into the end of each underdrain pipe run.
  - The portion of the cleanout pipe/observation well in the underdrain layer should be perforated.
    - Provide at least one cleanout pipe for every 2,000 sq. ft. of filter surface area.
- Good maintenance access must be provided, such that a vacuum truck or similar equipment can get close enough to the sedimentation chamber and filter to perform cleanouts.
- Installing media depths deeper than 18 inches can facilitate the removal of 1 to 3 inches of sand during maintenance without have to necessarily replace it.
- Access to the headbox and clearwell of *underground* sand filters must be provided by manholes at least 30 inches in diameter, along with steps to the areas where maintenance will occur.
- Install stormwater filters at the site so that inspection and maintenance personnel can easily see them. Provide adequate signs or markings at manhole access points for underground filters.
- For underground filters, note that special OSHA rules and training apply to protect workers that must access them.

# C. Landscape Plan

Consider the importance of aesthetics and visual characteristics (foliage form, texture, color, etc.)

- Consider visibility, traffic considerations and other safety issues
- Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Plant selection appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species.
- \_\_\_\_\_ Specify preservation measures for existing vegetation
- Where applicable, ensure that topsoil / planting soil is included in final grading

#### D. Construction Notes

- The future location of filtering practices may be used as the site of a temporary sediment trap or basin during site construction, as long as the design elevations are set with final cleanout and conversion in mind.
  - \_\_\_\_\_ The bottom elevation of the filtering practice should be lower than the bottom elevation of the temporary sediment basin.
  - \_\_\_\_\_ Appropriate procedures must be implemented to prevent discharge of turbid waters when the temporary basin is converted to the filtering practice.
    - \_\_\_\_\_ Then the sediment basin must be dewatered, dredged and regraded to the design dimensions for the post-construction stormwater filter.
  - Construction sequence for filtering practices and E&S controls

Stabilize the drainage area.

\_\_\_\_\_ Construct filtering practices only *after* the CDA to the facility is completely stabilized.

- \_\_\_ Install E&S controls for the filtering practice.
  - It is extremely important that stormwater is diverted around the filtering practice as it is being constructed, in order to prevent sediment from clogging the filter bed during construction.
  - \_\_\_\_\_ Install silt fence around the perimeter of the sand filter.
  - Install erosion control fabric on exposed side-slopes with gradients exceeding 4H:1V.
  - Rapidly stabilize exposed soils around the filter by hydro-seed, sod, mulch or other locally-approved method of soil stabilization.
- \_\_\_\_ Assemble construction materials, make sure they meet design specifications, and prepare staging areas

# Virginia Stormwater Management Handbook, Chapter 8

\_\_\_\_\_ Clear and strip the project area to the desired subgrade.

- Excavate/grade until the appropriate elevation and desired contours are achieved for the bottom and side slopes of the filtering practice.
- Install the filter structure
  - Check all design elevations (concrete vaults for surface, underground and perimeter sand filters).
  - Upon completion of the filter structure shell, plug inlets and outlets temporarily and fill the structure with water to the brim to check for water-tightness (maximum allowable leakage is 5% of the water volume in a 24-hour period).
  - \_\_\_\_\_ If the structure fails the test, perform repairs to make the structure watertight before any sand is place into it.
  - Install the gravel, underdrains, and choker layer of the filter.
- \_\_\_\_\_ Place the filter media:
  - \_\_\_\_\_ Spread sand across the filter bed in 1 foot lifts up to the design elevation.
  - Manually rake the sand.
    - Add clean water until the sedimentation chamber and filter bed are completely full.
  - \_\_\_\_\_ Allow the facility to drain, hydraulically compacting the sand layers.
  - After 48 hours of draining and drying, refill the structure to the final top elevation of the sand filter bed.
  - \_\_\_\_\_ Filter fabric installation:
    - \_\_\_\_\_ Install the permeable filter fabric over the sand.
      - \_\_\_\_ Add a 3-inch topsoil layer and pea gravel inlets.
    - \_\_\_\_ Immediately stabilize with permanent grass species.
      - \_\_\_\_\_ Water the grass as needed to develop a vigorous grass cover (do not activate the filter system until vigorous cover is present)
- E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)
  - Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
    - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, periodic replacement of soil media, care of the vegetation, and mowing.
- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the bioretention areas are not disturbed or converted to other uses.
- Provide sufficient facility access from the public ROW or roadway to both the filtration facility and any pre-treatment practices.
  - To prevent freezing in cold climates and winter weather, require or clearly recommend that filters be inspected before the onset of winter (prior to the first freeze) to dewater wet chambers and scarify the filter surface.

# IV. COMMENTS

Ву:	Date:
	200

# 8-A.14.0. CONSTRUCTED WETLANDS: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	
General Contractor	
Signature and stamp of licensed profest certification	ssional design consultant and owner
Plan Status	
Approved Legend:	Complete
Not Approved	Inc Incomplete/Incorrect N/A - Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration:	Type of Pre-Treatment Facility:
□ On-line facility	□ Sediment forebay (above ground)
$\Box$ Off-line facility	<ul> <li>Vegetated buffer area</li> </ul>
	Grass filter strip
Type of wetland:	□ Grass channel
Constructed Wetland Basin (Level 1 –	□ Other:
emergent))	
Constructed multi-cell wetland (Level 2	
– emergent and forest)	
Constructed multi-cell pond/emergent	
wetland combination (Level 2)	
I. SUPPORTING INFORMATION	
Provide a concise narrative describing the stormwater management strategy, describing how	
this practice fits into the overall plan, and stating all assumptions made in the design.	
Show the location of this BMP on the site map, including the following:	
The basin pool area The contributing drainage area (CDA) boundaries, acreage and land cover, sufficient to	
sustain a permanent water level within the constructed wetland.	
Delineation of FEMA 100-year floodplain	
Areas of the site compensated for in water quality calculations	
Provide topography of the site area, including the constructed wetland area.	
Provide a geotechnical report with recommendations and earthwork specifications and a	
description of any borrow area involved	
Provide a soil map for site and area of facility, showing CDA and facility boundaries	
Provide soil boring locations and soil boring logs with Unified Soils Classifications and soil	
descriptions.	
Borings should be taken below the proposed embankment, in the vicinity of the	
proposed outlet area, and in at least two locations within the planned wetland treatment	
area.	
Determine the physical characteristics of the soils regarding:	
Suitability for use as structural fill or spoil.	
Bearing capacity, buoyancy, etc. pertaining to outlet structure design.	
Compaction/composition needs for the embankment.	
Evaluation of potential infiltration losses (and the consequent need for a liner).	

Depth to bedrock.

Depth to seasonal high groundwater table (NOTE: It is permissible for wet swales to intersect the water table; this may reduce pollutant removal and increase excavation costs).

If karst is present, a detailed geotechnical investigation is recommended to ensure the constructed wetland does not aggravate potential karst impacts (e.g., sinkholes, etc.):

- Must maintain at least 3 feet of vertical separation from the underlying karst layer.
- Must employ an impermeable liner that meets the requirements of Stormwater Design Specification No. 13.
- Must use shallow, linear and multiple-cell wetland configurations rather than deep basin configurations (e.g., a pond/wetland or ED wetland).
- Constructed wetlands are ideal for coastal settings with flat terrain, low hydraulic head and high water table conditions:
  - \_\_\_\_\_ Choose shallow, linear and multiple-cell configurations
    - \_\_\_\_\_ Acceptable to excavate below the water table, as follows:
      - 6 inches below to provide the requisite hydrology for wetland planting zones.
      - Up to 3 feet below for micro-pools, forebays and other deep pool features.
  - The volume below the seasonably high groundwater table may count toward the Treatment Volume, as long as the other primary geometric and design requirements for the wetland are met (e.g., flow path, microtopography, etc.)
  - Plant selection should focus on species that are wet-footed and can tolerate some salinity.
  - Consider creating forested wetlands, since a greater range of coastal plain tree species (Atlantic White Cedar, Bald Cypress, Swamp Tupelo, etc.) can tolerate periodic inundation.
  - Consider using the Regenerative Conveyance System (RCS) where there is considerable drop in elevation from the channel to the outfall location (see Stormwater Design Specification No. 13).
- \_\_\_\_ Constructed wetlands are not effective at sites with steep terrain.
  - \_\_\_\_\_ May be able to terrace wetland cells in a linear configuration, as with the Regenerative Conveyance System.
- Where cold winter climates are typical, make the following adjustments:
  - \_\_\_\_\_ Treat larger runoff volumes in the spring by adopting seasonal operation of the permanent pool.
  - \_\_\_\_\_ Plant salt-tolerant vegetation (to deal with higher chloride content of road salts).
  - \_\_\_\_\_ Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage ice formation.
  - Locate low-flow orifices so they withdraw at least 6 inches below the typical ice layer.
  - \_\_\_\_\_ Angle trash racks to prevent ice formation.
  - Over-size the riser and weir structures to avoid ice formation and freezing pipes.
  - \_\_\_\_\_ If road sanding is prevalent in the CDA, increase the forebay size to accommodate additional sediment loading.
- \_\_\_\_\_ Constructed wetlands are generally *not* recommended in watersheds containing trout streams, due to the potential for stream warming, unless:
  - All other upland runoff reduction opportunities have been exhausted.
  - The Channel Protection Volume has not been provided through other means.
  - \_\_\_\_\_ A linear/mixed wetland design is applied to minimize stream warming.
  - A constructed wetland should *not* be built within an existing perennial stream or natural wetland nor should a constructed wetland discharge to jurisdictional waters without local/state/federal approvals and the necessary permit(s).
    - Constructed wetlands built for stormwater management purposes are typically *not* considered jurisdictional wetlands, but the designer should confirm this with applicable wetland regulatory authorities.
  - \_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).

\_ The designer should check to see whether sediments removed from the forebay can be spoiled (deposited) on-site or must be hauled away.

# **II. COMPUTATIONS**

# A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number determinations (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
- Ensure that there is adequate drainage area and/or water balance from groundwater, runoff or baseflow so the wetland will not go completely dry after a 30-day summer drought.

# **B. Hydraulics**

- \_\_\_\_\_ Specify assumptions and coefficients used.
- Typically, 2 to 4 feet of hydraulic head are need to drive flow through the wetland.
- Provide a stage-storage table and curve
- Weir/orifice control analysis for riser structure discharge openings and riser crest.
  - Carefully design the low-flow orifice to minimize clogging, as follows:
    - Recommend a minimum 3-inch diameter orifice to minimize clogging of an outlet or extended detention pipe when it is surface-fed (still susceptible to clogging from floating vegetation and debris).
    - \_\_\_\_\_ Smaller openings (down to 1-inch in diameter) are permissible, using internal orifice plates within the pipe.
      - All outlet pipes should be adequately protected by trash racks, half-round CMP, or reverse-sloped pipes extending to mid-depth of the micropool.
- \_\_\_\_\_ Barrel: conduct an inlet/outlet control analysis
- Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
- Provisions for use as a temporary sediment basin riser with clean out schedule & instructions for conversion to a permanent facility.
- Conduct an emergency spillway adequacy/capacity analysis (100-year design storm) with required embankment freeboard.
- Provide for large storm overflow or bypass
- Provide a stage-discharge table and curve (provide equations).
- Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required)
- Provide storm drainage and hydraulic grade line calculations.

# C. Downstream impacts

- Conduct a danger reach study.
- \_\_\_\_\_ Evaluate 100-year floodplain impacts.
- Provide downstream hydrographs at critical study points.
- Demonstrate safe conveyance to an "adequate" receiving channel.
  - If the receiving channel is natural and (1) has never been enhanced or "restored, OR (2) if stream channel erosion or localized flooding is an existing predevelopment condition, then conduct appropriate "energy balance" calculations to demonstrate safe conveyance from the facility to the receiving channel" (provide computations).

#### D. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
- \_\_\_\_ Calculate the treatment volume for extended detention (if added) with draw-down calculation
- Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 13.

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information

- Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- Setbacks (Note: local codes rule):
  - \_\_\_\_\_ Minimum 10 feet from property lines.
  - Minimum 25 feet from building foundations.
  - \_\_\_\_\_ Minimum 50 feet from septic system drainfields.
    - \_\_\_\_\_ Minimum 100 feet from private wells.
  - Pre-Treatment:
    - \_\_\_\_ Show all pre-treatment practices.
    - A sediment forebay should be considered an integral pre-treatment practice for all constructed wetlands.
      - \_\_\_\_\_ A forebay should be located at every major inlet to trap sediment and preserve the capacity of the main wetland treatment cell.
      - \_\_\_\_\_ A major inlet is any individual storm drain inlet pipe or open channel conveying runoff from at least 10% of the wetland's CDA.
      - The forebay is considered a separate cell in both Level 1 and Level 2 designs, formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabion baskets, etc.)
      - The forebay should be at least 4 feet deep and equipped with a variable width aquatic bench around the perimeter, for safety purposes. The aquatic bench should be 4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.
      - Show the location of the metered rod that monitors long-term sediment accumulation (in the center of the pool, as measured lengthwise along the low flow water travel path).
      - \_\_\_\_\_ The bottom of the forebay may be hardened (e.g., with concrete, asphalt, or grouted riprap) to make sediment removal easier.
  - \_\_\_\_ Show the locations of all conveyance system outfalls into basin
  - \_\_\_\_ Show the layout and dimensions of basin features: permanent pool, sediment forebay, embankment, emergency spillway. basin side slopes, basin bottom, etc.
    - \_\_\_\_ The footprint is typically *less* than 3% of the CDA for Level 1 designs and *more* than 3% of the CDA for Level 2 designs.
- Pool geometry
  - \_\_\_\_\_ Show the wet/dry weather flow paths
  - \_\_\_\_\_ Reflect the proper length-to-width ratio as specified in the BMP design specifications
  - Reflect the proper orientation to avoid short-circuiting
  - \_\_\_\_\_ Reflect the side slopes (H:V) of basin storage area and embankment (upstream and downstream slopes)
    - Provide an aquatic bench for safety
  - Indicate the location of outlet protection per VE&SCH Std. & Spec. 3.18
  - Indicate the top-of-bank and basin bottom elevations
- \_\_\_\_\_ Indicate the elevations of the permanent pool, the treatment volume and the maximum design water surface elevations for all appropriate design storms and safety storms
- \_\_\_\_\_ Snow any shoreline protection measures
- Show the location and dimensions of the riser and barrel
- \_\_\_\_\_ Identify the pool depth zones on the plan

- \_\_\_\_ Identify the constructed wetland/shallow marsh areas on the plan
- Provide basin liner specifications
- Provide sufficient maintenance access to the forebay, safety benches, riser structure, embankment, emergency spillway, basin shoreline, extended drawdown device, principal spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. The access road must:
  - Be constructed of load bearing materials able to withstand the expected frequency of use.
  - Have a minimum width of 12 feet.
  - \_\_\_\_\_ Possess a maximum profile grade of 15%.
  - Have sufficient turn-around area.
  - A maintenance right-of-way or easement must extend to the stormwater pond from a public or private road.

### B. BMP Section Views & Related Details

### 1. Pre-Treatment

- The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no less than 0.1 inch per impervious acre.
  - For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total required pool or detention volume may be more practical.
  - This volume should be a maximum of 4 feet deep (or a depth determined by the summer drought water balance) near the inlet to adequately dissipate turbulent inflow without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wetland cell.
- The forebay should be equipped with a variable width aquatic bench around the perimeter of the 4-foot depth, for safety purposes. The aquatic bench should be4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.
- \_\_\_\_\_ The volume of the forebay is part of the treatment volume of the stormwater basin for which it provides pre-treatment.
  - However, for dry facilities, the forebay does *not* represent available storage volume if it remains full of water.
  - \_\_\_\_\_ A dry forebay must be carefully designed to avoid the resuspension of previously deposited sediments.
- The total volume of all forebays should be at least 15% of the total Treatment Volume. The relative size of individual forebays should be proportional to the percentage of their total inflow to the wetland.
- \_\_\_\_\_ Separation between the forebay and the main basin may be achieved through the use of an earthen berm, gabion baskets, concrete, or a riprap wall.
- A designed overflow section should be constructed on the top of the separation to allow flow to exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design storms.
  - \_\_\_\_ The overflow section may be set at the permanent pool elevation or the extended detention volume elevation.
- \_\_\_\_\_ The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap) to make sediment removal easier.
- Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay and basin from excessive erosion from heavy equipment operation used for maintenance.
- Provide a typical grading section through the forebay, including typical side slopes, aquatic bench, shoreline protection, etc.

#### 2. Wetland Cells

- Since most constructed wetlands are on-line facilities, they need to be designed to safely pass the maximum design storm (e.g., the 10-year and 100-year design storms).
  - Ponding depths for the more frequent Treatment Volume storm (1-inch rainfall) and Channel Protection storm (1-year event) are limited in order to avoid adverse impacts to plant materials.
  - \_\_\_\_\_ Overflow for the less frequent 10- and 100-year storms should likewise be carefully designed to minimize the depth of ponding (a maximum of 4 feet over the wetland pool is recommended).
  - \_\_\_\_\_ The use of flashboard risers is strongly recommended to control or adjust water elevations in wetlands constructed on relatively flat terrain.
  - \_\_\_\_\_ Alternatively, a weir can be designed to accommodate passage of larger storms flows at relatively low ponding depths.
  - Level 1 designs may incorporate extended detention that meets a maximum of 50% of the treatment volume or up to 12 inches of detention storage above the wetland pool (for channel protection); Level 2 designs may *not* incorporate extended detention.
- \_\_\_\_\_ Internal design geometry:
  - Internal design geometry and depth zones are critical in maintaining the pollutant removal capability and plant diversity of constructed wetlands.
  - When feasible, wetlands should be irregularly shaped with long, sinuous flow paths, multiple cells (Level 2), and a high ratio of surface area to volume (see Stormwater Design Specification No. 13).
  - Flow Path:
    - \_\_\_\_\_ Overall flow path through the wetland (length-to-width ratio):
      - Level 1 design: 2L:1W.
      - \_\_\_\_\_ Level 2 design: 3L:1W.
      - \_ Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
        - Level 1 design: 0.5.
          - Level 2 design: 0.8.
          - If unable to meet these targets, then the drainage area served by these "closer" inlets should constitute no more than 20% of the total CDA.
    - Side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth of wetland vegetation, provide for easier maintenance, and create a more natural appearance.
    - The slope profile within individual wetland cells should generally be flat from inlet to outlet (adjusting for microtopography). The recommended elevation drop between wetland cells should be no more than 1 foot.

Proper surface area/depth allocations for permanent pool/shallow marsh/constructed wetland.

- Indicate the elevations of permanent pool, treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
- Pool depths:
  - Level 1 wetlands have a uniform depth with the mean pool depth greater than 1 foot.
    - Level 2 wetlands have variable depths with the mean pool depth # 1 foot.
- At least 25% of the Treatment Volume must be provided in at least three (3) deeper pools of from 18 to 48 inches, located at the inlet (forebay), center, and outlet (micropool) of the wetland.
- High Marsh Zone: At least 70% of the wetland surface must exist in the high marsh zone (-6 inches to +6 inches, relative to normal pool elevation)
- Transition Zone: The Low Marsh Zone (-6 inches to -18 inches below the normal pool elevation) is *no longer an acceptable wetland zone*, and is only allowed as a short transition zone from the deeper pools to the high marsh zone.
  - \_\_\_\_\_ This transition zone should have a maximum slope of 5H:1V, or preferably flatter, from the deep pool to the high marsh zone.
  - It is advisable to install biodegradable erosion control fabrics or similar materials during construction to prevent erosion and slumping of this transition zone.

Micro-topographic features (mix of above-pool vegetation, shallow pools and deep pools) that promote dense and diverse vegetative cover (Level 2 designs require at least two of the following):

- Tree peninsulas, high marsh wedges or rock filter cells configured perpendicular to the flow path.
- \_\_\_\_\_ Tree islands above the normal pool elevation and maximum extended detention zone, formed by coir fiber logs.
- \_\_\_\_\_ Inverted root wads or large woody debris.
- \_\_\_\_\_ Gravel diaphragm layers within high marsh zones.
- \_\_\_\_\_ Cobble sand weirs.
- \_\_\_\_\_ Additional deeper pools.

#### 3. Embankment (or dam)

- \_\_\_\_\_ Type of embankment:
  - Homogenous embankment
    - Zoned embankment
  - The earthen embankment must be designed to be stable against any force condition or combination of force conditions that may develop during the life of the structure (including differential settlement within the embankment, seepage through the embankment and foundation, or sharing stresses within the embankment and foundation) and is dependent upon:
    - Construction materials
    - \_\_\_\_\_ Foundation conditions
    - \_\_\_\_\_ Embankment height and cross-section geometry
    - \_\_\_\_\_ Normal and maximum pool levels
    - Purpose of structure (i.e., retention, extended detention, etc.).
  - Embankment geometry:
    - \_\_\_\_\_ Top of dam elevations: constructed height and settled height (allowing for 10% settlement).
      - Height (based on the freeboard requirements): There must be at least 1 foot of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment (excluding the emergency spillway).
      - An embankment *without* an emergency spillway must provide at least 2 feet of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment.
      - NOTE: The spillway design storm WSE, if specified, may be substituted for the 100-year storm WSE in either of the above situations.
    - \_\_\_\_\_ Top width varies with embankment height and should be shaped to provide positive drainage.
    - \_\_\_\_\_ The top of the embankment must be level in order to avoid possible overtopping in one location in cases of extreme storms or spillway failure.
    - Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and 2H:1V upstream face).
    - For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than 3H:1V.
    - The embankment cross-section must be designed to provide an adequate factor of safety to protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability depends upon:
      - Physical characteristics of the fill materials
      - \_\_\_\_\_ Configuration of the site
      - \_\_\_\_\_ Foundation materials
        - \_\_\_\_\_ Shear strength
        - \_\_\_\_\_ Compressibility
        - Permeability

- Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be designed so that the collection conduits discharge downstream of the embankment at a location where access for observation is possible by maintenance personnel.
- \_\_\_\_\_ Adequate erosion protection is recommended along the contact point between the face of the embankment and the abutments, where runoff concentrates.

- Evaluate whether a gutter surface other than sod is necessary (riprap is generally preferred over a paved concrete gutter).
- Trees, shrubs or any other woody plants should not be planted or allowed on the embankment or adjacent areas extending at least 25 feet beyond the embankment toe and abutment contacts.
- Indicate the top of embankment elevations: constructed height and settled height (allowing for 10% settlement).
- Indicate the elevation of the crest of the emergency spillway.
- Indicate the emergency spillway, with side slopes.
- Indicate the emergency spillway inlet, level, and outlet sections.
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the embankment.
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the principal spillway
- Provide a typical grading section through the pond, including typical side slopes with the aquatic bench, shoreline protection, etc.
- Show the existing ground and proposed improvements along the center line of the emergency spillway
  - \_ Show the dimensions of zones for any zoned embankment

#### 4. Seepage Control

The contact point between the embankment soil, the foundation material, and the conduit is the most likely location for *piping* to occur, due to the discontinuity in materials and the difficulty in compacting the soil around the pipe.

All utility conduits (except the principal spillway) should be installed away from the embankment.

- When utility conduits through the embankment cannot be avoided, they should meet the requirements for spillways:
  - \_\_\_\_\_ Watertight joints
    - No gravel bedding
      - Restrained to prevent joint separation due to settlement
- Phreatic line (4:1 slope measured from the principal spillway design high water elevation) is the upper limit of the saturation zone..
  - At a minimum, this should be the 10-year design storm water surface elevation.
  - If the phreatic line intersects the downstream slope of the embankment, a qualified soil scientist should be consulted to decide if additional controls, such as an internal drain, are needed.
  - \_ Seepage control should be included in the design if the following conditions exist:
    - Pervious layers in the foundation are not intercepted by the cutoff.
    - Possible seepage from the abutments may create a wet embankment.
    - \_\_\_\_\_ The phreatic line intersects the downstream slope.
    - \_\_\_\_\_ Special conditions exist that require drainage to ensure a stable embankment.
  - Seepage may be controlled by:
    - \_\_\_\_\_ A foundation, abutment or embankment drains.
  - \_\_\_\_\_ A downstream drainage blanket.
  - \_\_\_\_\_ A downstream toe drain (often desirable for homogeneous embankments).
  - A combination of these measures.
  - Seepage along pipe conduits that extend through an embankment should be controlled by use of the following to prevent piping failures along conduit surfaces:
    - \_\_\_\_\_ Anti-seep collar (provide detail).
      - \_\_\_\_\_ The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA no longer recommend the use of anti-seep collars, in deference to graded filters

or *filter diaphragms* and *drainage blankets* (more complex to design, but less complicated and more cost-effective to construct and allow for easier placement of fill material).

- Size, based on the length of pipe in the saturation zone (aim is a minimum 15% increase in seepage length).
- \_\_\_\_\_ Spacing and location of collars on barrel:
  - Maximum collar spacing is 14 times the minimum projection above the pipe.
  - \_\_\_\_\_ Minimum collar spacing is 5 times the minimum projection above the pipe.
  - Collar dimensions should extend a minimum of 2 feet in all directions around the pipe.
- Anti-seep collars should be placed within the saturation zone. Where the spacing limit will not allow this, then at least one collar must be in the saturation zone.
- All anti-seep collars and their connections to the conduit should be completely water-tight and made of material compatible with the conduit. NOTE: Dimple bands are *not* considered water-tight.
- \_\_\_\_\_ Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
- Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless flanged joints are used.
- Collars size should be calculated using the procedure specified in Chapter 13 of the Virginia Stormwater Management Handbook (2011).
- \_ The embankment filter and drainage diaphragm should be designed by a professional geotechnical engineer.
  - \_\_\_\_\_ These devices channel seepage flow through a filter of fine graded material, such as sand, which traps any embankment material being transported.
    - \_\_\_\_\_ The flow is then conveyed out of the embankment through a perforated toe drain or other acceptable technique.
    - The critical design element: the filter material grain size distribution is based on the grain size distribution of the embankment fill and foundation material.
      - The diaphragm should consist of sand, meeting fine concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than 10% passing the No. 100 sieve).
      - The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to rock, whichever is encountered first.
      - \_\_\_\_\_ The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam.
      - \_\_\_\_\_ The diaphragm should be discharged at the downstream toe of the embankment.
      - \_\_\_\_\_ The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria.
      - \_\_\_\_\_ A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings.
      - \_\_\_\_\_ Fabric should *not* be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.

5. Foi	undation and Cut Off Trench or Key Trench
	Label all materials
	The presence of rock in the embankment foundation area requires specific design and construction recommendations (provided by the geotechnical engineering analysis) to ensure a proper bond between the foundation and the embankment.
	Generally, no blasting should be permitted within 100 feet of the foundation and abutment area. If blasting is necessary, it should be carried out under controlled conditions to reduce
	adverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.), especially critical in karst topography.
	Show the cut-off trench bottom width (4 foot minimum or greater as specified in the geotechnical report).
	<ul> <li>Show the cut-off trench depth (4 foot minimum or as specified in the geotechnical report)</li> <li>Show the cut-off trench side slopes (no steeper than 1H:1V).</li> </ul>
6. Mu	Iti Stage Riser and Barrel System
	Principal spillways should be sized according to calculation procedures in Chapter 13 of the <i>Virginia Stormwater Management Handbook (2011).</i>
	_ The principal spillway should be located within the embankment and accessible from dry land to ensure easy access for maintenance.
	Access to the riser should be provided by lockable manhole covers and manhole steps within easy reach of valves and other controls.
	Provide a schedule of materials and clearly label them in drawings.
	_ Drop inlet spillways (riser and barrel system) should be designed as follows:
	Full flow is established in the outlet conduit and riser at the lowest hydraulic head over
	the riser crest that is feasible. Indicate the crest elevation of riser structure. The facility must operate without excessive surging, noise, vibration, or vortex action at any stage.
	Therefore, the riser must have a larger cross-sectional area than the outlet conduit.
	_ Headwall or conduit spillways consist of a pipe extending through an embankment with a headwall at the upstream end. The headwall is typically oversized to provide an adequate surface against which to compact the embankment fill.
	_ Weir spillways should be designed as follows:
	When used as the principal spillway, it should be armored with concrete or other non- erosive material.
	At the spillway, armoring should extend from the upstream face of the embankment to a point downstream of the spillway toe.
	_ All principal spillways should be constructed of non-erosive material with an anticipated life expectancy similar to that of the stormwater management facility.
	Pre-cast riser structures may <i>not</i> be substituted if the plans call for a cast-in-place structure, unless approved by the design engineer and the plan approving authority. Sections of pre-cast structures must be anchored together to meet stability and flotation
	requirements.
	A separate principal spillway and emergency spillway is generally recommended, unless: Topography/abutments are too steep.
	<ul> <li>Existing or proposed development conditions impose constraints.</li> <li>Other factors (e.g., a road embankment is used as the dam, the basin is excavated, etc.)</li> </ul>
	In such instances, a combined principal/emergency spillway that passes both low flows and extreme flows may be considered for use, in the form of a drop inlet spillway, a headwall/conduit spillway, or some other design that achieves equivalent results. It is very important to protect such combined spillways from clogging.
	Conduits/structures through embankments: Limit the number of conduits that penetrate through the embankment.
	Indicate the barrel diameter, inverts, and slope (%).
	Show the inverts and dimensions of control release orifices/weirs

\_\_\_ Show the structure dimensions

- \_\_\_\_\_ Show the extended detention (if added) orifice protection
- NOTE: A cause of embankment failure is the separation of pipe joints due to differential settlement and pipe deflection.
  - All connections to pipes must be completely water-tight.
    - The drain pipe (or barrel) connection to the riser should be welded all around when both are metal.
      - \_\_\_\_\_ A rubber or neoprene gasket should be used when joining pipe sections.
      - The end of each pipe should be re-rolled by enough corrugations to fit the band width.
    - \_\_\_\_\_ Helically corrugated pipe should have either continuous welded seams or lock seams with internal caulking or a neoprene bead.
    - \_\_\_\_\_ The following connection types are acceptable:
      - \_\_\_\_\_ For pipes less than 24 inches in diameter:
        - \_\_\_\_\_ Flanges with gaskets on both ends of the pipe
        - A 12-inch wide standard lap type band with a 12-inch wide by ½-inch thick closed cell circular neoprene gasket.
          - A 12-inch wide hugger type band with O-ring gaskets having a minimum diameter of 3/8 inch greater than the corrugation depth.
        - \_ For pipes  $\exists$  24 inches in diameter:
          - \_\_\_\_\_ A 24-inch long annular corrugated band using rods and lugs.
            - \_\_\_\_\_ A 24-inch wide by 3/8 inch thick closed cell circular neoprene gasket.
    - Corrugated metal pipe (CMP) must meet or exceed the minimum required design thickness.
      - Steel pipe and its appurtenances should be galvanized and fully bituminouscoated and should conform to the requirements of AASHTO Specification M-190 Type A with water-tight coupling bands.
        - Any bituminous coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.
        - Steel pipes with polymeric coatings should have a minimum coating thickness of 0.01 inches (10 mils) on both sides of the pipe.
        - Coated corrugated steel pipe should meet the requirements of AASHTO M-245 and M-246; the following coatings or an approved equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu-Loy.
      - Aluminum coated steel pipe and its appurtenances should conform to the requirements of AASHTO Specification M-274 with water-tight coupling bands or flanges.
        - Any aluminum coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.

Aluminum pipe and its appurtenances should conform to the requirements of AASHTO Specification M-196 or M-211 with water-tight coupling bands or flanges.

- Aluminum surfaces that are to be in contact with concrete should be painted with one coat of zinc chromate primer, and hot-dipped galvanized bolts may be used for connections.
  - \_ The pH of the surrounding soils should be between 4 and 9.

\_\_\_\_\_ The contractor and project inspector should verify the metal thickness, corrugation size, proper connecting bands, and gasket type.

Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.

- \_\_\_\_\_ Water-tight joints are necessary to prevent infiltration of embankment soils into the conduit.
  - All joints must be constructed as specified by the pipe manufacturer.

Field joints (the ends of the pipes are cut off in the field) should not be accepted. With larger pipe sizes, it may be difficult to get water-tight joints, even if the deflection is within design parameters. In such cases, the designer may choose to specify a heavier gage pipe. Bands: All connectors must be composed of the same material as the pipe. Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick. 6-inch hugger bands and "dimple bands" should not be accepted for CMP conduits. For pipes  $\leq$  24 inches in diameter, use 12-inch wide bands with 12-inch O-ring or flat neoprene gaskets. For larger pipes, use 24-inch wide bands with 24-inch wide flat gaskets and four "rod and lug" type connectors. Flanged pipe with gaskets may also be used. All pipe gaskets should be properly lubricated with the material provided by the manufacturer, and tensioned, to prevent deterioration of the gasket material. Flat gaskets must be factory welded or solvent-glued into a circular ring, with no overlaps or gaps The pipe should be firmly and uniformly bedded throughout its length: Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support. Under no conditions should gravel bedding be placed under a conduit through the embankment. Installation of a concrete pipe cradle will help to reduce the risk of piping under the barrel and the subsequent failure of the embankment, resulting from differential settlement. The concrete cradle may not be necessary along the entire length of the conduit to prevent piping, but it is recommended since gravel bedding under an embankment conduit is never appropriate unless it is designed as a filter or drainage diaphragm If the external load (e.g., from height of the embankment, anticipated construction traffic, the weight of compaction equipment, etc.) on the barrel is enough to warrant provision for its maximum supporting strength, then a concrete cradle should be installed along the conduit's entire length. Reinforced concrete pipe should have bell and singular spigot joints with rubber gaskets and should equal or exceed ASTM Designation C-361. Bell and spigot pipe should be placed with the bell end upstream. Joints should be made consistent with manufacturer recommendations. After the joints are sealed for the entire run of pipe, the bedding should be placed so that all spaces under the pipe are filled. All reinforced concrete pipe conduits should be laid in a concrete bedding for their entire length. This bedding should consist of high slump concrete placed under the pipe and up the sides of the pipe at least 25% of its outside diameter, and preferably to the spring line, with a minimum thickness of 3 inches, or otherwise as shown on the drawings. Care should be taken to prevent any deviation from the original line and grade of the pipe. Polyvinyl Chloride (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM D-1785 or ASTM D-2241. Joints and connections to anti-seep collars should be completely water-tight.

The pipe should be firmly and uniformly bedded throughout its length.

- Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.
- \_\_\_\_\_ All conduits penetrating dam embankments should be designed using the following criteria:
  - Conduits and structures penetrating an embankment should have a smooth surface without protrusions or indentations that will hinder compaction of embankment materials.
  - All conduits should be circular in cross-section except cast-in-place reinforced concrete box culverts. This is also true where multiple conduits are employed.
  - Conduits should be designed to withstand the external loading from the proposed embankment without yielding, buckling or cracking, all of which will result in joint separation.
  - Conduit strength should not be less than the values shown in the design specifications for corrugated steel, aluminum, and PVC pipes, and the applicable ASTM standards for other materials.
    - The designer or contractor should obtain a manufacturer's certification that the pipe meets plan requirements for design load, pipe thickness, joint design, etc.
  - \_\_\_\_\_ Inlet and outlet flared-end sections should be made from materials that are compatible with the pipe.
  - \_\_\_\_\_ All pipe joints should be made water-tight by using flanges with gaskets, coupling bands with gaskets, bell and spigot ends with gaskets, or by welding.
    - Where multiple conduits are employed, sifficient space should be provided between the conduits and installed anti-seep collars to allow for backfill material to be placed between the conduits with earth-moving equipment and easy access by hand-operated compaction equipment.
      - The distance between conduits should be  $\exists$  1/2 of the pipe diameter, but not less than 2 feet.
- Cathodic protection should be provided for *coated welded steel* and *galvanized corrugated metal pipe* when soil and resistivity studies indicate the need for a protective coating against acidic soils.
- Outlet protection must be used for the downstream toe of a spillway structure to help dissipate the high-energy flow through the spillway and to prevent excessive erosion in the receiving channel.
  - \_\_\_\_\_ The type of outlet protection depends on the flow velocities associated with the spillway.
    - \_ Riprap is the preferred form of outlet protection, designed according to Chapter 13 of the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet protection material.
      - \_\_\_\_\_ The bottom of the riprap apron should be constructed at 0% slope along its length.
      - \_\_\_\_\_ The end of the apron should match the grade and alignment of the receiving channel.
      - If the receiving channel is well-defined, the riprap should be place on the channel bottom and side slopes (no steeper than 2H:1V) for the entire length, as required in the design criteria in Chapter 13 of the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992).
        - Riprap placement should not alter the channel's geometry.
      - Excavation of the channel bed and banks may be required to construct the full thickness of the apron.
      - \_\_\_\_\_ If the barrel discharges into the receiving channel at an angle, the opposite bank must be protected up the 10-year storm elevation. In no instance should the total length of outlet protection be shortened.

- If a permit requires that no work may be performed in the stream or channel, then the outlet structure must be moved back to allow for adequate protection.
- \_\_\_\_\_ The horizontal alignment of the apron should have no bends within the design length.
- \_\_\_\_\_ Additional riprap should be placed if a significant change in grade occurs at the downstream end of the outfall apron.
  - Filter fabric should be placed between the riprap and the underlying soil to prevent soil movement into and through the riprap.
- \_ All control structures should have a trash rack or debris control device, designed as follows:
  - All trash rack and debris control components should be made of stainless steel or galvanized metal meeting VDOT specifications.
  - Trash racks attached to a concrete spillway structure should be secured with stainless steel anchor bolts.
  - Openings for trash racks should be no larger than 1/2 of the minimum conduit dimension and, to discourage child access, bar spacing should be no greater than 1 foot apart. The clear distance between the bars on large storm discharge openings generally should be no less than 6 inches.
  - \_\_\_\_\_ Flat grates for trash racks are *not* acceptable.
  - Inlet structures that have flow over the top should have a non-clogging trash rack (e.g., a hood-type inlet that allows passage of water from underneath the trash rack into the riser, or a vertical or sloped grate).
  - \_\_\_\_\_ The designer should verify that the surface area of the vertical perimeter of a raised grate equals the area of the horizontal top opening, to allow adequate flow passage should the top horizontal surface become clogged.
  - \_\_\_\_\_ Metal trash racks and monitoring hardware should be constructed of galvanized or stainless steel.
  - Methods to prevent clogging of extended detention orifices in dry extended detention bains should be carefully designed, since these orifices are usually very small and located at the invert or bottom of the basin.
- \_ All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (*not* required if weir control is maintained in the riser through all flow stages, including the maximum design storm or safety storm):
  - \_\_\_\_\_ The device may be a baffle or plate installed on top of the riser, or a headwall set on one side of the riser.
- \_ The design of a principal spillway riser structure should include a *flotation* or *buoyancy* calculation (see Chapter 13 of the *Virginia Stormwater Management Handbook, 2011*).
  - The downward force of the riser and footing (to which the riser must be firmly attached) is the *structure weight*, which must be 1.25 times greater than the buoyant force acting on the riser.
- Stormwater management facilities having permanent impoundments may be designed so that the permanent pool can be drained to simplify maintenance and sediment removal.
  - The draining mechanism will usually consist of a valve or gate attached to the spillway structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris control device.
  - \_\_\_\_\_ The typical configuration of a drainpipe will place the valve inside the riser structure with the pipe extending out to the pool area.
    - \_\_\_\_\_ This configuration results in the drainpipe being pressurized by the hydraulic head associated with the permanent pool.
    - Pressurized pipes should have mechanical joints in order to avoid possible leaks and seepage resulting from the innate pressure.
    - In all cases, valves should be secured to prevent unauthorized draining of the facility.
    - Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that sediment removal and other maintenance functions are not hampered.

An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in the saturated upstream slope of the dam embankment or shoreline area.

\_\_\_\_\_ Therefore, the design of the basin drain system should include specific operating instructions for the owner.

- Generally, the drawdown rate should not exceed 6 inches per day.
- For embankment or shoreline slopes of clay or silt, the drawdown rate may be as low as 1 inch per week to ensure slope stability.
- may be as low as 1 inch per week to ensure

### 7. Emergency Spillway

- Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the abutments at one or both ends of an earthen embankment or over a topographic saddle anywhere on the periphery of the basin. They should *never* be located on any portion of the embankment fill material.
- Excavated emergency spillways consist of three elements:
  - An inlet channel, through which *subcritical* flow enters the spillway.
    - The inlet channel should have a straight alignment and grade.
    - \_\_\_\_\_ The cross-sectional area of flow in the inlet channel should be large in comparison to the flow area at the control section.
    - Where the depth of the channel changes to provide for the increased flow area, the bottom width should be altered gradually to avoid abrupt changes in the shape of the sloping channel banks.
  - \_\_\_\_ A level section, which controls the depth of flow.
    - The maximum design water surface elevation (normally for the 100-year storm) through the emergency spillway should be at least 1 foot lower than the settled top of the embankment and should be confined by undisturbed earth or rock.
    - \_\_\_\_\_ The bottom width of the spillway should not exceed 35 times the design depth of flow, to avoid damage by meandering flow and accumulated debris.
    - Whenever the required bottom width is likely to be excessive, consideration should be given to incorporation of a spillway at each end of the dam.
      - \_\_\_\_\_ The two spillways do not need to be of equal width if their total capacity meets design requirements.
  - An exit channel, through which either *critical* or *supercritical* flow discharges from the spillway
    - \_\_\_\_\_ The alignment of the exit channel must be straight to a point far enough below the embankment to ensure that any flow escaping the exit channel cannot damage the embankment.
      - \_\_\_\_ The exit channel should have the same cross-section as the control section.
    - \_\_\_\_\_ The slope of the exit channel must be:
      - \_\_\_\_\_ Adequate to discharge the peak flow within the channel.
        - No greater than that which will produce maximum permissible velocities for the soil type or the planned grass cover.
          - \_\_\_\_ The slope range of the exit channel is selected to ensure *supercritical* flow in the channel.
  - The control section is the point on the spillway where the flow passes through *critical* depth, usually installed close to the intersection of the earthen embankment and the emergency spillway centerlines.
  - The type of soil and vegetative cover used in the emergency spillway will influence the spillway design dimensions and geometry.
    - Vegetation provides a degree of retardance to the flow through the spillway, depending mostly on the height and density of the vegetative cover chosen.

Hydraulic design for emergency spillways must be done in accordance with criteria provided in *Appendix C: Vegetated Emergency Spillways* of the *Introduction to the New Virginia Stormwater Design Specifications* (as posted on the Virginia Stormwater BMP Clearinghouse web site at <a href="http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html">http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html</a>) and in Chapter 13 of the *Virginia Stormwater Management Handbook (2011)*.

Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.

Show the existing ground and proposed improvements along the center line of the emergency spillway

# C. Landscape Plan

- \_\_\_\_\_ The landscaping plan should be jointly developed by the design engineer and a wetlands expert or experienced landscape architect
- \_\_\_\_\_ It may be advisable to use a subcontractor who specializes in aquatic landscaping.
- The plan should outline a detailed schedule for the installation, care, maintenance and possible reinforcement or replacement of vegetation in the wetland and its buffer for up to 10 years after the original planting.
- The plan should indicate how appropriate wetland plants will be established within each inundation zone (e.g., wetland plants, seed mixes, volunteer colonization, tree and shrub stock, etc.) and whether soil amendments are needed to get plants started.
- \_\_\_\_\_ Include a plan view with topography at a contour interval of no more than 1 foot and spot elevations throughout the cell showing the wetland configuration, different planting zones, microtopography, grades, site preparation, and construction sequence.
- Provide a planting schedule and specifications (transport / storage / installation / maintenance) for emergent, perennial, shrub and tree species, quantity of each species, stock size, type of root stock to be installed, and spacing.
  - *Plan early.* As much as 6 to 9 months of lead time may be needed to fill orders for wetland plant stock from aquatic plant nurseries.
  - Plant stock should be nursery grown (unless otherwise approved by the local regulatory authority) and should be healthy and vigorous native species free from defects, decay, disfiguring roots, sun-scald, injuries, abrasions, diseases, insects, pests, and all forms of infestations or objectionable disfigurements.
  - Plant selection must be appropriate for the site's vegetation climatic zone (6-8 in Virginia)
    - Plant materials should be wet-footed species but must be able to withstand both wet and dry periods as well as relatively high velocity flows within the swale.
    - If the swale is adjacent to a roadway where winter conditions will require the use of road salts in the CDA, then salt-tolerant non-woody plant species should be specified.
    - \_\_\_\_\_ To the degree feasible, the species list should contain native species found in similar local wetlands.
    - \_\_\_\_\_ Plant 5 to 7 species of emergent wetland plants, with at least four (4) of these designated as aggressive colonizers.
    - No more than 25% of the high marsh surface area needs to be planted, with individual plants 18 inches on center within each single species cluster. If done properly, the entire wetland should be colonized within three years.
      - Trees and shrubs should be integrated into the design in tree islands, peninsulas, and fringe buffer areas (Level 2 design).
        - \_\_\_\_\_ Trees may be planted in clusters to share rooting space on compacted wetland side slopes.
        - Planting holes should be amended with compost (a 2:1 ratio of loose soil to compost) prior to planting.
      - \_\_\_\_\_ Vary the size and age of the plant stock to promote a diverse structure.
    - Plants should be kept in containers of water or moist coverings to protect their root systems and keep them moist when transporting them to the planting location.
      - Buffer areas should be over-planted with a small stock of fast-growing successional species to achieve quick canopy closure and shade out invasive plant species.
  - The construction contract should include a *Care and Replacement Warranty* that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.
  - \_\_\_ Specify preservation measures for existing vegetation

#### **D.** Construction Notes

- \_\_\_\_ Ideally, planned constructed wetland areas should be clearly marked off and remain *outside* the limits of land disturbance during construction to prevent soil compaction by heavy equipment.
  - Constructed wetland areas may be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the facility will be de-watered, dredged and re-graded to design dimensions after the original site construction is complete.
- Ideally, stormwater wetlands should be constructed during months that are best for establishing vegetative cover without irrigation (February 15 April 15; September 15 November 15).
- In some cases, it will be necessary to divert flow while the stormwater wetland is being constructed, so that no sediment flows into the wetland area until installation and stabilization are complete.
  - Flow diversions may be required to meet additional requirements of and obtain permits from state and federal regulatory agencies.
  - Construction sequence (Phase 1: Wetland construction):
    - Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications.
      - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
        - \_\_\_\_ The following are critical inspection points:
          - During initial site preparation and installation of E&S Controls.
          - Excavation and grading (e.g., interim and final elevations).
          - Embankment construction
          - \_\_\_\_\_ Wetland installation (e.g., microtopography, soil amendments, and staking of planting zones)
            - Planting phase (with the wetland expert or landscape architect).
    - \_\_\_ Check the proposed site for existing utilities prior to any excavation.
    - \_\_\_\_\_ Assemble the construction materials on-site, making sure they meet design specifications, and prepare any staging areas.
    - Clear, grub and strip the areas designated for borrow sites, embankment construction, and structural work to the desired subgrade, removing all trees, vegetation, roots and other objectional material.
      - \_\_\_\_\_ All cleared and grubbed material should be disposed of outside and below the limits of the embankment and reservoir.
      - When specified, a sufficient quantity of topsoil should be stockpiled in a suitable location for use on the embankment and other designated areas.
      - Install applicable temporary E&S control measures prior to construction.
    - Areas surrounding the wetland area that are graded or denuded during construction of the wetland must be planted with turf grass, native plant materials or other approved methods of soil stabilization. Grass sod is preferred over grass seed, to prevent seed colonization of the wetland.
    - Excavate the core trench for the embankment and install the spillway (outlet) pipe, including the downstream rip-rap apron (energy dissipation) protection..
      - The cutoff trench should be excavated into impervious material along or parallel to the centerline of the embankment.
      - Trench side slopes should be laid back in steps at a 1H:1V slope or flatter. (from page 6; conflicts with 2:1 specified on page 10, Earthen Embankment Spec?).
        - Backfill should be compacted with construction equipment, rollers, or hand tampers to assure maximum density and minimum permeability.
      - Install the riser pipe or overflow structure, ensuring the top invert of the overflow weir is constructed level and at the proper design elevation (flashboard risers are strongly recommended).

Construct the embankment and any internal berms in 8- to 12-inch lifts, compacted with appropriate equipment. Areas on which fill is to be placed should be scarified before its placement. The most permeable borrow material should be placed in the downstream portions of the embankment. Install the principal spillway or overflow weir concurrently with fill placement and not excavated into the embankment. A vertical trench through the embankment material (in order to place the spillway pipe) should not be allowed under any circumstances. Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands. Filter and Drainage Lavers: In order to achieve maximum density of clean sands, filter layers should be flooded with clean water and vibrated just after the water drops below the sand surface. The filter material should be placed in lifts of no more than 12 inches in thickness. Up to 4 feet of embankment material may be laced over a filter material layer before excavating back down to expose the previous layer. After removing any unsuitable materials, the trench may be filled with additional 12-inch lifts of filter material, flooded, and vibrated as described above, until the top of adjacent fill is reached. The contractor should ensure that a qualified professional inspect filter and drainage diaphragms, ensuring that backfill material meets specifications for quality, lift thickness, placement, moisture content, and dry unit weight. Fill material should be taken from an approved, designated borrow area or stockpile. Fill material should be free of roots, stumps, wood, rubbish, stones greater than 6 inches in diameter, and frozen or other objectionable materials. Fill material for the center of the embankment and the cutoff trench should conform to Unified Soil Classification GC. SC. or CL. Fill material that is beside pipes or structures should be of the same type and quality as specified for the adjoining fill material. The fill material should be placed in horizontal lifts not to exceed 4 inches in thickness and compacted by hand tampers or other manually directed compaction equipment. The material should completely fill all spaces under and beside the pipe. \_\_\_\_ During backfilling, equipment should not be driven closer the 4 feet horizontally to any part of a structure. Equipment should NEVER be driven over any part of a structure or pipe, unless compacted fill has been placed to a depth specified by the structural live load capacity of the structure or pipe, that adequately distributes the load. Consideration may be given to the use of other materials in the embankment based on the recommendation of a geotechnical engineer supervising the design and construction. The surface layer of compacted fill should be scarified prior to placement of at least 6 inches of topsoil, which must be properly stabilized.

Fill material should be compacted with appropriate compaction equipment.

- The number of necessary passes by the compaction equipment over the fill material may vary with soil conditions.
- Fill material should contain sufficient moisture so that the required degree of compaction will be obtained with the equipment used.

The minimum required density is 95% of maximum dry density with a moisture content within  $\pm$  2% of the optimum, unless otherwise specified by the engineer.

Each layer of fill should be compacted as necessary to obtain minimum density.

\_\_\_\_\_ Compaction tests should be performed regularly throughout the embankment construction.

Typically, one test per 5,000 sq. ft. on each layer of fill or as directed by the geotechnical engineer.

Use either a Standard Proctor Test (ASTM D698) or a Modified Proctor Test (ASTM D1557 – usually more appropriate for earthen dams).

A new Proctor test is required if the material changes from that previously tested.

The engineer should certify, at the time of construction, that each fil layer meets the minimum density.

- A geotechnical or construction inspector should be on site during embankment construction to do the following:
  - \_\_\_\_ Test fill compaction

Observe foundation preparation.

- \_\_\_\_\_ Observe pipe installation.
- Observe riser construction.
- \_\_\_\_\_ Observe filter installation, etc.

Construct the emergency spillway in cut or structurally stabilized soils.

- Excavate/grade until the appropriate elevations and desired contours are achieved for the bottom and side slopes of the wetland.
  - \_\_\_\_\_ Rough up the interim elevations with a skid loader or other similar equipment to achieve the desired topography across the wetland.
    - \_\_\_\_\_ Spot surveys should be made to ensure that the interim elevations for the wetland are 3 to 6 inches below the final elevations.

Install micro-topographic features and soil amendments (essential for wetland plant survival).

Planting soil within the wetland should be loam or sandy loam with a high organic content, placed by mechanical methods, and spread by hand to a depth of at least 4 inches for shallow wetlands.

\_\_\_\_\_ Planting soil should be tamped as directed in the design specifications, but it should not be overly compacted.

- After the planting soil is placed, it should be saturated and allowed to settle for at least one week prior to installation of plant materials.
- \_\_\_\_\_ No machinery should be allowed to traverse over the planting soil during or after construction.
- Stabilize exposed soils with temporary seed mixtures appropriate for a wetland environment. All wetland features above the normal pool elevation should be temporarily stabilized by hydro-seeding or seeding over straw.

Construction sequence (Phase 2: Establishing wetland vegetation):

Finalize the wetland landscaping plan. Several weeks standing time is needed following wetland construction so that the designer can more precisely predict the following two things:

\_\_\_\_\_ Where the inundation zones are located in and around the wetland.

\_\_\_\_\_ Whether the final grade and wetland microtopography will persist over time.

- Selection of appropriate species and additional soil amendments, based on actual field confirmation of soil properties and the actual depths and inundation frequencies occurring within the wetland.
- Open up the wetland construction, to allow the wetland cell(s) to fill up to normal pool elevation.
  - \_\_\_\_\_ Inundation must occur in stages so the deep pool and high marsh plant materials can be placed effectively and safely.
    - \_\_\_\_\_ Wetland planting areas should be at least partially inundated during planting to promote plant survivability.
- \_\_\_\_\_ Measure (to the nearest inch) and stake planting depths at the onset of the planting season.
  - It may be necessary to modify the planting plan to reflect altered depths or a change in the availability of wetland plant stock.

\_\_\_\_\_ Surveyed planting zones should be marked on the as-built or design plan, and the locations should be identified in the field, using stakes or flags.

- Propagate the stormwater wetland between mid-April and mid-June, using three simultaneous techniques to prapogate the emergent community over the wetland bed:
  - \_\_\_\_\_ Initial planting of container-grown wetland plant stock.
  - Broadcast wetland seed mixes over the higher wetland elevations, to establish diverse emergent wetlands.
    - Seeding of switchgrass or wetland seed mixes as a ground cover is recommended for all zones above 3 inches below the normal pool elevation.
    - Hand broadcasting or hydroseeding can be used to spread seed, depending on the size of the wetland cell.
  - Allow volunteer plants from upstream or the forest buffer to establish on their own (over the next 3 to 5 years).
  - Install goose protection for newly planted or newly growing vegetation, especially emergents and herbacious plants.
    - Place netting, webbing, or string installed in a criss-cross pattern over the surface area of the wetland above the level of the emergent plants.
- Plant the wetland fringe and buffer area in the zone generally extending from 1 to 3 feet above the normal pool elevation (from the shoreline fringe to about half of the maximum water surface elevation for the 2-year storm) with vegetation that can tolerate both wet and dry periods.
- Implement any remaining permanent stabilization measures.
- Conduct a final inspection, log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including installation/maintenance of safety signage; removal and disposal of trash, debris and sediment accumulations; and periodic harvesting and disposal of overgrown or old wetland plant materials. The narrative should also include a list of qualified contractors that can perform inspection and maintenance services plus contact information for local or state assistance to solve common nuisance problems.
- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the constructed wetland area is not disturbed or converted to other uses.
- Provide sufficient facility access from the public ROW or roadway to both the constructed wetland and any pre-treatment practices.

# **IV. COMMENTS**

By:	Date:
Ву:	Date:

# 8-A.15.0. WET PONDS: DESIGN CHECKLIST

Plan Submission Date Project Name Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number
Signature and stamp of license certification	d professional design consultant and owner
Plan Status	
Approved L	Legend: Complete
Not Approved	<u>Inc.</u> - Incomplete/Incorrect <u>N/A</u> - Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration:	Turne of wetlende in comparate de
On-line facility	Type of wetlands incorporated:
Off-line facility	<ul> <li>Emergent</li> <li>Forested</li> </ul>
Wet Pond Configuration:	Type of Pre-Treatment Facility:
□ Wet Pond with 100% of	Sediment forebay (above ground)
permanent pool in a single cell	<ul> <li>Vegetated buffer area</li> </ul>
Wet ED and/or multi-cell Wet	Grass filter strip
Pond	Grass channel
Pond/Wetland Combination	□ Other:
regulated under the Virginia Dam Safety Provide a concise narrative describing this practice fits into the overall plan, and Show the location of this BMP on the site The basin pool area The contributing drainage area ( acres) and land cover, suffici constructed wetland. Delineation of FEMA 100-year fla Areas of the site compensated fo Areas of the site compensated fo Provide topography for the site area. Provide the geotechnical report with r description of any borrow area involved. Provide a soil map for site and area of fa Show the soil boring locations and provi and soil descriptions. Borings should be taken belo	CDA) boundaries, acreage (typically between 10 and 25 ient to sustain a permanent water level within the oodplain or in the water quality calculations recommendations and earthwork specifications and a acility, including the CDA ide the soil boring logs with Unified Soils Classifications ow the proposed embankment, in the vicinity of the cleast two locations within the planned basin treatment eristics of the soils regarding:

\_\_\_\_ Bearing capacity, buoyancy, etc. pertaining to outlet structure design.

\_\_\_\_\_ Compaction/composition needs for the embankment.

- \_\_\_\_\_ Depth to groundwater bedrock.
  - Depth to seasonal high groundwater table: if the water table is close to the surface, it may make excavation difficult and expensive, and groundwater inputs can also reduce the pollutant removal rates of wet ponds.
    - \_\_\_\_ Evaluation of potential infiltration losses (and the consequent need for a liner).
- Wet ponds are generally not recommended to be used in karst areas and should be the option of last resort. If karst is present, a detailed geotechnical investigation is recommended to ensure the wet pond does not aggravate potential karst impacts (e.g., sinkholes, groundwater contamination, etc.):
  - \_\_\_\_\_ A minimum of 6 feet of unconsolidated soil material must exist between the bottom of the pond and the top of the underlying karst layer.
  - \_\_\_\_\_ The maximum temporary or permanent water elevation with the basin must not exceed 6 feet.
  - \_\_\_\_\_ Employ an impermeable liner that meets the requirements of Stormwater Design Specification No. 14.
  - Annual maintenance inspections must be conducted to detect sinkhole formation. Sinkholes that develop should be reported immediately after they have been observed and should be repaired, abandoned, adapted or observed over time following the guidance prescribed by the appropriate local or state groundwater protection authority.
- \_\_\_\_ The use of wet ponds is constrained in coastal plain sites due to flat terrain, low hydraulic head and high water table (constructed wetlands are preferred). Wet ponds may be considered *acceptable* in coastal settings if the following design considerations apply:
  - Slightly lower nutrient removal rates are assigned to coastal plain wet ponds.
  - If a "pocket pond" (one that has a small CDA and is supplied solely by groundwater and runoff) is constructed in a coastal setting, then it must meet the minimum design geometry requirements for all ponds, in order to avoid nuisance conditions.

\_ The use of wet ponds is highly constrained at sites with steep terrain.

- \_ May be able to terrace pond cells in a linear configuration where slopes do not exceed 10% by using a 1 to 2 foot armored elevation drop between individual cells.
- \_ Where cold winter climates are typical, make the following adjustments:
  - \_\_\_\_\_ Treat larger runoff volumes in the spring by adopting seasonal operation of the permanent pool.
  - \_\_\_\_\_ Plant salt-tolerant vegetation at pond benches (to deal with higher chloride content of road salts).
  - \_\_\_\_\_ Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage ice formation.
  - \_\_\_\_\_ Locate low-flow orifices so they withdraw at least 6 inches below the typical ice layer.
- \_\_\_\_\_ Angle trash racks to prevent ice formation.
  - Over-size the riser and weir structures to avoid ice formation and freezing pipes.
- If road sanding is prevalent in the CDA, increase the forebay size by 25% to accommodate additional sediment loading.
- Wet ponds are poorly suited to treat runoff within open channels located in highway rights-ofway, unless storage is available in a cloverleaf interchange or in an expanded right-of-way and special VDOT design criteria are used.
- \_\_\_\_\_ Wet ponds are generally *not* recommended in watersheds containing trout streams, due to the potential for stream warming.
- A wet pond should *not* be built within an existing perennial stream or natural wetland nor should a wet pond discharge to jurisdictional waters without local/state/federal approvals and the necessary permit(s).
- \_\_\_\_\_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).
  - \_\_\_\_\_ The designer should check to see whether sediments removed from the forebay can be spoiled (deposited) on-site or must be hauled away.

# **II. COMPUTATIONS**

## A. Hydrology

- \_\_\_\_\_ Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrograph (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
- Confirm that there is adequate drainage area and/or water balance from groundwater, runoff or baseflow so the wet pond will not experience unacceptable drawdown after a 30-day summer drought (minimum 24-inch deep reservoir recommended).

# B. Hydraulics

- \_\_\_\_\_ Specify assumptions and coefficients used.
- Typically, 6 to 8 feet of hydraulic head are need to drive flow through the wetland.
- Provide a stage-storage table and curve
  - Weir/orifice control analysis for riser structure discharge openings and riser crest.
    - Carefully design the low-flow orifice to minimize clogging, as follows:
      - All outlet pipes should be adequately protected by an acceptable external trash racks or by internal orifice protection that may allow for smaller diameters.
      - Recommend a minimum 3-inch diameter orifice to minimize clogging of an outlet or extended detention pipe when it is surface-fed (still susceptible to clogging from floating vegetation and debris).
      - Smaller openings (down to 1-inch in diameter) are permissible, using internal orifice plates within the pipe.
      - Another option is a submerged reverse-slope pipe that extends downward from the riser to an inflow point 1 foot below the normal pool elevation.
      - Alternative methods must employ a broad-crested rectangular V-notch (or proportional) weir, protected by a half-round CMP that extends at least 12 inches below the normal pool elevation.
  - Barrel: Conduct an inlet/outlet control analysis
- Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
- Conduct appropriate calculations for use as a temporary sediment basin riser with clean out schedule & instructions for conversion to a permanent facility.
- Provide for large storm overflow or bypass: emergency spillway adequacy/capacity analysis (100-year design storm) with required embankment freeboard.
- Provide a stage-discharge table and curve (provide equations).
- Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required)
- Provide storm drainage and hydraulic grade line calculations.

# C. Downstream impacts

- Conduct a danger reach study.
- \_\_\_\_\_ Describe the 100 year floodplain impacts.
- Provide downstream hydrographs at critical study points.
  - Demonstrate safe conveyance to an "adequate" receiving channel.
    - If the receiving channel is natural and (1) has never been enhanced or "restored, OR (2) if tream channel erosion or localized flooding is an existing predevelopment condition, then conduct appropriate "energy balance" calculations to demonstrate safe conveyance from the facility to the receiving channel" (provide computations).

#### D. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - \_ Indicate the treatment volume for extended detention (if added) with draw-down calculation
- \_\_\_\_ Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 14.

#### **III. PLAN REQUIREMENTS**

#### A. BMP Plan View Information

- Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
- \_\_\_\_\_ Setbacks (local codes rule):
  - \_\_\_\_\_ Minimum 20 feet from property lines.
    - Minimum 25 feet from building foundations.
  - Minimum 100 feet from septic system drainfields and private wells.
- Pre-Treatment:
  - \_\_\_\_\_ Show all pre-treatment practices.
  - \_\_\_\_ A sediment forebay should be considered an integral pre-treatment practice for all wet ponds.
    - \_\_\_\_\_ A forebay should be located at every major inlet to trap sediment and preserve the capacity of the main pond treatment cell.
    - \_\_\_\_\_ A major inlet is any individual storm drain inlet pipe or open channel conveying runoff from at least 10% of the wet pond's CDA.
    - The forebay is considered a separate cell in both Level 1 and Level 2 designs, formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabion baskets, etc.)
      - Show the location of the metered rod that monitors long-term sediment accumulation (in the center of the pool, as measured lengthwise along the low flow water travel path).
  - \_\_\_\_\_ Show the locations of all conveyance system outfalls (inlets) into basin
  - Show the layout and dimensions of basin features: permanent pool, sediment forebay, embankment, emergency spillway, basin side slopes, basin bottom, etc.
    - \_\_\_\_ The footprint is typically between 1% and 3% of the CDA, depending on the pond depth (deeper ponds need a smaller footprint).
  - Pool geometry
    - \_\_\_\_\_ Show the wet/dry weather flow path
    - Confirm the proper orientation to avoid short-circuiting
    - \_\_\_\_\_ Internal design geometry and depth zones are critical in maintaining the pollutant removal capability.
    - \_\_\_\_\_ Wet ponds should have an irregular shape and a long flow path from inlet to outlet, to increase water residence time and pond performance.
    - \_\_\_\_ Flow Path:
      - \_\_\_\_\_ Overall flow path through the wetland (length-to-width ratio):
        - Level 1 design: 2L:1W.
        - Level 2 design: 3L:1W.
        - \_\_\_ Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
          - Level 1 design: 0.5.
          - Level 2 design: 0.8.
            - If unable to meet these targets, then the drainage area served by these "closer" inlets should constitute no more than 20% of the total CDA.
      - Treatment volume storage may be provided by a combination of a permanent pool, a shallow marsh and/or extended detention storage.
        - \_\_\_\_\_ The permanent pool storage may be divided among multiple cells
        - Performance is enhanced by multiple treatment cells, longer flow paths, high surface area-to-volume ratios, and/or redundant treatment methods.

A berm or simple weir should be used instead of pipes to separate multiple pond cells.

\_\_\_\_\_ Stormwater pond benches:

A safety bench is a flat bench located just outside of the perimeter of the permanent pool to allow for maintenance access and reduce safety risks when the pond side slopes exceed 5H:1V.

The safety bench generally extends 8 to 15 feet outward from the normal water edge to the shoulder of the stormwater pond side slope.

An aquatic bench is a shallow area just inside the perimeter of the normal pool that promotes growth of aquatic and wetland vegetation.

- The bench also serves as a safety feature, reduces shoreline erosion, and conceals floatable trash.
- The bench should extend up to 10 feet inward from the normal shoreline and have an irregular configuration.
- Safety features:
  - \_\_\_\_ End walls above pipe outfalls greater than 48 inches in diameter must be fenced to prevent a hazard.
  - \_\_\_\_\_ The emergency spillway must be located so that downstream structures will not be impacted by spillway discharges.
  - Warning signs prohibiting swimming must be posted.
  - Show outlet protection per VE&SCH Std. & Spec. 3.18
    - \_\_\_\_\_ Must be stable for the 10-year design storm.
    - The channel immediately below the pond outfall must be modified to prevent erosion and conform to natural dimensions in the shortest possible distance.
      - This is done typically by placing appropriately-sized riprap over filter fabric, which can reduce flow velocities from the principal spillway to non-erosive levels (3.5 to 5 ft./sec.).
    - \_\_\_\_\_ Flared pipe sections, which discharge at or near the stream invert or into a step/plunge pool, should be used at the spillway outlet.
- Indicate the top-of-bank and basin bottom elevations
- Indicate the elevations of the permanent pool, the treatment volume and the maximum design water surface elevations for all appropriate design storms and safety storms
- \_\_\_\_\_ Show any shoreline protection provided
- NOTE: Fencing the perimeter of wet ponds is discouraged, except at or above the maximum water surface elevation in the rare instances when the pond slope is a vertical wall.
- Show the location and dimensions of the riser and barrel.
- \_\_\_\_\_ Identify the pool depth zones on the plan
- Identify any wetland/shallow marsh areas incorporated into the pond plan
  - Show sufficient maintenance access to the forebay, safety benches, riser structure, embankment, emergency spillway, basin shoreline, extended drawdown device, principal spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. Access roads must:
    - \_\_\_\_\_ Be constructed of load bearing materials.
    - \_\_\_\_\_ Have a minimum width of 12 feet.
    - Possess a maximum profile grade of 15%.
    - \_\_\_\_\_ Have sufficient turn-around area.
    - \_\_\_\_\_ A maintenance right-of-way or easement must extend to the stormwater pond from a public or private road.

### B. BMP Section Views & Related Details

### 1. Pre-Treatment

- The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no less than 0.1 inch per impervious acre.
  - For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total required pool or detention volume may be more practical.
  - This volume should be a maximum of 4 feet deep (or a depth determined by the summer drought water balance) near the inlet to adequately dissipate turbulent inflow without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wet pond cell.
  - The forebay should be equipped with a variable width aquatic bench around the perimeter of the 4-foot depth, for safety purposes. The aquatic bench should be4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.
  - \_ The volume of the forebay is part of the treatment volume of the stormwater basin for which it provides pre-treatment.

However, for dry facilities, the forebay does *not* represent available storage volume if it remains full of water.

A dry forebay must be carefully designed to avoid the resuspension of previously deposited sediments.

- The total volume of all forebays should be at least 15% of the total Treatment Volume. The relative size of individual forebays should be proportional to the percentage of their total inflow to the wet pond.
- Separation between the forebay and the main basin may be achieved through the use of an earthen berm, gabion baskets, concrete, or a riprap wall.
- A designed overflow section should be constructed on the top of the separation to allow flow to exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design storms.

\_ The overflow section may be set at the permanent pool elevation or the extended detention volume elevation.

- The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap) to make sediment removal easier.
- Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay and basin from excessive erosion from heavy equipment operation used for maintenance.
- Provide a typical grading section through the forebay, including typical side slopes, aquatic bench, shoreline protection, etc.

### 2. Embankment (or dam) and Ponding Areas

Indicate the type of embankment:

- \_\_\_ Homogenous embankment
- Zoned embankment

The earthen embankment must be designed to be stable against any force condition or combination of force conditions that may develop during the life of the structure (including differential settlement within the embankment, seepage through the embankment and foundation, or sharing stresses within the embankment and foundation) and is dependent upon:

- \_\_\_\_\_ Construction materials
- \_\_\_\_\_ Foundation conditions
- \_\_\_\_\_ Embankment height and cross-section geometry
- \_\_\_\_\_ Normal and maximum pool levels
- \_\_\_\_\_ Purpose of structure (i.e., retention, extended detention, etc.).

Embankment geometry:

- Top of dam elevations: constructed height and settled height (allowing for 10% settlement).
  - \_\_\_\_\_ Height (based on the freeboard requirements):
    - \_\_\_\_\_ There must be at least 1 foot of freeboard between the maximum 100year storm water surface elevation (WSE) to the lowest point on the top of the embankment (excluding the emergency spillway).
      - An embankment *without* an emergency spillway must provide at least 2 feet of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment.
      - \_ NOTE: The spillway design storm WSE, if specified, may be substituted for the 100-year storm WSE in either of the above situations.
- \_\_\_\_\_ The top width varies with embankment height and should be shaped to provide positive drainage.
- \_\_\_\_\_ The top of the embankment must be level in order to avoid possible overtopping in one location in cases of extreme storms or spillway failure.
- Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and 2H:1V upstream face).
- For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than 3H:1V.
  - \_\_\_\_\_ The slope profile within a wet pond should be at least 0.5% to 1% to promote positive flow through the pond.
- Pond side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth of wetland vegetation, provide for easier maintenance, and create a more natural appearance.
   Stormwater pond benches:
- \_ Stormwater pond benches:
  - \_\_\_\_ The maximum slope of the safety bench is 5%.
  - An aquatic bench should have a maximum depth of 18 inches below the normal pool water surface elevation.
- Liners: When a stormwater pond is located over highly permeable soils or fractured bedrock, a liner may be needed to sustain a permanent pool of water. Acceptable liners include (1) a clay liner consistent with the criteria in Stormwater Design Specification No. 14, (2) a 30-mil poly liner, (3) bentonite, (4) use of chemical soil additives, or (5) an engineering design approved by the local regulatory authority.
  - Inlet pipe inverts should generally be located at or slightly below the permanent pool elevation.
    - Inlet areas should be stabilized to ensure that non-erosive conditions exist during storm events up to the overbank flood event (10-year design storm).
- Since most wet ponds are typically on-line facilities, they need to be designed to safely pass the maximum design storm (e.g., the 10-year and 100-year design storms).
  - Level 1 designs may incorporate extended detention associated with the treatment volume of up to 12 inches of detention storage above the permanent pool (at least 10% of the Level 2 surface area) at its maximum water surface elevation. The maximum ED and channel protection detention levels can be up to 5 feet above the wet pond permanent pool elevation.
- Show the elevations of permanent pool, treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
- Proper surface area/depth allocations for permanent pool and any shallow marsh/constructed wetlands

- The embankment cross-section must be designed to provide an adequate factor of safety to protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability depends upon:
  - Physical characteristics of the fill materials
  - Configuration of the site
  - \_\_\_\_\_ Foundation materials
    - Shear strength
      - <u>Compressibility</u>
      - Permeability
- Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be designed so that the collection conduits discharge downstream of the embankment at a location where access for observation is possible by maintenance personnel.
- \_\_\_\_\_ Adequate erosion protection is recommended along the contact point between the face of the embankment and the abutments, where runoff concentrates.
  - Evaluate whether a gutter surface other than sod is necessary (riprap is generally preferred over a paved concrete gutter).
  - Pond drain: Except for flat areas of the coastal plain, each wet pond should have a drain pipe that can completely or partially drain the permanent pool.
    - In cases where a low level drain is not feasible (such as in an excavated pond), a pump wet well should be provided to accommodate a temporary pump intake when needed to drain the pond.
    - The drain pipe should have an up-turned elbow or protected intake within the pond, to prevent sediment deposition, and a pipe diameter capable of draining the pond within 24 hours.
    - The pond drain must be equipped with an adjustable valve located within the riser, where it will not be normally inundated and can be operated in a safe manner.
  - Trees, shrubs or any other woody plants should not be planted or allowed on the embankment or adjacent areas extending at least 25 feet beyond the embankment toe and abutment contacts.

\_\_\_\_\_ Safety features:

- \_\_\_\_\_ The principal spillway opening must be designed and constructed to prevent access by small children.
- An emergency spillway and associated freeboard must be provided in accordance with Stormwater Design Specification No. 14 and applicable local or state dam safety requirements.
  - \_\_\_\_\_ Manage the contours of the stormwater pond to eliminate drop-offs or other safety hazards.
- Indicate the top of embankment elevations: constructed height and settled height (allowing for 10% settlement).
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the embankment.
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the principal spillway
- Provide a typical grading section through the pond, including typical side slopes with the aquatic bench, shoreline protection, etc.
- \_\_\_\_\_ Show the dimensions of zones for any zoned embankment

#### 3. Seepage Control

- All utility conduits (except the principal spillway) should be installed away from the embankment.
  - When utility conduits through the embankment cannot be avoided, they should meet the requirements for spillways:
    - Watertight joints
    - No gravel bedding
    - \_\_\_\_\_ Restrained to prevent joint separation due to settlement

- The contact point between the embankment soil, the foundation material, and the conduit is the most likely location for *piping* to occur, due to the discontinuity in materials and the difficulty in compacting the soil around the pipe.
  - Phreatic line (4:1 slope measured from the principal spillway design high water elevation through the embankment) is the upper limit of the *saturation zone*..
    - \_\_\_\_ At a minimum, this should be the 10-year design storm water surface elevation.
    - If the phreatic line intersects the downstream slope of the embankment, a qualified soil scientist should be consulted to decide if additional controls, such as an internal drain, are needed.
    - Seepage control should be included in the design if the following conditions exist:
      - \_\_\_\_\_ Pervious layers in the foundation are not intercepted by the cutoff.
        - Possible seepage from the abutments may create a wet embankment.
        - The phreatic line intersects the downstream slope.
        - Special conditions exist that require drainage to ensure a stable embankment.
      - Seepage may be controlled by:
        - Foundation, abutment or embankment drains.
      - \_\_\_\_\_ A downstream drainage blanket.
        - A downstream toe drain (often desirable for homogeneous embankments).
        - A combination of these measures.
      - Seepage along pipe conduits that extend through an embankment should be controlled by use of the following to prevent piping failures along conduit surfaces:
        - \_\_\_\_ Anti-seep collar (provide detail).
          - The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA no longer recommend the use of anti-seep collars, in deference to graded filters or filter diaphragms and drainage blankets (more complex to design, but less complicated and more cost-effective to construct and allow for easier placement of fill material).
          - \_\_\_\_\_ Size, based on the length of pipe in the saturation zone (aim is a minimum 15% increase in seepage length).
          - \_\_\_\_\_ Spacing and location of collars on barrel:
            - \_\_\_\_\_ Maximum collar spacing is 14 times the minimum projection above the pipe.
            - \_\_\_\_\_ Minimum collar spacing is 5 times the minimum projection above the pipe.
            - Collar dimensions should extend a minimum of 2 feet in all directions around the pipe.
          - Anti-seep collars should be placed within the saturation zone. Where the spacing limit will not allow this, then at least one collar must be in the saturation zone.
          - All anti-seep collars and their connections to the conduit should be completely water-tight and made of material compatible with the conduit. NOTE: Dimple bands are *not* considered water-tight.
          - \_\_\_\_\_ Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
          - \_\_\_\_\_ Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless flanged joints are used.
            - Collars size should be calculated using the procedure specified in Chapter 13 of the *Virginia Stormwater Management Handbook (2011).*
        - \_\_\_\_\_ The embankment filter and drainage diaphragm should be designed by a professional geotechnical engineer.
          - \_\_\_\_\_ These devices channel seepage flow through a filter of fine graded material, such as sand, which traps any embankment material being transported.
          - \_\_\_\_\_ The flow is then conveyed out of the embankment through a perforated toe drain or other acceptable technique.
          - \_\_\_\_\_ The critical design element: the filter material grain size distribution is based on the grain size distribution of the embankment fill and foundation material.

The diaphragm should consist of sand, meeting fince concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than 10% passing the No. 100 sieve).

The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to rock, whichever is encountered first.

The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam.

\_\_\_\_\_ The diaphragm should be discharged at the downstream toe of the embankment.

\_\_\_\_\_ The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria.

A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings.

\_\_\_\_\_ Fabric should *not* be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.

# 4. Foundation and Cut Off Trench or Key Trench

# \_\_\_\_ Label all materials

- The presence of rock in the embankment foundation area requires specific design and construction recommendations (provided by the geotechnical engineering analysis) to ensure a proper bond between the foundation and the embankment.
  - Generally, no blasting should be permitted within 100 feet of the foundation and abutment area.
    - If blasting is necessary, it should be carried out under controlled conditions to reduce adverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.), especially critical in karst topography.

\_\_\_\_ Indicate the cut-off trench bottom width (4 foot minimum or greater as specified in the geotechnical report).

Indicate the cut-off trench depth (4 foot minimum or as specified in the geotechnical report)

Indicate the cut-off trench side slopes (no steeper than 1H:1V).

### 5. Multi Stage Riser and Barrel System

- Principal spillways should be sized according to calculation procedures in Chapter 13 of the *Virginia Stormwater Management Handbook (2011).* 
  - \_\_\_\_ The principal spillway should be located within the embankment and accessible from dry land to ensure easy access for maintenance.
    - Access to the riser should be provided by lockable manhole covers and manhole steps within easy reach of valves and other controls.
- Provide a schedule of materials and clearly label them in drawings.
- Drop inlet spillways (riser and barrel system) should be designed as follows:
  - Full flow is established in the outlet conduit and riser at the lowest hydraulic head over the riser crest that is feasible. Indicate the crest elevation of riser structure.
    - The facility must operate without excessive surging, noise, vibration, or vortex action at any stage.
    - \_\_\_\_ Therefore, the riser must have a larger cross-sectional area than the outlet conduit.
- Headwall or conduit spillways consist of a pipe extending through an embankment with a headwall at the upstream end. The headwall is typically oversized to provide an adequate surface against which to compact the embankment fill.
  - Weir spillways should be designed as follows:
    - \_\_\_\_\_ When used as the principal spillway, it should be armored with concrete or other nonerosive material.
    - \_\_\_\_\_ At the spillway, armoring should extend from the upstream face of the embankment to a point downstream of the spillway toe.

All principal spillways should be constructed of non-erosive material with an anticipated life expectancy similar to that of the stormwater management facility. Pre-cast riser structures may not be substituted if the plans call for a cast-in-place structure. unless approved by the design engineer and the plan approving authority. Sections of pre-cast structures must be anchored together to meet stability and flotation requirements. A separate principal spillway and emergency spillway is generally recommended, unless: Topography/abutments too steep. Existing or proposed development conditions impose constraints. Other factors (e.g., a road embankment is used as the dam, the basin is excavated, etc.) In such instances, a combined principal/emergency spillway that passes both low flows and extreme flows may be considered for use, in the form of a drop inlet spillway, a headwall/conduit spillway, or some other design that achieves equivalent results. It is very important to protect such combined spillways from clogging. Conduits/structures through embankments: Limit the number of conduits that penetrate through the embankment. Indicate the barrel diameter, inverts, and slope (%). Show the inverts and dimensions of control release orifices/weirs Show the structure dimensions Show the extended detention (if added) orifice protection A cause of embankment failure is the separation of pipe joints due to differential settlement and pipe deflection. All connections to pipes must be completely water-tight. \_\_\_\_\_ The drain pipe (or barrel) connection to the riser should be welded all around when both are metal. \_ A rubber or neoprene gasket should be used when joining pipe sections. \_\_\_\_\_ The end of each pipe should be re-rolled by enough corrugations to fit the band width. \_\_\_\_\_ Helically corrugated pipe should have either continuous welded seams or lock seams with internal caulking or a neoprene bead. The following connection types are acceptable: \_\_\_\_\_ For pipes less than 24 inches in diameter: Flanges with gaskets on both ends of the pipe A 12-inch wide standard lap type band with a 12-inch wide by <sup>1</sup>/<sub>2</sub>-inch thick closed cell circular neoprene gasket. \_\_\_\_ A 12-inch wide hugger type band with O-ring gaskets having a minimum diameter of 3/8 inch greater than the corrugation depth. For pipes  $\exists$  24 inches in diameter: A 24-inch long annular corrugated band using rods and lugs. \_\_\_\_\_ A 24-inch wide by 3/8 inch thick closed cell circular neoprene gasket. Corrugated metal pipe (CMP) must meet or exceed the minimum required design thickness. Steel pipe and its appurtenances should be galvanized and fully bituminouscoated and should conform to the requirements of AASHTO Specification M-190 Type A with water-tight coupling bands. Any bituminous coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound. Steel pipes with polymeric coatings should have a minimum coating thickness of 0.01 inches (10 mils) on both sides of the pipe. Coated corrugated steel pipe should meet the requirements of AASHTO M-245 and M-246; the following coatings or an approved equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu-

Loy.

- Aluminum coated steel pipe and its appurtenances should conform to the requirements of AASHTO Specification M-274 with water-tight coupling bands or flanges.
  - Any aluminum coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.
- Aluminum pipe and its appurtenances should conform to the requirements of AASHTO Specification M-196 or M-211 with water-tight coupling bands or flanges.
  - Aluminum surfaces that are to be in contact with concrete should be painted with one coat of zinc chromate primer, and hot-dipped galvanized bolts may be used for connections.
    - \_ The pH of the surrounding soils should be between 4 and 9.
- The contractor and project inspector should verify the metal thickness, corrugation size, proper connecting bands, and gasket type.
- Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.
- \_\_\_\_\_ Water-tight joints are necessary to prevent infiltration of embankment soils into the conduit.
  - \_\_\_\_\_ All joints must be constructed as specified by the pipe manufacturer.
    - Field joints (the ends of the pipes are cut off in the field) should *not* be accepted.
    - With larger pipe sizes, it may be difficult to get water-tight joints, even if the deflection is within design parameters.
  - In such cases, the designer may choose to specify a heavier gage pipe. Bands:
  - All connectors must be composed of the same material as the pipe.
  - Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
  - 6-inch hugger bands and "dimple bands" should not be accepted for CMP conduits.
  - For pipes  $\leq$  24 inches in diameter, use 12-inch wide bands with 12-inch O-ring or flat neoprene gaskets.
  - For larger pipes, use 24-inch wide bands with 24-inch wide flat gaskets and four "rod and lug" type connectors.
  - \_\_\_\_\_ Flanged pipe with gaskets may also be used.
  - All pipe gaskets should be properly lubricated with the material provided by the manufacturer, and tensioned, to prevent deterioration of the gasket material.
    - Flat gaskets must be factory welded or solvent-glued into a circular ring, with no overlaps or gaps
- \_\_\_\_\_ The pipe should be firmly and uniformly bedded throughout its length:
  - Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.
  - \_\_\_\_\_ Under no conditions should gravel bedding be placed under a conduit through the embankment.
- Installation of a concrete pipe cradle will help to reduce the risk of piping under the barrel and the subsequent failure of the embankment, resulting from differential settlement.
  - The concrete cradle may not be necessary along the entire length of the conduit to prevent piping, but it is recommended since gravel bedding under an embankment conduit is *never* appropriate unless it is designed as a filter or drainage diaphragm

If the external load (e.g., from height of the embankment, anticipated construction traffic, the weight of compaction equipment, etc.) on the barrel is enough to warrant provision for its maximum supporting strength, then a concrete cradle should be installed along the conduit's entire length.

Reinforced concrete pipe should have bell and singular spigot joints with rubber gaskets and should equal or exceed ASTM Designation C-361.

Bell and spigot pipe should be placed with the bell end upstream.

Joints should be made consistent with manufacturer recommendations.

After the joints are sealed for the entire run of pipe, the bedding should be placed so that all spaces under the pipe are filled.

All reinforced concrete pipe conduits should be laid in a *concrete* bedding for their entire length.

This bedding should consist of high slump concrete placed under the pipe and up the sides of the pipe at least 25% of its outside diameter, and preferably to the spring line, with a minimum thickness of 3 inches, or otherwise as shown on the drawings.

Care should be taken to prevent any deviation from the original line and grade of the pipe.

Polyvinyl Chloride (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM D-1785 or ASTM D-2241.

\_\_\_\_\_ Joints and connections to anti-seep collars should be completely water-tight.

\_\_\_\_\_ The pipe should be firmly and uniformly bedded throughout its length.

Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.

\_\_\_\_ All conduits penetrating dam embankments should be designed using the following criteria:

Conduits and structures penetrating an embankment should have a smooth surface without protrusions or indentations that will hinder compaction of embankment materials.

All conduits should be circular in cross-section except cast-in-place reinforced concrete box culverts. This is also true where multiple conduits are employed.

Conduits should be designed to withstand the external loading from the proposed embankment without yielding, buckling or cracking, all of which will result in joint separation.

Conduit strength should not be less than the values shown in the design specifications for corrugated steel, aluminum, and PVC pipes, and the applicable ASTM standards for other materials.

The designer or contractor should obtain a manufacturer's certification that the pipe meets plan requirements for design load, pipe thickness, joint design, etc.

\_\_\_\_\_ Inlet and outlet flared-end sections should be made from materials that are compatible with the pipe.

All pipe joints should be made water-tight by using flanges with gaskets, coupling bands with gaskets, bell and spigot ends with gaskets, or by welding.

Where multiple conduits are employed, sufficient space should be provided between the conduits and installed anti-seep collars to allow for backfill material to be placed between the conduits with earth-moving equipment and easy access by hand-operated compaction equipment.

The distance between conduits should be  $\exists$  1/2 of the pipe diameter, but not less than 2 feet.

Cathodic protection should be provided for *coated welded steel* and *galvanized corrugated metal pipe* when soil and resistivity studies indicate the need for a protective coating against acidic soils.

- \_\_\_\_\_ Outlet protection must be used for the downstream toe of a spillway structure to help dissipate the high-energy flow through the spillway and to prevent excessive erosion in the receiving channel.
  - \_\_\_\_\_ The type of outlet protection depends on the flow velocities associated with the spillway.
    - \_\_\_\_ Riprap is the preferred form of outlet protection, designed according to Chapter 13 of the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet protection material.
      - \_\_\_\_\_ The bottom of the riprap apron should be constructed at 0% slope along its length.
      - \_\_\_\_\_ The end of the apron should match the grade and alignment of the receiving channel.
      - If the receiving channel is well-defined, the riprap should be place on the channel bottom and side slopes (no steeper than 2H:1V) for the entire length, as required in the design criteria in Chapter 13 of the *Virginia Stormwater Management Handbook (2011)* and the *Virginia Erosion and Sediment Control Handbook (1992).*
      - Riprap placement should not alter the channel's geometry.
      - Excavation of the channel bed and banks may be required to construct the full thickness of the apron.
      - \_\_\_\_\_ If the barrel discharges into the receiving channel at an angle, the opposite bank must be protected up the the 10-year storm elevation. In no instance should the total length of outlet protection be shortened.
      - If a permit requires that no work may be performed in the stream or channel, then the outlet structure must be moved back to allow for adequate protection.
      - \_\_\_\_\_ The horizontal alignment of the apron should have no bends within the design length.
      - \_\_\_\_\_ Additional riprap should be placed if a significant change in grade occurs at the downstream end of the outfall apron.
      - Filter fabric should be placed between the riprap and the underlying soil to prevent soil movement into and through the riprap.
  - All control structures should have a trash rack or debris control device, designed as follows:
    - \_\_\_\_\_ All trash rack and debris control components should be made of stainless steel or galvanized metal meeting VDOT specifications.
    - Trash racks attached to a concrete spillway structure should be secured with stainless steel anchor bolts.
  - Openings for trash racks should be no larger than 1/2 of the minimum conduit dimension and, to discourage child access, bar spacing should be no greater than 1 foot apart. The clear distance between the bars on large storm discharge openings generally should be no less than 6 inches.
  - \_\_\_\_\_ Flat grates for trash racks are *not* acceptable.
  - Inlet structures that have flow over the top should have a non-clogging trash rack (e.g., a hood-type inlet that allows passage of water from underneath the trash rack into the riser, or a vertical or sloped grate).
  - \_\_\_\_\_ The designer should verify that the surface area of the vertical perimeter of a raised grate equals the area of the horizontal top opening, to allow adequate flow passage should the top horizontal surface become clogged.
  - \_\_\_\_\_ Metal trash racks and monitoring hardware should be constructed of galvanized or stainless steel.
  - Methods to prevent clogging of extended detention orifices in dry extended detention basins should be carefully designed, since these orifices are usually very small and located at the invert or bottom of the basin.
  - All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (*not* required if weir control is maintained in the riser through all flow stages, including the maximum design storm or safety storm):

The device may be a baffle or plate installed on top of the riser, or a headwall set on one side of the riser. The design of a principal spillway riser structure should include a *flotation* or *buoyancy* calculation (see Chapter 13 of the Virginia Stormwater Management Handbook, 2011). The downward force of the riser and footing (to which the riser must be firmly attached) is the structure weight, which must be 1.25 times greater than the buoyant force acting on the riser. Stormwater management facilities having permanent impoundments may be designed so that the permanent pool can be drained to simplify maintenance and sediment removal. The draining mechanism will usually consist of a valve or gate attached to the spillway structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris control device. The typical configuration of a drainpipe will place the valve inside the riser structure with the pipe extending out to the pool area. This configuration results in the drainpipe being pressurized by the hydraulic head associated with the permanent pool. Pressurized pipes should have mechanical joints in order to avoid possible leaks and seepage resulting from the innate pressure. In all cases, valves should be secured to prevent unauthorized draining of the facility. Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that

 sediment removal and other maintenance functions are not hampered.
 An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in the saturated upstream slope of the dam embankment or shoreline area.

\_\_\_\_\_ Therefore, the design of the basin drain system should include specific operating instructions for the owner.

Generally, the drawdown rate should not exceed 6 inches per day.

For embankment or shoreline slopes of clay or silt, the drawdown rate may be as low as 1 inch per week to ensure slope stability.

#### 6 Emergency Spillway

Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the abutments at one or both ends of an earthen embankment or ovr a topographic saddle anywhere on the periphery of the basin. They should *never* be located on any portion of the embankment fill material.

Excavated emergency spillways consist of three elements:

\_\_\_\_ An inlet channel, through which *subcritical* flow enters the spillway.

The inlet channel should have a straight alignment and grade.

The cross-sectional area of flow in the inlet channel should be large in comparison to the flow area at the control section.

Where the depth of the channel changes to provide for the increased flow area, the bottom width should be altered gradually to avoid abrupt changes in the shape of the sloping channel banks.

\_\_\_\_\_ A level section, which controls the depth of flow.

The maximum design water surface elevation (normally for the 100-year storm) through the emergency spillway should be at least 1 foot lower than the settled top of the embankment and should be confined by undisturbed earth or rock.

The bottom width of the spillway should not exceed 35 times the design depth of flow, to avoid damage by meandering flow and accumulated debris.

\_\_\_\_\_ Whenever the required bottom width is likely to be excessive, consideration should be given to incorporation of a spillway at each end of the dam.

\_\_\_\_\_ The two spillways do not need to be of equal width if their total capacity meets design requirements.

 An exit channel,	through	which	either	critical	or	supercritical	flow	discharges	from	the
spillway	Ũ							Ū.		

The alignment of the exit channel must be straight to a point far enough below the embankment to ensure that any flow escaping the exit channel cannot damage the embankment.

- \_\_\_\_\_ The exit channel should have the same cross-section as the control section.
  - The slope of the exit channel must be:
    - \_\_\_\_\_ Adequate to discharge the peak flow within the channel.

No greater than that which will produce maximum permissible velocities for the soil type or the planned grass cover.

- The slope range of the exit channel is selected to ensure *supercritical* flow in the channel.
- \_\_\_\_\_ The control section is the point on the spillway where the flow passes through *critical* depth, usually installed close to the intersection of the earthen embankment and the emergency spillway centerlines.

The type of soil and vegetative cover used in the emergency spillway can be used to establish the spillway design dimensions and geometry.

\_\_\_\_ Vegetation provides a degree of retardance to the flow through the spillway, depending mostly on the height and density of the vegetative cover chosen.

- Hydraulic design for emergency spillways must be done in accordance with criteria provided in *Appendix C: Vegetated Emergency Spillways* of the *Introduction to the New Virginia Stormwater Design Specifications* (as posted on the Virginia Stormwater BMP Clearinghouse web site at <u>http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html</u>) and in Chapter 13 of the *Virginia Stormwater Management Handbook (2011).*
- Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.
   Show the existing ground and proposed improvements along the center line of the emergency spillway

### C. Landscape Plan

- \_\_\_\_\_ The landscaping plan must indicate the methods to be used to establish and maintain vegetative cover in the Wet Pond and its buffer area, including the following:
  - \_\_\_\_\_ Delineation of pondscaping zones within both the pond and buffer.
  - \_\_\_\_\_ Selection of corresponding plant species.
  - \_\_\_\_\_ The planting plan.
  - \_\_\_\_\_ The sequence for preparing the wetland benches (including soil amendments, if needed).
  - \_\_\_\_\_ Sources of native plant material.
  - Elements that promote diverse wildlife and waterfowl use within the wet pond and buffer.
  - \_\_\_\_\_ Woody vegetation may not be allowed to grow within 15 feet of the toe of the embankment nor within 25 feet from the principal spillway structure.
  - \_\_\_\_\_ A vegetated buffer should be provided that extends at least 25 feet outward from the maximum water surface elevation of the wet pond.
  - Permanent structures (e.g., buildings) should *not* be constructed within the buffer area.
  - \_\_\_\_\_ Existing trees within the buffer area should be preserved during construction.
  - \_\_\_\_\_ Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for container-grown stock.
  - \_\_\_\_\_ Avoid species that require full shade, or are prone to wind damage.
    - Extra mulching around the base of trees and shrubs is strongly recommended as a means of conserving moisture and suppressing weeds.
  - Provide a planting schedule and specifications (transport / storage / installation / maintenance)
- Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
  - \_\_\_\_\_ Specify preservation measures for existing vegetation
- Ensure that topsoil / planting soil is included in final grading plan.

#### **D.** Construction Notes

- \_\_\_\_\_ Ideally, planned wet pond areas should be constructed after the contributing drainage area is completely stabilized.
- Wet pond areas *may* be used during construction as sites for temporary sediment traps or basins (properly sized for E&S control purposes), provided the construction plans include notes and graphical details specifying the facility will be de-watered, dredged and re-graded to design dimensions after the original site construction is complete.
  - Installation of the permanent riser should be initiated during the construction phase
  - Design elevations should be set with final cleanout of the sediment basin and conversion to the post-construction wet pond in mind.
  - \_\_\_\_\_ The bottom elevation of the permanent wet pond should be lower than the bottom elevation of the temporary sediment basin.
  - Appropriate procedures should be implemented to prevent discharge of turbid waters when the basin is being converted into a wet pond.
  - In some cases, it will be necessary to divert flow while the wet pond is being constructed, so that no sediment flows into the pond area until installation and stabilization are complete.
    - Flow diversions may be required to meet additional requirements of and obtain permits from state and federal regulatory agencies.
    - \_\_\_ Construction sequence:
      - Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications.
        - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
        - The following are critical inspection points:
          - \_\_\_\_\_ During initial site preparation and installation of E&S Controls.
          - Excavation and grading (e.g., interim and final elevations).
          - Installation of the embankment, the riser/primary spillway, and the outlet structure.
            - \_\_\_\_ Pondscaping installation and final stabilization.
        - \_\_\_\_ Check the proposed site for existing utilities prior to any excavation.
      - Assemble the construction materials on-site, making sure they meet design specifications, and prepare any staging areas.
        - Clear, grub and strip the areas designated for borrow sites, embankment construction, and structural work to the desired subgrade, removing all trees, vegetation, roots and other objectional material.
          - \_\_\_\_\_ All cleared and grubbed material should be disposed of outside and below the limits of the embankment and reservoir.
          - When specified, a sufficient quantity of topsoil should be stockpiled in a suitable location for use on the embankment and other designated areas.
          - \_ Install applicable temporary E&S control measures prior to construction.
      - Excavate the core trench for the embankment and install the spillway (outlet) pipe, including the downstream rip-rap apron (energy dissipation) protection.
        - The cutoff trench should be excavated into impervious material along or parallel to the centerline of the embankment.
        - Trench side slopes should be laid back in steps at a 1H:1V slope or flatter. (from page 6; conflicts with 2:1 specified on page 10, Earthen Embankment Spec?).
        - Backfill should be compacted with construction equipment, rollers, or hand tampers to assure maximum density and minimum permeability.
      - Install the riser pipe or overflow structure, ensuring the top invert of the overflow weir is constructed level and at the proper design elevation.
      - Construct the embankment and any internal berms in 8- to 12-inch lifts, compacted with appropriate equipment.
        - \_\_\_\_\_ Areas on which fill is to be placed should be scarified before its placement.

- \_\_\_\_\_ The most permeable borrow material should be placed in the downstream portions of the embankment.
- Install the principal spillway or overflow weir concurrently with fill placement and not excavated into the embankment. A vertical trench through the embankment material (in order to place the spillway pipe) should not be allowed under any circumstances.
  - Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands.

\_\_\_\_ Filter and Drainage Layers:

- In order to achieve maximum density of clean sands, filter layers should be flooded with clean water and vibrated just after the water drops below the sand surface.
- The filter material should be placed in lifts of no more than 12 inches in thickness.
- Up to 4 feet of embankment material may be laced over a filter material layer before excavating back down to expose the previous layer.
- After removing any unsuitable materials, the trench may be filled with additional 12-inch lifts of filter material, flooded, and vibrated as described above, until the top of adjacent fill is reached.
- The contractor should ensure that a qualified professional inspect filter and drainage diaphragms, ensuring that backfill material meets specifications for quality, lift thickness, placement, moisture content, and dry unit weight.
- Fill material should be taken from an approved, designated borrow area or stockpile.
  - Fill material should be free of roots, stumps, wood, rubbish, stones greater than 6 inches in diameter, and frozen or other objectionable materials.
  - Fill material for the center of the embankment and the cutoff trench should conform to Unified Soil Classification GC, SC, or CL.
  - Fill material that is beside pipes or structures should be of the same type and quality as specified for the adjoining fill material.
    - The fill material should be placed in horizontal lifts not to exceed 4 inches in thickness and compacted by hand tampers or other manually directed compaction equipment.
    - \_\_\_\_\_ The material should completely fill all spaces under and beside the pipe.
    - \_\_\_\_\_ During backfilling, equipment should not be driven closer the 4 feet horizontally to any part of a structure.
    - Equipment should *NEVER* be driven *over* any part of a structure or pipe, unless compacted fill has been placed to a depth specified by the structural live load capacity of the structure or pipe, that adequately distributes the load.
  - Consideration may be given to the use of other materials in the embankment based on the recommendation of a geotechnical engineer supervising the design and construction.
  - The surface layer of compacted fill should be scarified prior to placement of at least 6 inches of topsoil, which must be properly stabilized.
  - \_\_\_\_ Fill material should be compacted with appropriate compaction equipment.
    - The number of necessary passes by the compaction equipment over the fill material may vary with soil conditions.
    - Fill material should contain sufficient moisture so that the required degree of compaction will be obtained with the equipment used.

- The minimum required density is 95% of maximum dry density with a moisture content within  $\pm$  2% of the optimum, unless otherwise specified by the engineer.
- \_\_\_\_\_ Each layer of fill should be compacted as necessary to obtain minimum density.
- Compaction tests should be performed regularly throughout the embankment construction.
  - Typically, one test per 5,000 sq. ft. on each layer of fill or as directed by the geotechnical engineer.
  - Use either a Standard Proctor Test (ASTM D698) or a Modified Proctor Test (ASTM D1557 – usually more appropriate for earthen dams).
  - A new Proctor test is required if the material changes from that previously tested.
  - The engineer should certify, at the time of construction, that each fil layer meets the minimum density.
- A geotechnical or construction inspector should be on site during embankment construction to do the following:
  - \_\_\_\_\_ Test fill compaction
  - Observe foundation preparation.
  - Observe pipe installation.
  - Observe riser construction.
    - Observe filter installation, etc.
- Construct the emergency spillway in cut or structurally stabilized soils.
- Excavate/grade until the appropriate elevations and desired contours are achieved for the bottom and side slopes of the pond.
- Install outlet pipes, including the downstream rip-rap apron (energy dissipation) protection.
- Stabilize exposed soils with temporary seed mixtures appropriate for the pond buffer. All areas above the normal pool elevation should be temporarily stabilized by hydroseeding or seeding over straw.
- \_\_\_\_\_ Plant the pond buffer area and implement any remaining permanent stabilization measures.
- \_\_\_\_\_ Conduct a final inspection, log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including installation/maintenance of safety signage; removal and disposal of trash, debris and sediment accumulations; mowing; and periodic harvesting and disposal of overgrown or old aquatic plant materials.
- Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the wet pond is not converted to other uses.
- Provide sufficient facility access from the public ROW or roadway to both the wet pond and any pre-treatment practices.

# **IV. COMMENTS**

-		
-		
-		
	Ву:	Date:

# 8-A.16.0. EXTENDED DETENTION PONDS: DESIGN CHECKLIST

Plan Submission Date		
Project Name Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
BMP Designer		Phone Number
General Contractor		
<u></u> Signature and stamp certification	of licensed profession	onal design consultant and owner
Plan Status		
Approved	Legend:	Complete
Not Approved		Inc Incomplete/Incorrect N/A - Not Applicable
Facility Type: Level 1	Le	vel 2
Design Configuration	Turne	
Design Configuration:		of Pre-Treatment Facility: Sediment forebay (above ground)
<ul> <li>Wet ED Pond (see Stormwate</li> </ul>		Vegetated buffer area
Design Specification No. 14)		Grass filter strip
□ Limited ED above Wetlands (		Grass channel
Stormwater Design Specificat		Other:
No. 13)		<u> </u>
Hydraulic Configuration:		
□ On-line facility		
Off-line facility		
I. SUPPORTING INFORMATION		
ED ponds with high embank	ments or large drainage a	reas and impoundments may be regulated
under the Virginia Dam Safe		
		ter management strategy, describing how
		ssumptions made in the design.
Show the location of this BM		ng:
The basin pool area		
		aries, acreage and land cover, sufficient to
	t water level within the con A 100-year floodplain	nstructed wetland.
	nsated for in water quality	v calculations
		pond area, its CDA and any pre-treatment
practices.	the area, mendaling the ED	pond area, its ODA and any pre-treatment
•	eport with recommendat	ions and earthwork specifications and a
description of any borrow are		
Provide a soil map for site a		ig the CDA
		oring logs with Unified Soils Classifications
and soil descriptions.		
Borings should be		sed embankment, in the vicinity of the
proposed outlet are	a, and in at least two loc	ations within the planned basin treatment
area.		

Determine the physical characteristics of the soils regarding:

- \_\_\_\_\_ Infiltration rate: infiltration through the bottom of the pond is encouraged unless it will impair the integrity of the embankment.
- Suitability for use as structural fill or spoil.
- Bearing capacity, buoyancy, etc. pertaining to outlet structure design.
- \_\_\_\_\_ Compaction/composition needs for the embankment.
- \_\_\_\_\_ Depth to groundwater and bedrock not less than 2 feet below the floor of the pond.
  - \_ Evaluation of potential infiltration losses (and the consequent need for a liner).
- ED ponds are normally combined with other stormwater treatment options within those facilities (e.g., wet pond, constructed wetland) to enhance their performance and appearance.
- \_ ED ponds are generally discouraged for use in karst areas and should be considered the practice of last resort. If karst is present, a detailed geotechnical investigation is recommended to ensure the ED pond does not aggravate potential karst impacts (e.g., sinkholes, groundwater contamination, etc.):
  - A minimum of 3 feet of unconsolidated soil material must exist between the bottom of the pond and the top of the underlying karst layer.
  - Employ an impermeable liner that meets the requirements of Stormwater Design Specification No. 13 (Constructed Wetlands).
  - Annual maintenance inspections must be conducted to detect sinkhole formation. Sinkholes that develop should be reported immediately after they have been observed and should be repaired, abandoned, adapted or observed over time following the guidance prescribed by the appropriate local or state groundwater protection authority.
    - \_\_\_\_ The use of ED ponds is constrained in coastal plain sites due to flat terrain, low hydraulic head and high water table (constructed wetlands are preferred).

\_\_\_\_ The use of ED ponds is highly constrained at sites with steep terrain.

- \_ Where cold winter climates are typical, make the following adjustments:
  - Plant salt-tolerant vegetation at pond benches (to deal with higher chloride content of road salts).
  - \_\_\_\_\_ Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage standing water and ice formation.
- Place all pipes below the frost line to prevent frost heave and pipe freezing.
- Locate low-flow orifices in the micropool, so they withdraw at least 6 inches below the typical ice layer.
- \_\_\_\_\_ Angle trash racks to prevent ice formation.
- \_\_\_\_\_ If road sanding is prevalent in the CDA, increase the forebay size by 25% to accommodate additional sediment loading.
- ED ponds are poorly suited to treat runoff within open channels located in highway rights-ofway, unless storage is available in a cloverleaf interchange or in an expanded right-of-way and special VDOT design criteria are used.
  - \_ ED ponds are generally *not* recommended in watersheds containing trout streams, due to the potential for stream warming.
    - However, where other upland runoff reduction practices cannot meet the full Channel Protection Volume requirement, a micropool ED pond may be used if the following criteria are met:
      - \_\_\_\_\_ It must be designed with a maximum 12-hour detention time
      - It must have a minimum pool volume sufficient to prevent clogging
      - It must be planted with trees so it becomes fully shaded
      - It must be located outside of any required stream buffer areas.
- An ED pond should *not* be built within an existing perennial stream or natural wetland nor should an ED pond discharge to jurisdictional waters without local/state/federal approvals and the necessary permit(s).
- \_\_\_\_\_ Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.).
- \_\_\_\_\_ The designer should check to see whether sediments removed from the forebay can be spoiled (deposited) on-site or must be hauled away.

# **II. COMPUTATIONS**

# A. Hydrology

- Determine runoff curve number (pre- and post-developed conditions), providing the worksheets.
- \_\_\_\_\_ Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
- Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
- Ensure that there is adequate drainage area and/or base flow

# **B. Hydraulics**

\_\_\_\_\_ Specify assumptions and coefficients used.

- Typically, 6 to 10 feet of hydraulic head are need to drive flow through the wetland.
- Provide a stage-storage table and curve
  - Average treatment volume extended detention drawdown time is 24 hours or less for Level 1 designs and 36 hours or less for Level 2 designs.
  - \_\_\_\_\_ Vertical treatment volume fluctuation may exceed 4 feet for Level 1 designs but may not exceed 4 feet for Level 2 designs.
  - Weir/orifice control analysis for riser structure discharge openings and riser crest.
    - \_\_\_\_\_ Consider providing a micropool at the outlet structure.
      - The micropool should be designed to that the depth will not draw down by more than 2 feet during a 30 day summer drought, but should be at least 4 feet deep.
      - \_\_\_\_\_ Use a submerged reverse-slope pipe that extends downward from the riser to an inflow point at mid-depth of the normal pool or micropool.
      - Install a down-turned elbow or half-round CMP over a riser orifice (circular, rectangular, V-notch, etc.) to pull water from at least 12 inches below the micropool surface.
  - \_\_\_\_\_ Use a perforated pipe under a gravel blanket with an orifice control at the end in the riser structure to supplement the primary outlet.
    - \_\_\_\_\_ Carefully design the low-flow orifice to minimize clogging, as follows:
      - All outlet pipes should be adequately protected by an acceptable external trash racks or by internal orifice protection that may allow for smaller diameters.
      - Recommend a minimum 3-inch diameter orifice to minimize clogging of an outlet or extended detention pipe when it is surface-fed (still susceptible to clogging from floating vegetation and debris).
        - \_\_\_\_\_ Smaller openings (down to 1-inch in diameter) are permissible, using internal orifice plates within the pipe.
- Barrel: Conduct an inlet/outlet control analysis
- Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
- Conduct appropriate calculations for use as a temporary sediment basin riser with clean out schedule & instructions for conversion to a permanent facility.
- Provide for large storm overflow or bypass: emergency spillway adequacy/capacity analysis (100-year design storm) with required embankment freeboard.
- Provide a stage-discharge table and curve (provide equations).
- Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required)
- Provide storm drainage and hydraulic grade line calculations.

# C. Downstream impacts

- Conduct a danger reach study.
- \_\_\_\_\_ Describe the 100 year floodplain impacts.
- Provide downstream hydrographs at critical study points.

Demonstrate safe conveyance to an "adequate" receiving channel.

If the receiving channel is natural and (1) has never been enhanced or "restored, OR (2) if stream channel erosion or localized flooding is an existing predevelopment condition, then conduct appropriate "energy balance" calculations to demonstrate safe conveyance from the facility to the receiving channel" (provide computations).

# D. Water Quality

- Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
  - \_\_\_\_ Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 15.

# III. PLAN REQUIREMENTS

# A. BMP Plan View Information

\_\_\_\_ Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.

\_\_\_ Setbacks (local ordinances rule):

- Minimum 10 feet from property lines.
- \_\_\_\_\_ Minimum 25 feet from building foundations.
- Minimum 50 feet from septic system drainfields
- \_\_\_\_\_ Minimum 100 feet from private wells.

Pre-Treatment:

\_\_\_\_\_ Show all pre-treatment practices.

- A sediment forebay should be considered an integral pre-treatment practice for all ED ponds. Consider providing an over-sized forebay to trap sediment, trash and debris before it reaches the ED pond's low-flow orifice.
  - The forebay is considered a separate cell in both Level 1 and Level 2 designs, formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabion baskets, etc.). Any outlet protection associated with the end section or end wall should be designed according to state and local standards.
  - A forebay should be located at every major inlet to trap sediment and preserve the capacity of the main pond treatment cell.
  - A major inlet is any individual storm drain inlet pipe or open channel conveying runoff from at least 10% of the ED pond's CDA.
  - \_\_\_\_\_ The relative size of individual forebays should be proportional to the percentage of the total inflow to the ED Pond.
  - The total volume of all forebays should be at least 15% of the total Treatment Volume (inclusively, thereby satisfying the Level 1 design permanent pool volume requirement). However, a micropool is still encouraged for maintenance benefits.
  - The outlet from each forebay should be designed in such a manner that it acts as a level spreader to distribute runoff evenly across the entire bottom surface area of the main basin treatment cell. Therefore, there should be no low-flow pilot channel constructed in the basin bottom.
  - Show the location of the metered rod that monitors long-term sediment accumulation (in the center of the pool, as measured lengthwise along the low flow water travel path).
- \_ Show the locations of all conveyance system outfalls (inlets) into basin
  - Inlets should be stabilized to ensure that non-erosive conditions exist during storm events up to the overbank flood event (the 10-year storm).
  - \_\_\_\_\_ Inlet pipe inverts should generally be located at or slightly below the forebay pool elevation.
- \_ Show the layout and dimensions of basin features: permanent pool, sediment forebay, embankment, emergency spillway. basin side slopes, basin bottom, etc.

- \_ The footprint is typically between 1% and 3% of the CDA, depending on the pond depth (a deeper pond needs a smaller footprint).
- \_\_\_\_ Pool geometry wet/dry weather flow path
  - Internal design geometry and depth zones are critical in maintaining the pollutant removal capability.
  - \_\_\_\_\_ Ensure proper orientation and inlet locations to avoid short-circuiting
  - \_\_\_\_\_ Ensure that there is adequate surface area
  - Show the wet/dry weather flow path:
    - \_\_\_\_\_ Overall flow path through the wetland (length-to-width ratio):
      - Level 1 design: 2L:1W.
      - Level 2 design: 3L:1W.
      - \_\_\_\_\_ Internal berms, baffles or topography can be used to extend flow paths and/or create multiple pond cells.
      - Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
        - Level 1 design: 0.4.
        - Level 2 design: 0.7.
          - \_ If unable to meet these targets, then the drainage area served by these "closer" inlets should constitute no more than 20% of the total CDA.
    - The permanent pool storage may be divided among multiple cells
      - A berm or simple weir should be used instead of pipes to separate multiple pond cells.
      - \_\_\_\_ ED pond benches:
        - A safety bench is a flat bench located just outside of the perimeter of the permanent pool to allow for maintenance access and reduce safety risks when the pond side slopes exceed 5H:1V.
          - The safety bench generally extends 8 to 15 feet outward from the normal water edge to the shoulder of the stormwater pond side slope.
        - An aquatic bench is a shallow area just inside the perimeter of the normal pool that promotes growth of aquatic and wetland vegetation.
          - The bench also serves as a safety feature, reduces shoreline erosion, and conceals floatable trash.
          - The bench should extend up to 10 feet inward from the normal shoreline and have an irregular configuration.
        - Both the safety bench and the aquatic bench should be landscaped with vegetation that hinders or prevents access to the pool.
        - Micropool ED ponds should *not* have a low flow pilot channel, but instead must be constructed in a manner whereby flows are evenly distributed across the pond bottom, to promote the maximum infiltration possible.
  - \_\_\_ Other safety features:
    - \_\_\_\_\_ End walls above pipe outfalls greater than 48 inches in diameter must be fenced to prevent a hazard.
    - \_\_\_\_\_ The emergency spillway must be located so that downstream structures will not be impacted by spillway discharges.
  - \_\_\_ Outlet protection per VE&SCH Std. & Spec. 3.18
    - \_\_\_\_\_ Stable for the 10-year design storm.
    - The channel immediately below the pond outfall must be modified to prevent erosion and conform to natural dimensions in the shortest possible distance.
      - This is done typically by placing appropriately-sized riprap over filter fabric, which can reduce flow velocities from the principal spillway to non-erosive levels (3.5 to 5 ft./sec.).
    - Flared pipe sections, which discharge at or near the stream invert or into a step/plunge pool, should be used at the spillway outlet.
- Indicate the top-of-bank and basin bottom elevations
  - Indicate the elevations of permanent pool, treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms

- \_\_\_\_\_ Fencing the perimeter of ED ponds is discouraged, except at or above the maximum water surface elevation in the rare instances when the pond slope is a vertical wall.
- \_\_\_\_\_ Identify the riser and barrel materials and label their dimensions
- Identify the pool depth zones on the plan, ensuring adequate surface area for each depth zone
- Provide sufficient maintenance access to the forebay, micropool, safety benches, riser structure, embankment, emergency spillway, basin shoreline, extended drawdown device, principal spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. Access roads must:
  - \_\_\_\_\_ Be constructed of load bearing materials able to withstand the expected frequency of use.
  - \_\_\_\_\_ Have a minimum width of 12 feet.
  - Possess a maximum profile grade of 15%.
  - Have sufficient turn-around area.
    - A maintenance right-of-way or easement must extend to the stormwater basin from a public or private road.

# B. BMP Section Views & Related Details

# 1. Pre-Treatment

- \_\_\_\_\_ The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no less than 0.1 inch per impervious acre.
  - \_\_\_\_\_ For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total required pool or detention volume may be more practical.
    - This volume should be a maximum of 4 feet deep (or a depth determined by the summer drought water balance) near the inlet to adequately dissipate turbulent inflow without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wetland cell.

The forebay should be equipped with a variable width aquatic bench around the perimeter of the 4-foot depth, for safety purposes. The aquatic bench should be 4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.

\_\_\_\_ The volume of the forebay is part of the treatment volume of the stormwater basin for which it provides pre-treatment.

- However, for dry facilities, the forebay does *not* represent available storage volume if it remains full of water.
  - \_\_\_\_\_ A dry forebay must be carefully designed to avoid the resuspension of previously deposited sediments.
- The total volume of all forebays should be at least 15% of the total Treatment Volume. The relative size of individual forebays should be proportional to the percentage of their total inflow to the ED pond.
- \_\_\_\_\_ Separation between the forebay and the main basin may be achieved through the use of an earthen berm, gabion baskets, concrete, or a riprap wall.
- A designed overflow section should be constructed on the top of the separation to allow flow to exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design storms.
  - \_\_\_\_ The overflow section may be set at the extended detention volume elevation.
  - The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap) to make sediment removal easier.
- Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay and basin from excessive erosion from heavy equipment operation used for maintenance.
- Provide a typical grading section through the forebay, including typical side slopes, aquatic bench, shoreline protection, etc.

#### 2. Embankment (or dam) and Ponding Areas

- \_\_\_\_\_ Type of embankment:
  - Homogenous embankment
  - Zoned embankment

\_\_\_\_ The earthen embankment must be designed to be stable against any force condition or combination of force conditions that may develop during the life of the structure (including differential settlement within the embankment, seepage through the embankment and foundation, or sharing stresses within the embankment and foundation) and is dependent upon:

- Construction materials
- \_\_\_\_\_ Foundation conditions
- \_\_\_\_\_ Embankment height and cross-section geometry
- Normal and maximum pool levels
- Purpose of structure (i.e., extended detention).
- \_\_\_\_\_ Embankment geometry:
  - \_ Top of dam elevations: constructed height and settled height (allowing for 10% settlement).
    - Height (based on the freeboard requirements): There must be at least 1 foot of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment (excluding the emergency spillway).
    - An embankment *without* an emergency spillway must provide at least 2 feet of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment.
      - \_\_\_\_NOTE: The spillway design storm WSE, if specified, may be substituted for the 100-year storm WSE in either of the above situations.
  - \_\_\_\_\_ Top width varies with embankment height and should be shaped to provide positive drainage.
  - The top of the embankment must be level in order to avoid possible overtopping in one location in cases of extreme storms or spillway failure.
  - Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and 2H:1V upstream face).
  - For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than 3H:1V.
    - The slope profile within an ED pond should be at least 0.5% to 1% to promote positive flow through the pond.
  - Basin side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth of vegetation, provide for easier maintenance, and create a more natural appearance.
- ED pond benches:
  - . The maximum slope of the safety bench is 5%.
  - An aquatic bench should have a maximum depth of 18 inches below the normal pool water surface elevation.
  - \_ Inlet pipe inverts should generally be located at or slightly below the permanent pool elevation.
    - Inlet areas should be stabilized to ensure that non-erosive conditions exist during storm events up to the overbank flood event (10-year design storm).
  - Since most ED ponds are typically on-line facilities, they need to be designed to safely pass the maximum design storm (e.g., the 10-year and 100-year design storms) with adequate freeboard between the maximum design water surface elevation and the top of the embankment.
  - Show the elevations of the permanent pool, treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
    - The maximum Treatment Volume water surface elevation must not extend more than 5 feet above the basin floor or normal pool elevation for a Level 1 design, or 4 feet for a Level 2 design.
    - \_\_\_\_\_ The maximum vertical elevation for ED and channel protection detention over shallow wetlands is 1 foot.

Larger flood control storms (e.g., the 10-year design storm) may exceed the 5 foot vertical limit if they are managed by a multi-stage outlet structure.

The embankment cross-section must be designed to provide an adequate factor of safety to protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability depends upon:

Physical characteristics of the fill materials

- \_\_\_\_\_ Configuration of the site
- Foundation materials
  - \_\_\_\_\_ Shear strength
  - Compressibility
    - \_\_\_\_ Permeability
- Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be designed so that the collection conduits discharge downstream of the embankment at a location where access for observation is possible by maintenance personnel.
- \_\_\_\_\_ Adequate erosion protection is recommended along the contact point between the face of the embankment and the abutments, where runoff concentrates.
  - \_\_\_\_\_ Evaluate whether a gutter surface other than sod is necessary (riprap is generally preferred over a paved concrete gutter).
  - Pond drain: Except for flat areas of the coastal plain, each ED pond designed to have a permanent pool should have a drain pipe that can completely or partially drain the permanent pool.
    - In cases where a low level drain is not feasible (such as in an excavated pond), a pump wet well should be provided to accommodate a temporary pump intake when needed to drain the pond.
    - The drain pipe should have an up-turned elbow or protected intake within the pond, to prevent sediment deposition, and a pipe diameter capable of draining the pond within 24 hours.
      - \_\_\_\_ The pond drain must be equipped with an adjustable valve located within the riser, where it will not be normally inundated and can be operated in a safe manner.
- Trees, shrubs or any other woody plants should not be planted or allowed on the embankment or adjacent areas extending at least 25 feet beyond the embankment toe and abutment contacts.
- Safety features:
  - \_\_\_\_\_ The principal spillway opening must be designed and constructed to prevent access by small children.
  - An emergency spillway and associated freeboard must be provided in accordance with Stormwater Design Specification No. 15 and applicable local or state dam safety requirements.
    - \_\_\_\_ Manage the contours of the basin to eliminate drop-offs or other safety hazards.
- Indicate the top of embankment elevations: constructed height and settled height (allowing for 10% settlement).
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the embankment.
- \_\_\_\_\_ Show the existing ground and proposed improvements profile along the center line of the principal spillway
- Provide a typical grading section through the pond, including typical side slopes with the aquatic bench, shoreline protection, etc.
  - Show the dimensions of zones for any zoned embankment.

# 3. Seepage Control

All utility conduits (except the principal spillway) should be installed away from the embankment.

When utility conduits through the embankment cannot be avoided, they should meet the requirements for spillways:

- \_\_\_\_\_ Watertight joints
- No gravel bedding
- Restrained to prevent joint separation due to settlement

- The contact point between the embankment soil, the foundation material, and the conduit is the most likely location for *piping* to occur, due to the discontinuity in materials and the difficulty in compacting the soil around the pipe.
  - The phreatic line (4:1 slope measured from the principal spillway design high water elevation through the embankment) is the upper limit of the *saturation zone*.
    - \_\_\_\_ At a minimum, this should be the 10-year design storm water surface elevation.
    - If the phreatic line intersects the downstream slope of the embankment, a qualified soil scientist should be consulted to decide if additional controls, such as an internal drain, are needed.
    - Seepage control should be included in the design if the following conditions exist:
      - \_\_\_\_\_ Pervious layers in the foundation are not intercepted by the cutoff.
        - Possible seepage from the abutments may create a wet embankment.
        - The phreatic line intersects the downstream slope.
        - \_\_\_\_\_ Special conditions exist that require drainage to ensure a stable embankment.

Seepage may be controlled by:

- \_\_\_\_\_ Foundation, abutment or embankment drains.
- \_\_\_\_\_ A downstream drainage blanket.
  - A downstream toe drain (often desirable for homogeneous embankments).
  - A combination of these measures.

Seepage along pipe conduits that extend through an embankment should be controlled by use of the following to prevent piping failures along conduit surfaces:

- \_\_\_\_ Anti-seep collar (provide detail).
  - The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA no longer recommend the use of anti-seep collars, in deference to graded filters or filter diaphragms and drainage blankets (more complex to design, but less complicated and more cost-effective to construct and allow for easier placement of fill material).
  - \_\_\_\_\_ Size, based on the length of pipe in the saturation zone (aim is a minimum 15% increase in seepage length).
  - \_\_\_\_\_ Spacing and location of collars on the barrel:
    - \_\_\_\_\_ Maximum collar spacing is 14 times the minimum projection above the pipe.
    - \_\_\_\_\_ Minimum collar spacing is 5 times the minimum projection above the pipe.
    - Collar dimensions should extend a minimum of 2 feet in all directions around the pipe.
  - Anti-seep collars should be placed within the saturation zone. Where the spacing limit will not allow this, then at least one collar must be in the saturation zone.
  - All anti-seep collars and their connections to the conduit should be completely water-tight and made of material compatible with the conduit. NOTE: Dimple bands are *not* considered water-tight.
  - \_\_\_\_\_ Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
  - \_\_\_\_\_ Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless flanged joints are used.
    - Collar size should be calculated using the procedure specified in Chapter 13 of the Virginia Stormwater Management Handbook (2011).
- \_\_\_\_\_ The embankment filter and drainage diaphragm should be designed by a professional geotechnical engineer.
  - \_\_\_\_\_ These devices channel seepage flow through a filter of fine graded material, such as sand, which traps any embankment material being transported.
  - \_\_\_\_\_ The flow is then conveyed out of the embankment through a perforated toe drain or other acceptable technique.
  - \_\_\_\_\_ The critical design element: the filter material grain size distribution is based on the grain size distribution of the embankment fill and foundation material.

The diaphragm should consist of sand, meeting fine concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than 10% passing the No. 100 sieve).

The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to rock, whichever is encountered first.

The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam.

\_\_\_\_\_ The diaphragm should be discharged at the downstream toe of the embankment.

\_\_\_\_\_ The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria.

A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings.

Fabric should *not* be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.

# 4. Foundation and Cut Off Trench or Key Trench

# \_\_\_\_ Label all materials

- The presence of rock in the embankment foundation area requires specific design and construction recommendations (provided by the geotechnical engineering analysis) to ensure a proper bond between the foundation and the embankment.
  - Generally, no blasting should be permitted within 100 feet of the foundation and abutment area.
    - \_\_\_\_\_ If blasting is necessary, it should be carried out under controlled conditions to reduce adverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.), especially critical in karst topography.

Show the cut-off trench bottom width (4 foot minimum or as specified in the geotechnical report).

- \_\_\_\_ Show the cut-off trench depth (4 foot minimum or as specified in the geotechnical report)
- Show the cut-off trench side slopes labeled (no steeper than 1H:1V).

# 5. Multi Stage Riser and Barrel System

- Principal spillways should be sized according to calculation procedures in Chapter 13 of the *Virginia Stormwater Management Handbook (2011).*
- \_\_\_\_ The principal spillway should be located within the embankment and accessible from dry land to ensure easy access for maintenance.
  - Access to the riser should be provided by lockable manhole covers and manhole steps within easy reach of valves and other controls.
- Provide a schedule of materials and clearly label them in drawings.
  - \_ Drop inlet spillways (riser and barrel system) should be designed as follows:
    - Full flow is established in the outlet conduit and riser at the lowest hydraulic head over the riser crest that is feasible. Indicate the crest elevation of riser structure.
      - \_\_\_\_\_ The facility must operate without excessive surging, noise, vibration, or vortex action at any stage.
        - \_\_\_\_\_ Therefore, the riser must have a larger cross-sectional area than the outlet conduit.
- Headwall or conduit spillways consist of a pipe extending through an embankment with a headwall at the upstream end. The headwall is typically oversized to provide an adequate surface against which to compact the embankment fill.
  - Weir spillways should be designed as follows:
    - When used as the principal spillway, it should be armored with concrete or other nonerosive material.
    - \_\_\_\_\_ At the spillway, armoring should extend from the upstream face of the embankment to a point downstream of the spillway toe.
  - \_ All principal spillways should be constructed of non-erosive material with an anticipated life expectancy similar to that of the stormwater management facility.

Pre-cast riser structures may not be substituted if the plans call for a cast-in-place structure, unless approved by the design engineer and the plan approving authority.

- \_\_\_\_\_ Sections of pre-cast structures must be anchored together to meet stability and flotation requirements.
- \_\_\_\_ A separate principal spillway and emergency spillway is generally recommended, unless:
  - \_\_\_\_\_ Topography/abutments too steep.
    - Existing or proposed development conditions impose constraints.
    - Other factors (e.g., a road embankment is used as the dam, the basin is excavated, etc.)
  - In such instances, a combined principal/emergency spillway that passes both low flows and extreme flows may be considered for use, in the form of a drop inlet spillway, a headwall/conduit spillway, or some other design that achieves equivalent results.

It is very important to protect such combined spillways from clogging.

Conduits/structures through embankments:

- Limit the number of conduits that penetrate through the embankment.
- \_\_\_\_\_ Indicate the barrel diameter, inverts, and slope (%).
- \_\_\_\_\_ Show the inverts and dimensions of controlled release orifices/weirs
- \_\_\_\_\_ Show the structure dimensions
- \_\_\_\_\_ Show the extended detention orifice protection
- NOTE: A cause of embankment failure is the separation of pipe joints due to differential settlement and pipe deflection. All connections to pipes must be completely water-tight.
  - The drain pipe (or barrel) connection to the riser should be welded all around when both are metal.
  - \_\_\_\_\_ A rubber or neoprene gasket should be used when joining pipe sections.
  - \_\_\_\_\_ The end of each pipe should be re-rolled by enough corrugations to fit the band width.
  - \_\_\_\_\_ Helically corrugated pipe should have either continuous welded seams or lock seams with internal caulking or a neoprene bead.
  - \_\_\_\_\_ The following connection types are acceptable:
    - For pipes less than 24 inches in diameter:
      - \_\_\_\_\_ Flanges with gaskets on both ends of the pipe
      - A 12-inch wide standard lap type band with a 12-inch wide by ½-inch thick closed cell circular neoprene gasket.
      - A 12-inch wide hugger type band with O-ring gaskets having a minimum diameter of 3/8 inch greater than the corrugation depth.
      - **EXAMPLE** For pipes  $\exists$  24 inches in diameter:
        - \_\_\_\_\_ A 24-inch long annular corrugated band using rods and lugs.
          - A 24-inch wide by 3/8 inch thick closed cell circular neoprene gasket.

Corrugated metal pipe (CMP) must meet or exceed the minimum required design thickness.

Steel pipe and its appurtenances should be galvanized and fully bituminouscoated and should conform to the requirements of AASHTO Specification M-190 Type A with water-tight coupling bands.

Any bituminous coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.

\_\_\_\_\_ Steel pipes with polymeric coatings should have a minimum coating thickness of 0.01 inches (10 mils) on both sides of the pipe.

Coated corrugated steel pipe should meet the requirements of AASHTO M-245 and M-246; the following coatings or an approved equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu-Loy.

- Aluminum coated steel pipe and its appurtenances should conform to the requirements of AASHTO Specification M-274 with water-tight coupling bands or flanges.
  - Any aluminum coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.
- Aluminum pipe and its appurtenances should conform to the requirements of AASHTO Specification M-196 or M-211 with water-tight coupling bands or flanges.
  - Aluminum surfaces that are to be in contact with concrete should be painted with one coat of zinc chromate primer, and hot-dipped galvanized bolts may be used for connections.
    - \_ The pH of the surrounding soils should be between 4 and 9.
- The contractor and project inspector should verify the metal thickness, corrugation size, proper connecting bands, and gasket type.
- Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.
- Water-tight joints are necessary to prevent infiltration of embankment soils into the conduit.
  - \_\_\_\_\_ All joints must be constructed as specified by the pipe manufacturer.
    - Field joints (the ends of the pipes are cut off in the field) should *not* be accepted.
    - With larger pipe sizes, it may be difficult to get water-tight joints, even if the deflection is within design parameters.
  - In such cases, the designer may choose to specify a heavier gage pipe. Bands:
  - \_\_\_\_\_ All connectors must be composed of the same material as the pipe.
  - Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
  - 6-inch hugger bands and "dimple bands" should not be accepted for CMP conduits.
  - For pipes  $\leq$  24 inches in diameter, use 12-inch wide bands with 12-inch O-ring or flat neoprene gaskets.
  - For larger pipes, use 24-inch wide bands with 24-inch wide flat gaskets and four "rod and lug" type connectors.
  - \_\_\_\_\_ Flanged pipe with gaskets may also be used.
  - All pipe gaskets should be properly lubricated with the material provided by the manufacturer, and tensioned, to prevent deterioration of the gasket material.
    - Flat gaskets must be factory welded or solvent-glued into a circular ring, with no overlaps or gaps
- \_\_\_\_\_ The pipe should be firmly and uniformly bedded throughout its length:
  - Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.
  - \_\_\_\_\_ Under no conditions should gravel bedding be placed under a conduit through the embankment.
- Installation of a concrete pipe cradle will help to reduce the risk of piping under the barrel and the subsequent failure of the embankment, resulting from differential settlement.
  - The concrete cradle may not be necessary along the entire length of the conduit to prevent piping, but it is recommended since gravel bedding under an embankment conduit is *never* appropriate unless it is designed as a filter or drainage diaphragm

\_ If the external load (e.g., from the height of the embankment, anticipated construction traffic, the weight of compaction equipment, etc.) on the barrel is enough to warrant provision for its maximum supporting strength, then a concrete cradle should be installed along the conduit's entire length.

Reinforced concrete pipe should have bell and singular spigot joints with rubber gaskets and should equal or exceed ASTM Designation C-361.

Bell and spigot pipe should be placed with the bell end upstream.

\_\_\_\_\_ Joints should be made consistent with manufacturer recommendations.

\_\_\_\_\_ After the joints are sealed for the entire run of pipe, the bedding should be placed so that all spaces under the pipe are filled.

All reinforced concrete pipe conduits should be laid in a *concrete* bedding for their entire length.

This bedding should consist of high slump concrete placed under the pipe and up the sides of the pipe at least 25% of its outside diameter, and preferably to the spring line, with a minimum thickness of 3 inches, or otherwise as shown on the drawings.

Care should be taken to prevent any deviation from the original line and grade of the pipe.

Polyvinyl Chloride (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM D-1785 or ASTM D-2241.

\_\_\_\_\_ Joints and connections to anti-seep collars should be completely water-tight.

\_\_\_\_\_ The pipe should be firmly and uniformly bedded throughout its length.

Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.

\_\_\_\_ All conduits penetrating dam embankments should be designed using the following criteria:

Conduits and structures penetrating an embankment should have a smooth surface without protrusions or indentations that will hinder compaction of embankment materials.

All conduits should be circular in cross-section except cast-in-place reinforced concrete box culverts. This is also true where multiple conduits are employed.

Conduits should be designed to withstand the external loading from the proposed embankment without yielding, buckling or cracking, all of which will result in joint separation.

Conduit strength should not be less than the values shown in the design specifications for corrugated steel, aluminum, and PVC pipes, and the applicable ASTM standards for other materials.

The designer or contractor should obtain a manufacturer's certification that the pipe meets plan requirements for design load, pipe thickness, joint design, etc.

\_\_\_\_\_ Inlet and outlet flared-end sections should be made from materials that are compatible with the pipe.

All pipe joints should be made water-tight by using flanges with gaskets, coupling bands with gaskets, bell and spigot ends with gaskets, or by welding.

Where multiple conduits are employed, sufficient space should be provided between the conduits and installed anti-seep collars to allow for backfill material to be placed between the conduits with earth-moving equipment and easy access by hand-operated compaction equipment.

The distance between conduits should be  $\exists$  1/2 of the pipe diameter, but not less than 2 feet.

Cathodic protection should be provided for *coated welded steel* and *galvanized corrugated metal pipe* when soil and resistivity studies indicate the need for a protective coating against acidic soils.

- \_\_\_\_\_ Outlet protection must be used for the downstream toe of a spillway structure to help dissipate the high-energy flow through the spillway and to prevent excessive erosion in the receiving channel.
  - \_\_\_\_\_ The type of outlet protection depends on the flow velocities associated with the spillway.
    - \_\_\_\_ Riprap is the preferred form of outlet protection, designed according to Chapter 13 of the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet protection material.
      - \_\_\_\_\_ The bottom of the riprap apron should be constructed at 0% slope along its length.
      - \_\_\_\_\_ The end of the apron should match the grade and alignment of the receiving channel.
      - If the receiving channel is well-defined, the riprap should be placed on the channel bottom and side slopes (no steeper than 2H:1V) for the entire length, as required in the design criteria in Chapter 13 of the *Virginia Stormwater Management Handbook (2011)* and the *Virginia Erosion and Sediment Control Handbook (1992).*
      - Riprap placement should not alter the channel's geometry.
      - Excavation of the channel bed and banks may be required to construct the full thickness of the apron.
      - \_\_\_\_\_ If the barrel discharges into the receiving channel at an angle, the opposite bank must be protected up the the 10-year storm elevation. In no instance should the total length of outlet protection be shortened.
      - If a permit requires that no work may be performed in the stream or channel, then the outlet structure must be moved back to allow for adequate protection.
      - \_\_\_\_\_ The horizontal alignment of the apron should have no bends within the design length.
      - \_\_\_\_\_ Additional riprap should be placed if a significant change in grade occurs at the downstream end of the outfall apron.
        - Filter fabric should be placed between the riprap and the underlying soil to prevent soil movement into and through the riprap.
  - All control structures should have a trash rack or debris control device, designed as follows:
    - All trash rack and debris control components should be made of stainless steel or galvanized metal meeting VDOT specifications.
    - Trash racks attached to a concrete spillway structure should be secured with stainless steel anchor bolts.
  - Openings for trash racks should be no larger than 1/2 of the minimum conduit dimension and, to discourage child access, bar spacing should be no greater than 1 foot apart. The clear distance between the bars on large storm discharge openings generally should be no less than 6 inches.
  - \_\_\_\_\_ Flat grates for trash racks are *not* acceptable.
  - Inlet structures that have flow over the top should have a non-clogging trash rack (e.g., a hood-type inlet that allows passage of water from underneath the trash rack into the riser, or a vertical or sloped grate).
  - \_\_\_\_\_ The designer should verify that the surface area of the vertical perimeter of a raised grate equals the area of the horizontal top opening, to allow adequate flow passage should the top horizontal surface become clogged.
  - \_\_\_\_\_ Metal trash racks and monitoring hardware should be constructed of galvanized or stainless steel.
  - Methods to prevent clogging of extended detention orifices in dry extended detention basins should be carefully designed, since these orifices are usually very small and located at the invert or bottom of the basin.
  - All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (*not* required if weir control is maintained in the riser through all flow stages, including the maximum design storm or safety storm):

The device may be a baffle or plate installed on top of the riser, or a headwall set on one side of the riser. The design of a principal spillway riser structure should include a *flotation* or *buoyancy* calculation (see Chapter 13 of the Virginia Stormwater Management Handbook, 2011). The downward force of the riser and footing (to which the riser must be firmly attached) is the structure weight, which must be 1.25 times greater than the buoyant force acting on the riser. Stormwater management facilities having permanent impoundments may be designed so that the permanent pool can be drained to simplify maintenance and sediment removal. The draining mechanism will usually consist of a valve or gate attached to the spillway structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris control device. The typical configuration of a drainpipe will place the valve inside the riser structure with the pipe extending out to the pool area. This configuration results in the drainpipe being pressurized by the hydraulic head associated with the permanent pool. Pressurized pipes should have mechanical joints in order to avoid possible leaks and seepage resulting from the innate pressure. In all cases, valves should be secured to prevent unauthorized draining of the facility. Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that

 sediment removal and other maintenance functions are not hampered.
 An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in the saturated upstream slope of the dam embankment or shoreline area.

\_\_\_\_\_ Therefore, the design of the basin drain system should include specific operating instructions for the owner.

Generally, the drawdown rate should not exceed 6 inches per day.

For embankment or shoreline slopes of clay or silt, the drawdown rate may be as low as 1 inch per week to ensure slope stability.

#### 6 Emergency Spillway

Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the abutments at one or both ends of an earthen embankment or ovr a topographic saddle anywhere on the periphery of the basin. They should *never* be located on any portion of the embankment fill material.

Excavated emergency spillways consist of three elements:

\_\_\_\_ An inlet channel, through which *subcritical* flow enters the spillway.

The inlet channel should have a straight alignment and grade.

The cross-sectional area of flow in the inlet channel should be large in comparison to the flow area at the control section.

Where the depth of the channel changes to provide for the increased flow area, the bottom width should be altered gradually to avoid abrupt changes in the shape of the sloping channel banks.

\_\_\_\_\_ A level section, which controls the depth of flow.

The maximum design water surface elevation (normally for the 100-year storm) through the emergency spillway should be at least 1 foot lower than the settled top of the embankment and should be confined by undisturbed earth or rock.

The bottom width of the spillway should not exceed 35 times the design depth of flow, to avoid damage by meandering flow and accumulated debris.

Whenever the required bottom width is likely to be excessive, consideration should be given to incorporation of a spillway at each end of the dam.

\_\_\_\_\_ The two spillways do not need to be of equal width if their total capacity meets design requirements.

An exit spillwav	-	through	which	either	critica	l or si	Ipercritical	flow	disch	narges f	rom t	he
	The aligr						straight to escaping			0		
	damage <sup>-</sup>	the emba	nkmer	nt.		•						

- The exit channel should have the same cross-section as the control section.
  - The slope of the exit channel must be:
    - Adequate to discharge the peak flow within the channel.
      - No greater than that which will produce maximum permissible velocities for the soil type or the planned grass cover.
        - \_\_\_\_ The slope range of the exit channel is selected to ensure *supercritical* flow in the channel.
- \_\_\_\_\_ The control section is the point on the spillway where the flow passes through *critical* depth, usually installed close to the intersection of the earthen embankment and the emergency spillway centerlines.
- The type of soil and vegetative cover used in the emergency spillway can be used to establish the spillway design dimensions and geometry.
  - Vegetation provides a degree of retardance to the flow through the spillway, depending mostly on the height and density of the vegetative cover chosen.
- Hydraulic design for emergency spillways must be done in accordance with criteria provided in Appendix C: Vegetated Emergency Spillways of the Introduction to the New Virginia Stormwater Design Specifications (as posted on the Virginia Stormwater BMP Clearinghouse web site at http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html ) and in Chapter 13 of the Virginia Stormwater Management Handbook (2011).
- Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.
   Show the existing ground and proposed improvements along the center line of the emergency spillway

#### C. Landscape Plan

- \_\_\_\_ The landscaping plan must indicate the methods to be used to establish and maintain vegetative cover in the ED Pond and its buffer area, including the following:
  - Consider including design elements that promote diverse wildlife and waterfowl use within the ED pond and buffer.
    - Show the delineation of pondscaping zones within both the pond and buffer.
  - Provide a planting schedule and specifications (transport / storage / installation / maintenance)
  - Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species if feasible.
  - \_\_\_\_\_ Identify the sources of native plant material.
  - \_\_\_\_\_ Avoid species that require full shade, or are prone to wind damage.
  - \_\_\_\_\_ The planting plan should allow the pond to mature into a native forest in the right places, but yet keep mowable turf along the embankment and all access areas.
    - A wooded wetland approach may be a good option for many ED ponds.
  - \_\_\_\_\_ Specify the sequence for preparing the wetland bed, if one is included with the ED pond (including soil amendments, if needed).
  - Woody vegetation may not be allowed to grow within 15 feet of the toe of the embankment nor within 25 feet from the principal spillway structure.
  - \_\_\_\_\_ A vegetated buffer should be provided that extends at least 25 feet outward from the maximum water surface elevation of the ED pond.
  - \_\_\_\_\_ Existing trees within the buffer area should be preserved during construction.
  - \_\_\_\_\_ Permanent structures (e.g., buildings) should *not* be constructed within the buffer area.
  - \_\_\_\_\_ Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for container-grown stock.
  - Extra mulching around the base of trees and shrubs is strongly recommended as a means of conserving moisture and suppressing weeds.
  - Specify preservation measures for existing vegetation

\_\_\_\_ Ensure that topsoil / planting soil is included in final grading plan.

#### **D.** Construction Notes

- \_\_\_\_\_ Ideally, planned ED pond areas should be constructed after the contributing drainage area is completely stabilized.
- ED pond areas *may* be used during construction as sites for temporary sediment traps or basins (properly sized for E&S control purposes), provided the construction plans include notes and graphical details specifying the facility will be de-watered, dredged and re-graded to design dimensions after the original site construction is complete.
  - Installation of the permanent riser should be initiated during the construction phase
  - Design elevations should be set with final cleanout of the sediment basin and conversion to the post-construction ED pond in mind.
  - \_\_\_\_\_ The bottom elevation of the permanent ED pond should be lower than the bottom elevation of the temporary sediment basin.
  - Appropriate procedures should be implemented to prevent discharge of turbid waters when the basin is being converted into a ED pond.
- In some cases, it will be necessary to divert flow while the ED pond is being constructed, so that no sediment flows into the pond area until installation and stabilization are complete.
  - \_\_\_\_ Flow diversions may be required to meet additional requirements of and obtain permits from state and federal regulatory agencies.
  - \_ Construction sequence:
    - Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications.
      - Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
        - \_ The following are critical inspection points:
          - During initial site preparation and installation of E&S Controls.
          - Excavation and grading (e.g., interim and final elevations).
          - Installation of the embankment, the riser/primary spillway, and the outlet structure.
            - Pondscaping installation and final stabilization.
    - \_\_\_\_\_ Check the proposed site for existing utilities prior to any excavation.
    - Assemble the construction materials on-site, making sure they meet design specifications, and prepare any staging areas.
    - Clear, grub and strip the areas designated for borrow sites, embankment construction, and structural work to the desired subgrade, removing all trees, vegetation, roots and other objectional material.
      - \_\_\_\_\_ All cleared and grubbed material should be disposed of outside and below the limits of the embankment and reservoir.
        - When specified, a sufficient quantity of topsoil should be stockpiled in a suitable location for use on the embankment and other designated areas.
    - \_\_\_\_\_ Install applicable temporary E&S control measures prior to construction.
      - Excavate the core trench for the embankment and install the spillway (outlet) pipe, including the downstream rip-rap apron (energy dissipation) protection.
        - The cutoff trench should be excavated into impervious material along or parallel to the centerline of the embankment.
        - Trench side slopes should be laid back in steps at a 1H:1V slope or flatter. (from page 6; conflicts with 2:1 specified on page 10, Earthen Embankment Spec?).
          - Backfill should be compacted with construction equipment, rollers, or hand tampers to assure maximum density and minimum permeability.
  - Install the riser pipe or overflow structure, ensuring the top invert of the overflow weir is constructed level and at the proper design elevation.
  - \_\_\_\_\_ Construct the embankment and any internal berms in 8- to 12-inch lifts, compacted with appropriate equipment.

\_ Areas on which fill is to be placed should be scarified before its placement.

- \_\_\_\_\_ The most permeable borrow material should be placed in the downstream portions of the embankment.
- Install the principal spillway or overflow weir concurrently with fill placement and not excavated into the embankment. A vertical trench through the embankment material (in order to place the spillway pipe) should not be allowed under any circumstances.
  - Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands.
- \_\_\_\_\_ Filter and Drainage Layers:
  - In order to achieve maximum density of clean sands, filter layers should be flooded with clean water and vibrated just after the water drops below the sand surface.
  - The filter material should be placed in lifts of no more than 12 inches in thickness.
  - Up to 4 feet of embankment material may be laced over a filter material layer before excavating back down to expose the previous layer.
  - After removing any unsuitable materials, the trench may be filled with additional 12-inch lifts of filter material, flooded, and vibrated as described above, until the top of adjacent fill is reached.
    - The contractor should ensure that a qualified professional inspect filter and drainage diaphragms, ensuring that backfill material meets specifications for quality, lift thickness, placement, moisture content, and dry unit weight.
- Fill material should be taken from an approved, designated borrow area or stockpile.
  - Fill material should be free of roots, stumps, wood, rubbish, stones greater than 6 inches in diameter, and frozen or other objectionable materials.
  - Fill material for the center of the embankment and the cutoff trench should conform to Unified Soil Classification GC, SC, or CL.
    - Fill material that is beside pipes or structures should be of the same type and quality as specified for the adjoining fill material.
      - The fill material should be placed in horizontal lifts not to exceed 4 inches in thickness and compacted by hand tampers or other manually directed compaction equipment.
      - \_\_\_\_\_ The material should completely fill all spaces under and beside the pipe.
      - \_\_\_\_\_ During backfilling, equipment should not be driven closer the 4 feet horizontally to any part of a structure.
      - Equipment should *NEVER* be driven *over* any part of a structure or pipe, unless compacted fill has been placed to a depth specified by the structural live load capacity of the structure or pipe, that adequately distributes the load.
      - Consideration may be given to the use of other materials in the embankment based on the recommendation of a geotechnical engineer supervising the design and construction.
      - The surface layer of compacted fill should be scarified prior to placement of at least 6 inches of topsoil, which must be properly stabilized.
- Fill material should be compacted with appropriate compaction equipment.
  - \_\_\_\_ The number of necessary passes by the compaction equipment over the fill material may vary with soil conditions.

- Fill material should contain sufficient moisture so that the required degree of compaction will be obtained with the equipment used.
- The minimum required density is 95% of maximum dry density with a moisture content within  $\pm$  2% of the optimum, unless otherwise specified by the engineer.
- Each layer of fill should be compacted as necessary to obtain minimum density.

Compaction tests should be performed regularly throughout the embankment construction.

- Typically, one test per 5,000 sq. ft. on each layer of fill or as directed by the geotechnical engineer.
- Use either a Standard Proctor Test (ASTM D698) or a Modified Proctor Test (ASTM D1557 usually more appropriate for earthen dams).
- \_\_\_\_\_ A new Proctor test is required if the material changes from that previously tested.
- The engineer should certify, at the time of construction, that each fil layer meets the minimum density.
- A geotechnical or construction inspector should be on site during embankment construction to do the following:
  - \_\_\_\_\_ Test fill compaction
  - Observe foundation preparation.
  - Observe pipe installation.
    - Observe riser construction.
  - \_\_\_\_\_ Observe filter installation, etc.
- Construct the emergency spillway in cut or structurally stabilized soils.
- Excavate/grade until the appropriate elevations and desired contours are achieved for the bottom and side slopes of the pond.
- \_\_\_\_\_ Install outlet pipes, including the downstream rip-rap apron (energy dissipation) protection.
- \_\_\_\_\_ Stabilize exposed soils with temporary seed mixtures appropriate for the pond buffer. All areas above the normal pool elevation should be temporarily stabilized by hydroseeding or seeding over straw.
- Plant the pond buffer area and implement any remaining permanent stabilization measures.
- If the ED pond has a permanent pool, the contractor should measure the actual constructed pond depth at three locations within the permanent pool (fore-bay, mid-pond, and at the riser), and these depths should be marked and geo-referenced on an as-built drawing. This will facilitate long-term maintenance.
- Implement any remaining permanent stabilization measures.
- Conduct a final inspection, log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.

# E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook)

- Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
  - Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including installation/maintenance of safety signage; removal and disposal of trash, debris and sediment accumulations; and mowing.
- \_\_\_\_\_ Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the ED pond is not converted to other uses.
- Provide sufficient facility access from the public ROW or roadway to both the ED pond and any pre-treatment practices.

# **IV. COMMENTS**

By: \_\_\_\_\_ Date: \_\_\_\_\_

# 8-A.17.0. REFERENCES

Center for Watershed protection (CWP). July, 2008b. *Post-Construction Guidance Manual: Tool 6 – Plan Review, BMP Construction, and Maintenance Checklists.* Ellicott City, MD.

City of Gresham, Oregon. 2003. Inspection Checklist for Infiltration Systems. Gresham, OR.

City of Gresham, Oregon. 2003. Inspection Checklist for Ponds. Gresham, OR.

Interlocking Concrete Pavement Institute. 2008. *PICP Permeable Design Pro Software*. Herndon, VA. <u>www.icpi.org</u>.

Minnesota Pollution Control Agency. September, 2006. *Minnesota Stormwater Manual, Ver.* 1.1, Appendix D: Operations and Maintenance Checklists. St. Paul, MN.

Virginia Department of Conservation and Recreation (DCR). 1999. Virginia Stormwater Management Handbook. Richmond, VA.

Virginia Department of Environmental Quality (DEQ). 2013. Virginia Stormwater Management Handbook. Richmond, VA.

Virginia Department of Environmental Quality (DEQ). 2013. Various stormwater management BMP specifications. *Virginia Stormwater BMP Clearinghouse* web site: <u>http://www.vwrrc.vt.edu/swc/</u>. Richmond, VA.